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Deposition properties of selective tungsten chemical vapor deposition

Wen-Kuan Yeh a, Mao-Chieh Chen a, Pei-Jan Wang b, Lu-Min Liu b, Mou-Shiung Lin b

* Department of Electronics Engineering, National Chiao Tung University, and National Nano Device Laboratory, 1001 University Rd., Hsinchu, Taiwan, ROC

b Taiwan Semiconductor Manufacturing Company, Hsinchu, Taiwan, ROC

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Abstract

This work investigates the basic deposition properties of selective tungsten chemical vapor deposition (W-CVD) using the process of silane reduction of WF₆ with the SiH₄/WF₆ flow rate ratio less than 0.6 over the temperature range 280–350 °C. Selective W-CVD was performed on a contact hole patterned silicon substrate with in situ NF₃ plasma etching of the silicon substrate prior to the selective tungsten deposition. The W deposition rate, deposition selectivity and W film resistivity were investigated with respect to the SiH₄ partial pressure, WF₆ partial pressure, total (SiH₄ + WF₆) deposition pressure, as well as the flow rate of the hydrogen carrier gas. It was found that the deposition rate is proportional to the SiH₄ partial pressure. With a constant SiH₄/WF₆ flow rate ratio, the deposition rate increases with total pressure. At given flow rates of SiH₄ and WF₆, the deposition rate and film resistivity are dependent on the flow rate of the carrier gas. The experimental results show that the reverse bias junction leakage for the wet etching pretreated W/p⁺-n junction diode is smaller than that of the plasma pretreated diode. On the other hand, the contact resistance of the Al/W/n⁺p diode is smaller than that of the Al/W/p⁺n diode.

Keywords: Deposition; Tungsten chemical vapor deposition; Silane reduction; Resistivity

1. Introduction

Selective tungsten chemical vapor deposition (W-CVD) is one of the most attractive techniques for filling deep submicron contact holes for ULSI applications. Selective W-CVD can be performed using hydrogen (H_2) reduction [1] or silane (SiH_4) reduction [2,3] of tungsten hexafluoride (WF_6) .

Selective W-CVD using the H₂-reduction process suffers from the high reactivity of WF₆ toward the silicon substrate. This causes excessive Si consumption, encroachment at the Si/SiO₂ interface, and wormhole formation in the contact regions [4,5]. These disadvantages do not occur in the silane reduction process [6]. Nonetheless, in both processes, the first reaction that occurs between Si and WF₆ is the so-called Si displacement reaction [7]. During the Si displacement reaction, WF₆ first dissociates on the Si surface, forming WF_x (x < 6) adsorbed on the surface, and then further reduces to W. At the same time, Si is converted into SiF_x ($x \ge 1$) and further changes to SiF₄. The reaction products (e.g., WF_x and SiF_4) that can induce selectivity loss must be removed [8]. Thus Si reduces the WF₆ molecules, leading to the deposition of a W film. As the tungsten surface adsorbs more WF6 species, this highly fluorinated surface would react with SiH₄ to form further W film, leaving SiF_4 and H_2 on the surface [9].

In the SiH_4 reduction process, the chemical reaction of the SiH_4/WF_6 system is rather complicated. For selective W-CVD, the major problem is the lack of understanding and control of the selectivity loss. The most important parameters for the deposition selectivity of the SiH_4/WF_6 chemistry are the deposition temperature and the reactant flow rate. This work investigates the basic deposition properties of selective W-CVD using the SiH_4 reduction process. The deposition conditions of tungsten for submicron contact hole filling were investigated. The electrical characteristics of the W contacted shallow junction were also studied.

2. Experimental

The starting material was p-type $\langle 100 \rangle$ oriented Si wafers with 8–12 Ω cm nominal resistivity and n-type $\langle 100 \rangle$ oriented Si wafers with 10–20 Ω cm nominal resistivity. After RCA standard cleaning, the wafers were thermally oxidized to grow an oxide layer with a thickness of 1500 Å, followed by deposition of 4500-Å-thick BPSG. Diffusion areas with sizes ranging from 200×200 to 1200×1200 μ m were

defined on the oxide covered wafers using the conventional photolithographic technique.

For the p⁺n junction, the junction implant was carried out by BF₂⁺ implantation on the n-type substrate at 30 keV to a dose of 3×10^{15} cm⁻² followed by furnace annealing at 900 °C for 30 min in N₂ ambient. For the n⁺p junction, the junction implant was carried out by As⁺ implantation at 50 keV to a dose of 5×10^{15} cm⁻² followed by furnace annealing at 950 °C for 30 min in N₂ ambient. A 6000-Å-thick TEOS layer was then deposited on all the wafers, and contact holes with sizes ranging from 0.6 to 5 μ m were defined on the wafers using the conventional photolithographic technique. Prior to conducting the selective W-CVD, the wafers were dipped in dilute HF (2%) solution for 30 s, followed by a rinse in deionized water for 2 min. The wafers were then loaded into the load-locked cold wall W-CVD system within 5 min to avoid the formation of native oxide on the Si surface.

