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(54) **METHOD OF ENHANCING SPATIAL RESOLUTION FOR DISTRIBUTED TEMPERATURE MEASUREMENT**

(52) **U.S. Cl.** **374/137; 374/161**

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(57) **ABSTRACT**

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A method that utilizes a short sampling interval and a long-pulsewidth laser source to obtain the long sensing range and employs a signal processing technique of decomposing Brillouin spectrum to achieve high spatial resolution, high temperature resolution of the distributed temperature measurement is disclosed. The present method includes the steps of measuring the Brillouin spectra of an optical pulse applying to a sensing fiber and a overlapped area thereof, determining the length that the pulse enters according to the measured Brillouin spectra and a weighting factor and then determining a real Brillouin spectrum profile and a temperature distribution according to Brillouin frequency shifts thereof. For a 9500-m sensing range of standard single-mode fiber and a 100-ns pulsewidth laser source, spatial and position resolutions of 20 cm and a temperature resolution of 1° C. are simultaneously achieved by using this signal processing method.

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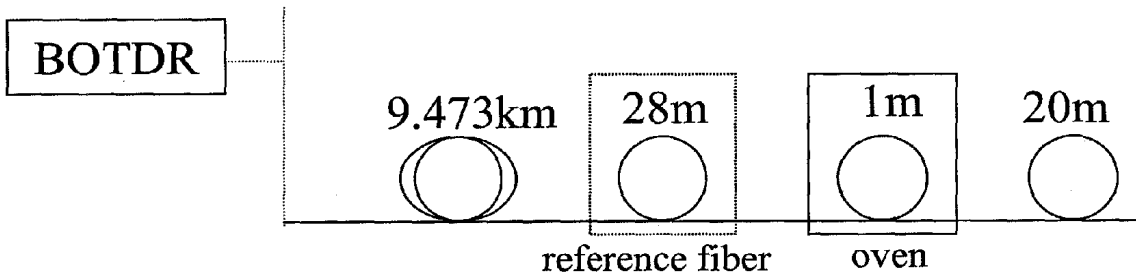
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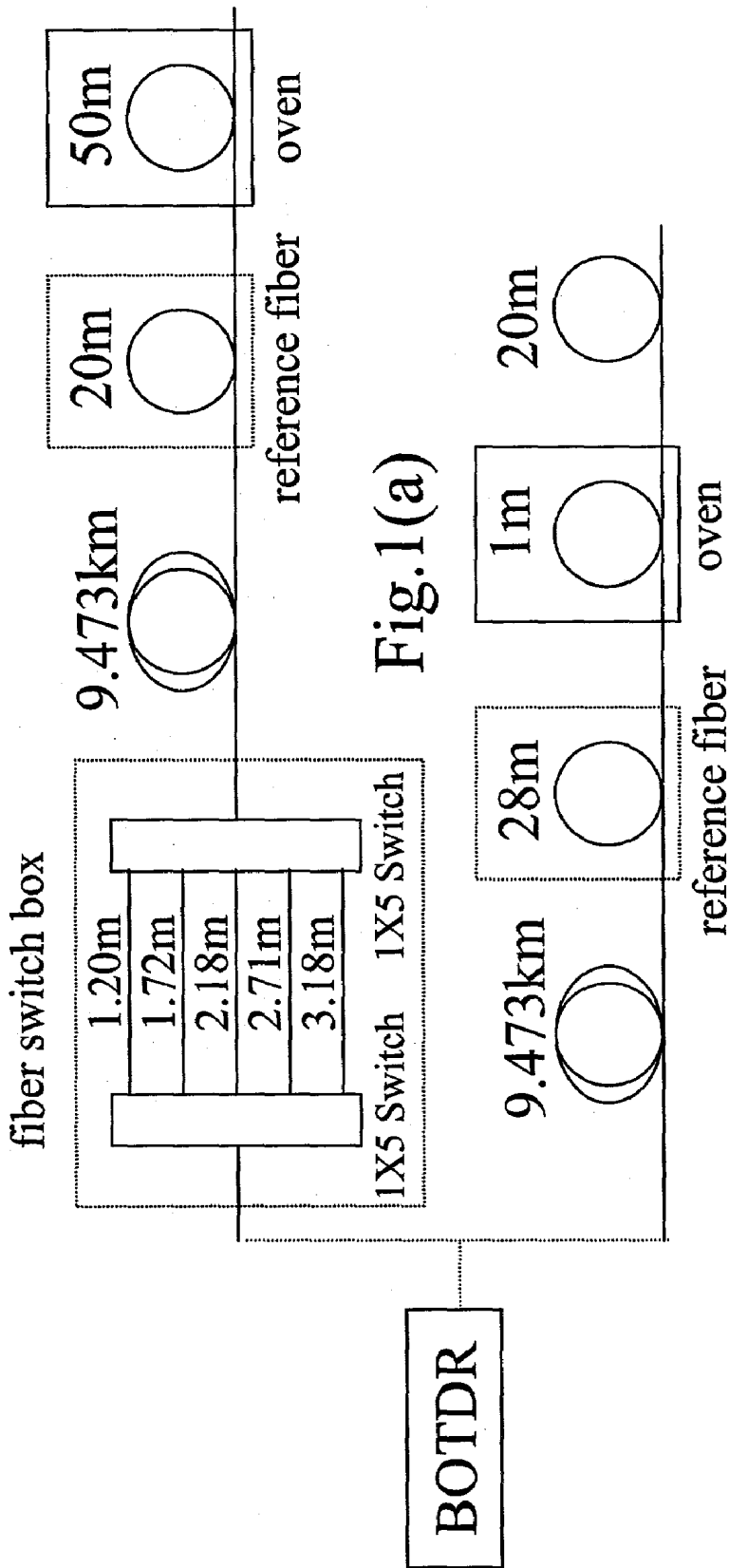


Fig.1(a)

Fig.1(b)

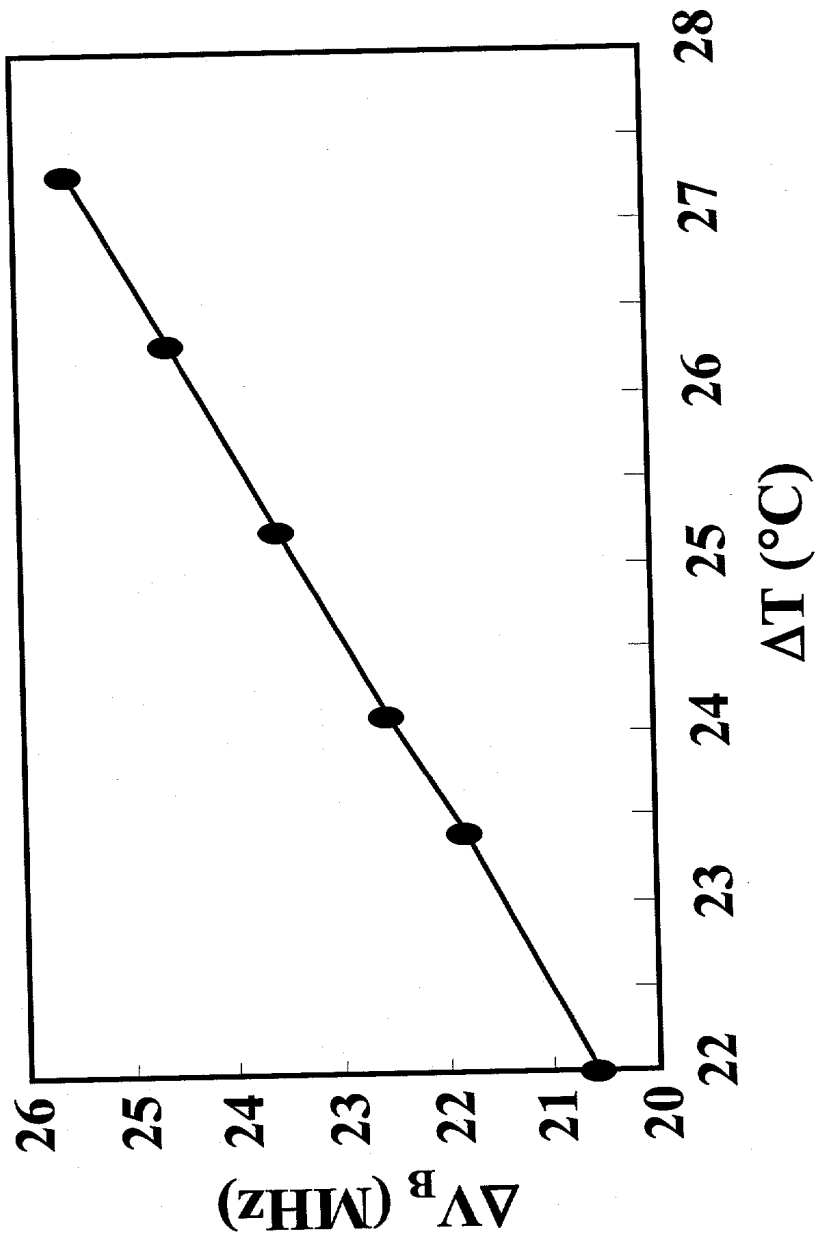


Fig.2

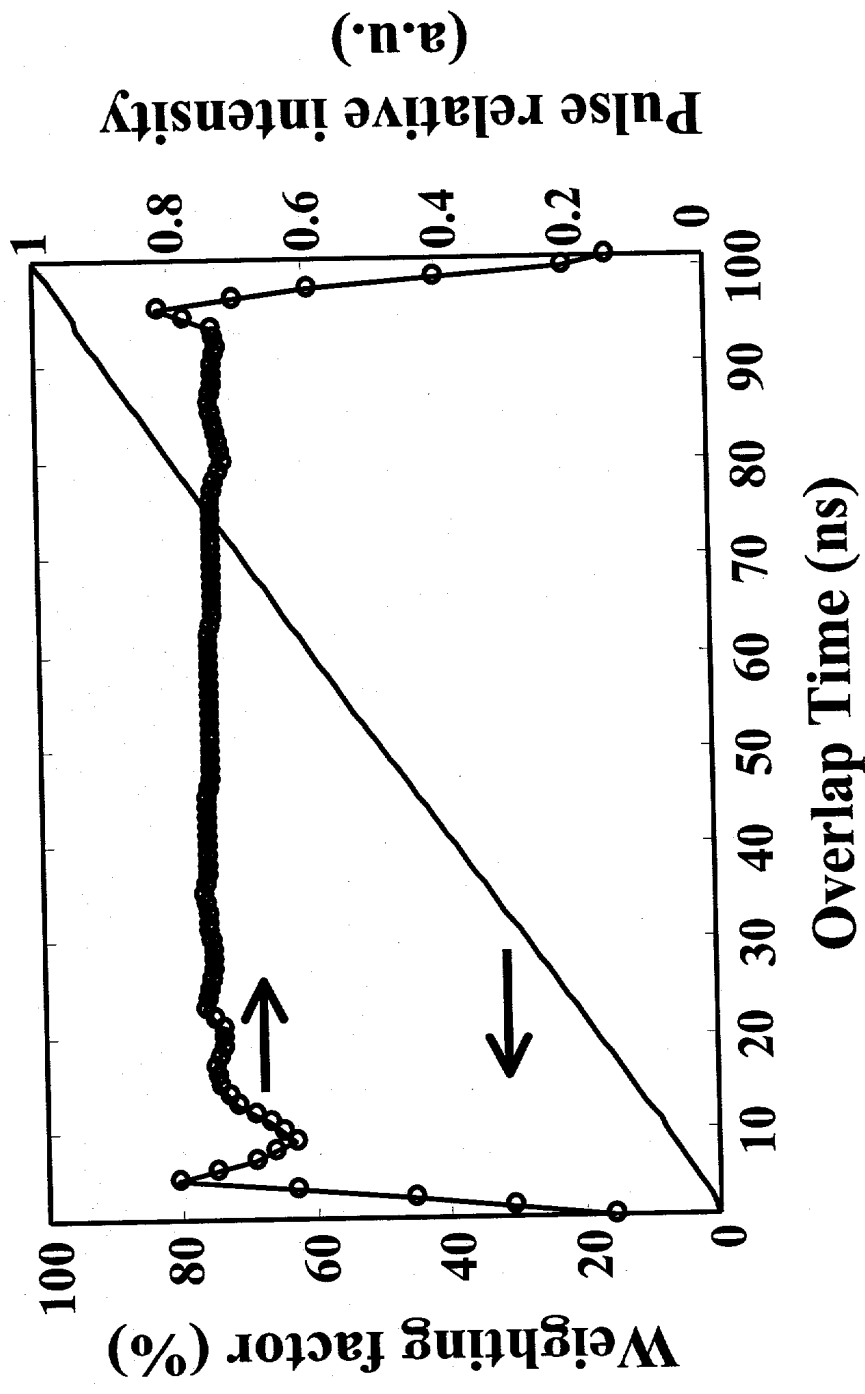


Fig.3

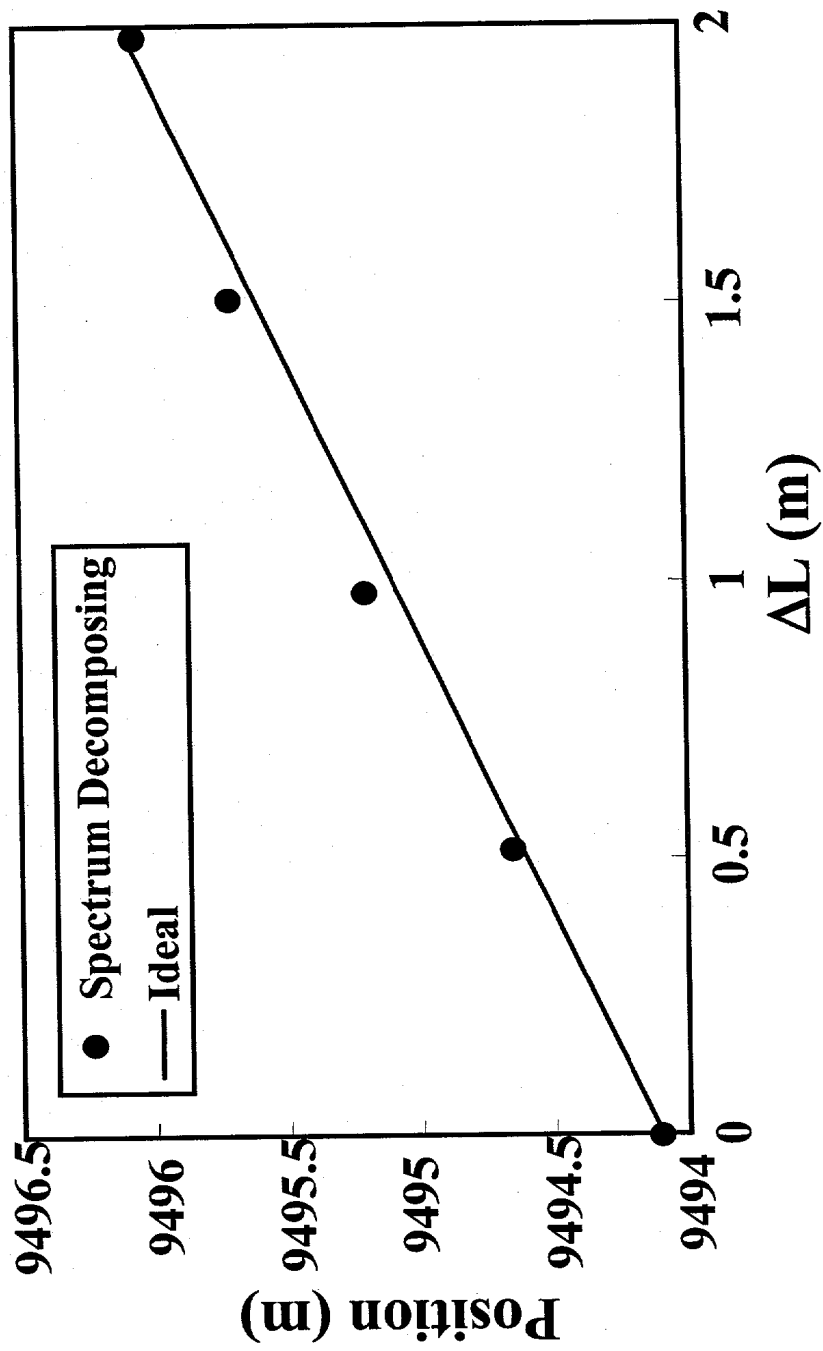


Fig.4