An in situ predeposition plasma etching was conducted using the following conditions: r.f. power 30 W, total gas pressure 100 mtorr, NF3 flow rate 12 sccm, and N2 flow rate 72 sccm. After the plasma etching, the wafers were transferred from the plasma etching chamber to the tungsten deposition chamber without being exposed to the atmosphere. In addition, a number of substrate wafers prepared for investigation of the diodes' current–voltage characteristics with respect to the tungsten predeposition treatment of the Si substrate were not subjected to the plasma etching procedure. The base pressure of the CVD chamber was 10^{-6} torr.

In this work, the W-CVD was conducted using the following conditions: substrate temperature 280–400 °C, total gas pressure 100 mtorr, WF $_6$ flow rate 20–30 sccm, SiH $_4$ flow rate 10–20 sccm, and H $_2$ carrier gas flow rate 0–1400 sccm. After the selective W-CVD, Al metallization was applied, followed by 30 min sintering at 400 °C. The thickness of tungsten-filling in the contact hole was determined from the cross-sectional scanning electron microscopy (SEM) micrograph. The W-CVD selectivity was examined using an optical microscope in the dark field mode. The contact resistance was measured using the four-terminal Kelvin structure as well as the contact chain structure.

3. Results and discussion

The Arrhenius plot for selective W-CVD on the submicron contact hole substrate is shown in Fig. 1. The process window for the selective deposition ranged from 280 to 350 °C, with an activation energy of 0.84 eV. In this temperature range, the surface reaction was the dominant process of W-CVD. Higher deposition temperature (>350 °C) facilitated the deposition of W atoms on SiO₂, because the reaction byproduct SiF₂ reacts with WF₆ species, leading to the loss of selectivity. The morphology of the W film deposited at high temperature has a columnar structure and possesses a higher resistivity. In addition, the high deposition temperature enhanced the Si reduction process, causing higher consump-

tion of Si and more severe encroachment at the $\rm Si/SiO_2$ interface. Within the selective process window of 280–350 °C, excellent selectivity, with a selectivity loss of less than 1 cm⁻², can be obtained using a $\rm SiH_4/WF_6$ flow rate ratio smaller than 0.6.

Tungsten can be selectively deposited for submicron contact hole filling at a deposition rate as high as 2300 Å min⁻¹, as shown in Fig. 2. The roughness of the W/Si interface can be quite different for different predeposition substrate surface treatments. For the SiH₄ reduction process, the flow rates of WF₆, SiH₄ and the carrier gas (H₂) were found to greatly

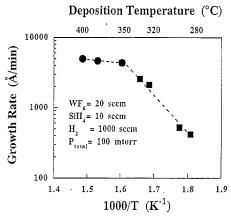


Fig. 1. Dependence of CVD tungsten deposition rate on the deposition temperature.





Fig. 2. (a) Top-view and (b) cross-sectional SEM micrographs showing selective W deposition for submicron contact hole filling.

influence the tungsten deposition rate and deposition selectivity.

The dependence of the tungsten deposition rate on the SiH₄ flow rate for various fixed WF₆ flow rates is shown in Fig. 3. At constant total pressure, the deposition rate is proportional to the SiH₄ partial pressure. At a constant SiH₄/WF₆ flow rate ratio, the deposition rate increases slightly with the total pressure of WF₆ and SiH₄, as shown in Fig. 4. In addition, the SiH₄/WF₆ flow rate ratio was found to have a profound effect on the resistivity of the deposited W film. The W film can be categorized as low-resistivity α -type (ρ < 100 $\mu\Omega$ cm) or high-resistivity β -type (ρ > 300 $\mu\Omega$ cm), depending on the deposition conditions.

Fig. 5 shows the dependence of the tungsten film resistivity on the SiH₄ flow rate for various fixed flow rates of WF₆. At a deposition temperature of 300 °C, low-resistivity W films with a granular structure (α -type) can be selectively and conformally deposited on submicron contact holes with a low (<0.6) SiH₄/WF₆ flow rate ratio. On the other hand, at a high SiH₄/WF₆ flow rate ratio (>2), high-resistivity W films with a columnar structure (β -type) were deposited not only on the Si substrate at the bottom of the contact hole but also along the sidewall of the contact hole, leading to W selectivity loss. For a SiH₄/WF₆ ratio of less than 1, pure W of bulk density and resistivity can be deposited.

The deposition rate and the film resistivity were also found to be dependent on the carrier gas flow rate of hydrogen, as shown in Fig. 6. At a constant total pressure and fixed flow rates of WF₆ and SiH₄, the partial pressures of WF₆ and SiH₄ will increase as the carrier gas flow rate is lowered. Thus, at a very low flow rate of carrier gas or no carrier gas at all, the increased partial pressures of WF₆ and SiH₄ would result in the deposition of W particles on the chamber wall of the W-CVD system and also lead to deposition selectivity loss and high-resistivity β -type film deposition.