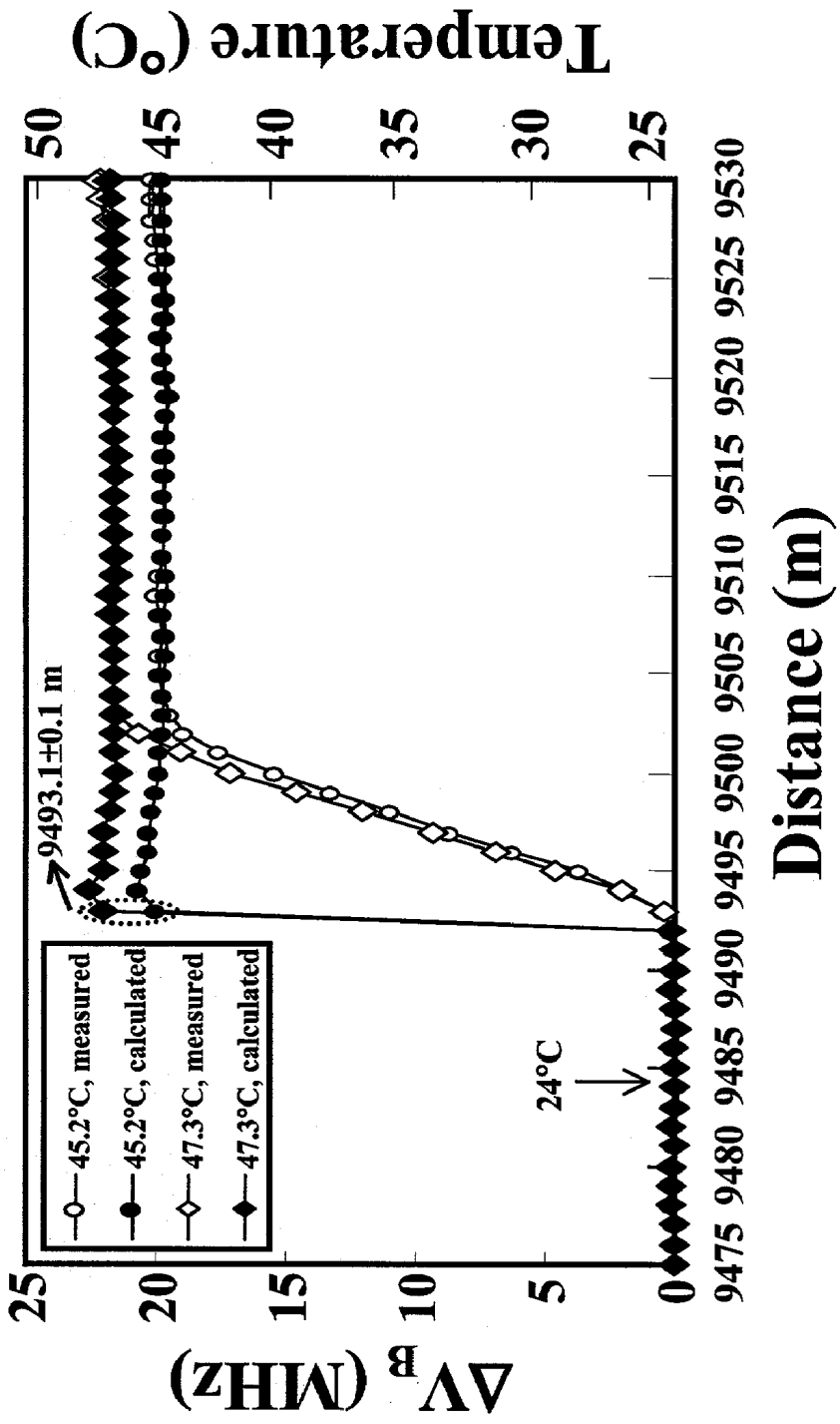


Fig.5

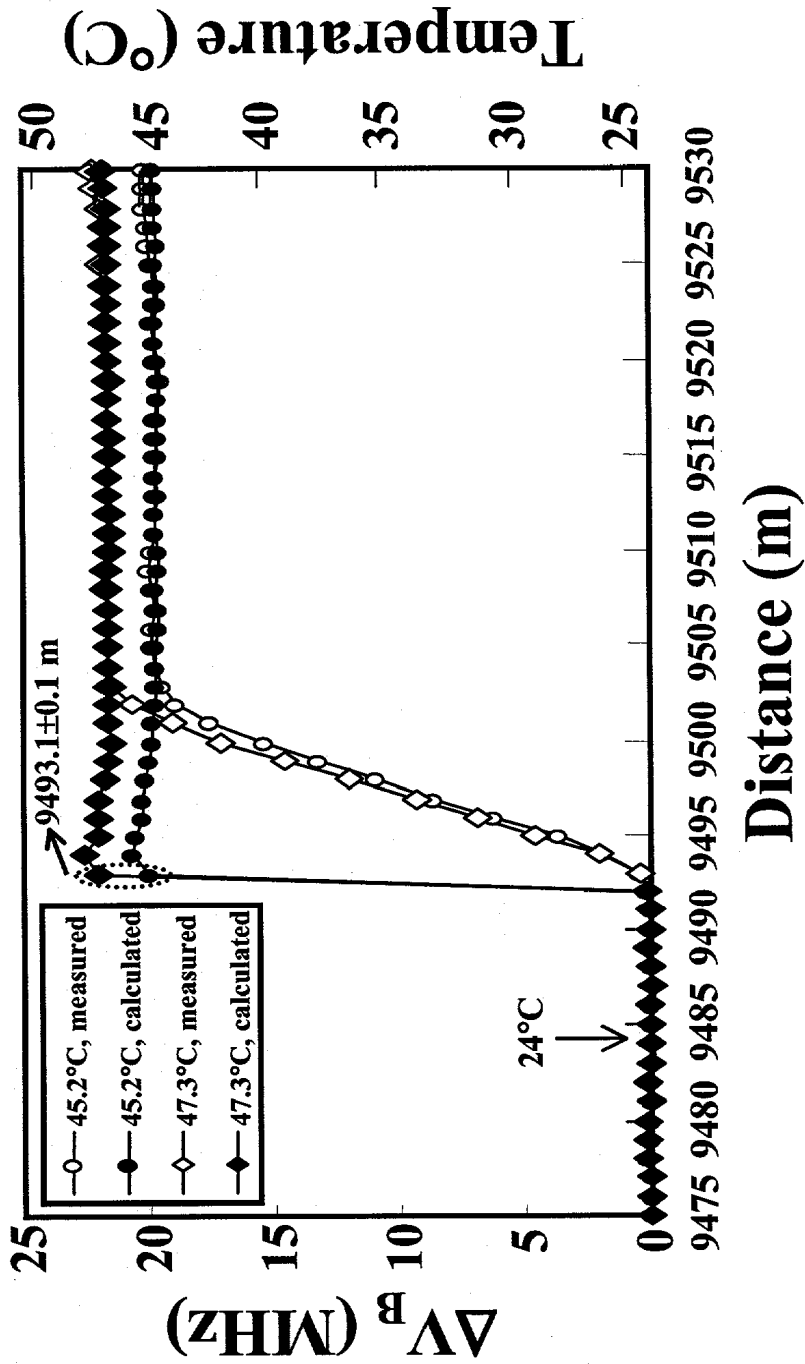


Fig.6

METHOD OF ENHANCING SPATIAL RESOLUTION FOR DISTRIBUTED TEMPERATURE MEASUREMENT

BACKGROUND OF THE INVENTION

[0001] 1. Field of Invention

[0002] The present invention relates in general to a distributed temperature sensing method based on the spontaneous Brillouin scattering effect, more particular, to a spectrum decomposing method to achieve high spatial resolution, high temperature resolution and long sensing range of the distributed temperature measurement.

[0003] 2. Description of Related Art

[0004] There are two ways to fulfill the distributed sensing approach. One includes the use of single sensors being discretely arranged along a sensing line, but will make the whole sensing system much complicated. The other one as described hereinafter includes the use of optical-fiber sensors to obtain the detecting physical parameters along a linear fiber depending upon the optical characteristics thereof. Under the circumstances, the optical fiber are regarded, on one hand, as an active component for sensing measurement and, on the other hand, as a passive component for the information transmitting material to obtain the following advantages:

[0005] 1. The optical fiber is small in volume and light. Thus, the optical fiber can be adopted easily anywhere.

[0006] 2. Since the frequency bandwidth of the optical fiber is large, many signals may be transmitted simultaneously.

[0007] 3. Since the optical fiber is made of nonconductive insulating material, it is not influenced by external electromagnetic waves. Thus, the signal may be transmitted without noise.

[0008] 4. Due to the development of optical fiber technology, optical fibers can be manufactured at a low cost.

[0009] As such, the utilization of fiber-distributed sensing for the measurement of strain and/or temperature distribution is widely applied on many implementations to monitor such as tunnels, bridges, dams and airplanes, buildings and etc. for safety-secured purpose.

[0010] Recently, the distributed temperature sensors (DTS's) that use Brillouin scattering as the sensing mechanism have been intensive studied. The Brillouin frequency shift is dependent on the temperature and strain conditions of the optical fiber, which provides the basis for a sensing technique capable of detecting these two parameters. In the Brillouin-based distributed temperature sensing system, if a higher spatial resolution is accomplished, the measured temperature distribution is more closed to the practical situation of the fiber. The sensing spatial resolution is defined as the 10%/90% rise times from the unheated section to the heated section of the fiber. To achieve higher spatial resolution in a Brillouin scattering system, the measurements utilizing a short-pulsewidth laser source have been reported, which are disclosed by T. Horguchi, K. Shimizu, T. Kurashima, M. Taleda, and Y. Koyamada, published in *J.*

Lightwave Technol., 13, 1296 (1995), and A. Fellay, L. Thevenaz, M. Facchini, M. Nikles, and P. Robert, published in *Proc. OSA Tech. Dig.*, 16, 324 (1997). However, owing to the Brillouin linewidth limitation, it is obvious that using the time-domain pulsed approach is unsuitable for distributed measurements of submeter spatial resolution unless other techniques are employed. More recently, several methods have been reported for performing the measurement with submeter spatial resolution. One such technique, disclosed by K. Hotate and T. Hasegawa, published in *Tech. Dig. Opt. Fiber Sens.*, 17, 337(1999), is the direct-frequency modulation method that demonstrated a sensing spatial resolution of 45 cm over 7.8 m sensing range, and another techniques, disclosed by M. D. DeMerchant, A. W. Brown, X. Bao, and T. W. Bremner, published in *J. Lightwave Technol.* 38, 2755 (1999), and A. W. Brown, M. D. DeMerchant, X. Bao, and T. W. Bremner, published in *J. Lightwave Technol.* 17, 1179 (1999), utilize the sensing fiber with uniform strain and identical length in each section to achieve the spatial resolution of 40 cm and even 25 cm with the enhancement of compound spectra processing method. In addition, a Brillouin-based distributed temperature sensing system that provide a spatial resolution of 35 cm and a temperature resolution of 4.3° C. over 1 km based on measuring the Landau-Placzek ratio with a pulsewidth of 3.5-ns has also been reported by H. H. Kee, G. P. Lees, and T. P. Newson, *IEEE Photon. Technol. Lett.*, 12, 873 (2000). However, the short-pulsewidth laser sources are requisite for these methods to accomplish measurements of submeter spatial resolution. Thus the sensing ranges of these methods are limited.

SUMMARY OF THE INVENTION

[0011] It is therefore, in one aspect, an object of the present invention to provide a method that can provide a distributed temperature measurement with high spatial resolution and long sensing range based on decomposing the spectra of the spontaneous Brillouin scattered signals. This method utilizes a long-pulsewidth laser source to derive the long sensing range and employs a signal processing technique of decomposing Brillouin spectrum to raise the spatial and resolutions to submeter level.