The current-voltage characteristics were investigated for the tungsten contacted W/p+n junction diodes, which were fabricated by selective W-CVD on two differently pretreated Si substrates with a defined diode area of $1000 \times 1000 \mu m$. At least 40 randomly chosen diodes were measured in each case. Fig. 7 illustrates histograms showing the distribution of the reverse leakage current density measured at -5 V for the W/p + n junction diodes with two different predeposition substrate treatments. For the diodes with a predeposition substrate treatment of dilute HF wet etch, the average reverse leakage current density is about 2 nA cm⁻². With an additional plasma treatment following the HF wet etch, the diodes' leakage current density was found to be about three times larger than that of the diodes that did not receive the predeposition plasma etching. The plasma etching tended to result in more Si consumption and a rough W/Si interface by the selective W-CVD. This is presumably the main reason for the increased reverse leakage for the shallow junction

The contact resistance was measured for the $Al/W/n^+p$ and $Al/W/p^+n$ diodes. For the $Al/W/n^+p$ diode with a

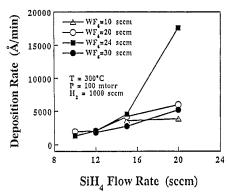


Fig. 3. Dependence of tungsten deposition rate on the SiH_4 flow rate, for various fixed WF $_6$ flow rates.

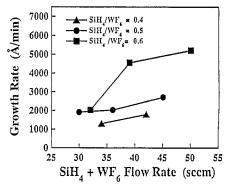


Fig. 4. Dependence of tungsten deposition rate on the total flow rate of SiH_4 and WF_6 , for various fixed SiH_4/WF_6 flow rate ratios.

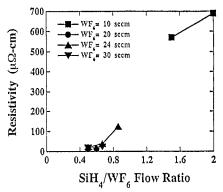


Fig. 5. Dependence of tungsten film resistivity on the SiH_4/WF_6 flow rate ratio, for various fixed flow rates of WF_6 .

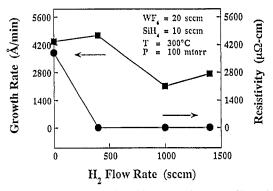


Fig. 6. Dependence of tungsten deposition rate and tungsten film resistivity on the carrier gas (H_2) flow rate.

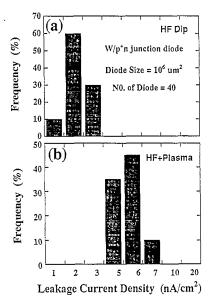


Fig. 7. Histograms showing the distribution of reverse leakage current density measured at -5 V for the W/p^+n junction diodes with the Si substrates pretreated with (a) dilute HF wet etching, and (b) dilute HF wet etching followed by plasma etching.

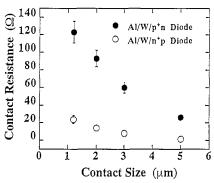


Fig. 8. Contact resistance as a function of contact size for (ullet) Al/W/p⁺n and (\bigcirc) Al/W/n⁺p diode structures.

contact area of $2\times 2~\mu m$, the measured contact resistances are about 20 and 120 Ω , using the four-terminal Kelvin structure and the contact chain structure, respectively. The larger contact resistance measured by the contact chain structure is due to the contribution from the n^+ diffusion layer. Fig. 8 shows the measured contact resistance versus contact size using the Kelvin structure. The contact resistance of the Al/W/p+n diode is about five times higher than that of the Al/W/n+p diode; this is presumably due to the fact that the As atoms are largely segregated at the W/Si interface.

4. Conclusions

Control of deposition selectivity is a problem of vital importance in the development of selective W-CVD. The experimental results in this work have revealed the selective process window for the SiH₄ reduction process to be as follows: substrate temperature 280-350 °C, total gas pressure 100 mtorr, SiH₄/WF₆ flow rate ratio less than 0.6, and H₂ carrier gas flow rate 1000 sccm. At a constant total pressure, the W deposition rate, selectivity loss and W film resistivity are all proportional to the deposition temperature, flow rate of SiH₄, and total pressure of SiH₄ and WF₆. Both the selectivity loss and W film resistivity increase with decreasing flow rate of the hydrogen carrier gas. Prior to the W-CVD, a proper substrate surface treatment must be performed. Better *I–V* characteristics were found for the W/p⁺n junction diodes with the Si substrates wet etched in dilute HF rather than etched in NF₃ plasma prior to the selective W-CVD. The contact resistance of the Al/W/n+p diode is about five times lower than that of the Al/W/p+n diode, which implies a large segregation of arsenic atoms at the W/Si interface.

Acknowledgements

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