[0012] According to the above-mentioned objects of the present invention, the method for distributed temperature measurement based on decomposing spectra of spontaneous Brillouin scattered signals, includes: (a) supplying a laser source with an optical pulse to an optical fiber; (b) obtaining a first Brillouin spectrum at a referenced temperature, and at least a second Brillouin spectrum and a third Brillouin spectrum in a temperature overlapped region of the optical fiber, the measured Brillouin spectra with respect to the optical pulse enter a fiber section of the optical fiber with a length of d at a traveling time t_d for $t_1 > t_d > t_0$ and a sampling interval $t_1 - t_0$; (c) determining the length of d according to measured Brillouin spectra and a weighting factor, ranged from 0 to 1; (d) determining a real Brillouin spectrum profile of the fiber section according to the length of d and the corresponding weighting factor and the measured Brillouin spectra; and (e) obtaining a temperature distribution according to Brillouin frequency shifts of the real Brillouin spectrum profile.

[0013] As a result, a spontaneous Brillouin-based distributed temperature sensing system using a new Brillouin spectrum decomposing technique to achieve high spatial and

position resolutions, high temperature resolution and long sensing range. For a 9500-m sensing range of standard single-mode fiber and a 100-ns pulsewidth laser source, a spatial resolution of 20 cm and a temperature resolution of 1° C. are simultaneously achieved by using this signal processing method.

[0014] Further scope of applicability of the present invention will become apparent from the detailed description given hereinafter. However, it should be understood that the detailed description and specific examples, while indicating preferred embodiments of the invention, are given by way of illustration only, since various changes and modifications within the spirit and scope of the invention will become apparent to those skilled in the art from this detailed description.

BRIEF DESCRIPTION OF THE DRAWINGS

[0015] The present invention will become fully understood from the detailed description given herein below illustration only, and thus are not limitative of the present invention, and wherein:

[0016] FIG. 1(a) shows an experimental setup for a long-range sensing approach according to the present invention.

[0017] FIG. 1(b) shows an experimental setup for a short-range sensing approach according to the present invention.

[0018] FIG. 2 shows the averaged change in Brillouin frequency shift as a function of temperature change by comparison structure in FIG. 1(a).

[0019] FIG. 3 shows the measured optical pulse shape and the corresponding weighting factor versus the overlap time of the optical pulse and the sensing fiber.

[0020] FIG. 4 shows the positions of sensing fiber obtained by the present invention with respect to the ideal one versus the changes.

[0021] FIG. 5 shows the measured and calculated results of the change in Brillouin frequency shift and the corresponding temperature along the fiber in FIG. 1(a).

[0022] FIG. 6 shows the measured and calculated results of the change in Brillouin frequency shift and the corresponding temperature along the fiber in FIG. 1(b).

DETAILED DESCRIPTION OF THE INVENTION

[0023] According to the paper discloses by T. Kurashima, M. Taleda, T. Horguchi, and Y. Koyamada, published in *IEEE Photon, Technol. Lett.*, 9, 360 (1997), the Brillouin optical-time-domain reflectometer (BOTDR) can be used to measure the spontaneous Brillouin spectra along an optical fiber from one-end. If the temperature in a fiber section is not uniform, a compound Brillouin spectrum composed of the frequency-domain signals of two sections is observed in the overlapped area where the traveling optical pulse is crossing these two sections. Assuming that an optical pulse enters a fiber section with a length of d at the traveling time t_d and the measured Brillouin spectra, $A(t_i)$ are known for $t_i > t_d > t_0$ ($t_0 = t_i$ -sampling interval), the real Brillouin spectra in this fiber section can be derived by decomposing the measured Brillouin spectra. The subscript, i , represents the sampling sequence of the returned Brillouin scattering lightwave

within this fiber section. If the real Brillouin spectrum profile of this fiber section is B , then the relationship between B and $A(t_i)$ can be expressed by

$$A(t_0) \cdot (1 - W(t_i - t_d)) + B \cdot (W(t_i - t_d)) = A(t_i) \text{ for } t_i - t_d < d/(c/n), \quad (1)$$

$$A(t_0) \cdot (1 - W(t_i - t_d) + W(t_i - t_d - d \cdot n/c)) + B \cdot (W(t_i - t_d) - W(t_i - t_d - d \cdot c/n)) = A(t_i) \text{ for } (c/n) \leq t_i - t_d \leq \text{pulsewidth}, \quad (2)$$

[0024] where c is the velocity of light in a vacuum, n is refraction of index, and $W(t_i - t_d)$, ranged from 0 to 1, is a weighting factor determined by the optical pulse shape and overlap time. Thus t_d , d and B can be derived from the above equations by substituting the measured profiles of compound Brillouin spectra in the overlap area. Moreover, the corresponding sensing temperature of this fiber section will be obtained from the change in the Brillouin frequency shift of B . For Example, if the temporal sampling interval of BOTDR is short enough to achieve $t_2 - t_d < d/(c/n)$, then t_d is, according to Eq. (1), obtain implicitly by

$$A(t_0) \cdot \left[1 - W(t_2 - t_d) + \frac{W(t_2 - t_d) \cdot (1 - W(t_1 - t_d))}{W(t_1 - t_d)} + A(t_1) \cdot \frac{W(t_2 - t_d)}{W(t_1 - t_d)} - A(t_2) \right] = 0 \quad (3)$$

[0025] In addition, Brillouin spectrum profile, B , can be given by

$$B = \frac{A(t_1) - A(t_0) \cdot (1 - W(t_1 - t_d))}{W(t_1 - t_d)} \quad (4)$$

[0026] Consequently, the sensing temperature of this fiber section is derived from the Brillouin frequency shift of B . Nevertheless, the sensing spatial resolution that is defined as the 10%/90% rise times from the unheated section to the heated section is obviously determined by $(t_d - t_0)$ and independent of the used optical pulsewidth of BOTDR. As a result, a distributed temperature measurement with a high spatial resolution and a long sensing range can be accomplished by using a short sampling interval and a long-pulsewidth laser source based on this signal processing method of decomposing Brillouin spectra.

[0027] FIG. 1 shows the experimental setup. A BOTDR with operating wavelength at 1554-nm is used to measure the spontaneous Brillouin spectra along the length of standard single-mode fiber (SMF). For the temperature measurement, three separate sections of the test SMF and an optical switch box are arranged as shown in FIG. 1(a). The optical switch box, as shown in FIG. 1(a), was composed of a pair of 1x5 optical switches and five fiber paths with lengths of 1.20, 1.72, 2.18, 2.71, and 3.18, respectively. The first 9.473-km SMF remained on the original spool as supplied by the manufacturer, the subsequent 20-m SMF is subject to a low-level tension as a reference section, and the final sensing 50-m SMF is placed in a thermally insulated oven. The operating conditions of BOTDR are as following: output power of 23 dBm, pulsewidth of 100 ns, average times of 2^{15} , sweep frequency of 5 MHz, and sampling interval of 2m. FIG. 2 is a plot of the averaged change Δv_B in Brillouin frequency shift as a function of temperature change (ΔT) by comparing the Brillouin frequency shift of

the 50-m sensing SMF with that of the 20-m reference fiber. From these data, the temperature coefficient of the Brillouin frequency shift is determined to be 0.934 MHz/° C. for this SMF. In addition, it can be observed that the temperature resolution is less than 1° C. by using this 50-m sensing SMF.

[0028] FIG. 3 shows the measured optical pulse shape under the BOTDR condition of 100-ns pulsewidth and the corresponding weighting factor, $W(t_i-t_d)$, versus the overlap time, (t_i-t_d) , of the optical pulse and the sensing fiber. It is obvious that the optical pulse has a rise/fall time of <5-ns and the weighting factor is presenting a linear relationship to the overlap time when the overlap time is not in the rising and falling region. To verify that the submeter position and spatial resolutions can be achieved for the temperature measurement by using this signal processing method, the condition in this experiment setup was as same as that in the above case of FIG. 1(a) except that the BOTDR parameter of 1-m sampling interval is set. By switching the 1×5 optical switch pair, the changes in the position of 50-m sensing fiber with 50-cm step can be obtained. In addition, the temperature in the oven was set as 45° C. and the room temperature for reference was 22° C. Using the arrangement in FIG. 1(a), the Brillouin spectra in the overlap region of reference fiber and sensing fiber are measured for different fiber paths in the optical switch box; thus, the location of 50-m sensing fiber for each case can be derived by substituting the measured results into Eq. (3). FIG. 4 shows the positions of the 50-m sensing fiber that are derived by using this Brillouin spectrum decomposing method versus the changes, ΔL , in the position of 50-m sensing fiber referred to the 1.20 m fiber path. Also from FIG. 4, it is known that the position error is within ± 10 cm. To further confirm that the submeter spatial resolution is achievable, the oven temperature of 45.2 or 47.3° C. and the temperature of 24° C. in reference fiber section were set. In addition, the optical switch box is removed. FIG. 5 shows the measured and calculated results of the change Brillouin frequency shift and the corresponding temperature along the fiber. The 10%/90% rise times (also defined as the spatial resolution) from the unheated section to the heated section are measured as 8 m and 8.5 m for oven temperature at 45.2 and 47.3° C., respectively. However, they can be dramatically improved to 20 cm and the corresponding temperature error are within ± 0.5 ° C. as shown in the calculated curves. As a result, a distributed temperature measurement with 20-cm position and spatial resolutions, 1° C. temperature resolution and 9500-m sensing range can be accomplished by using this Brillouin-spectrum decomposing method under the condition of 100-ns pulsewidth laser source.

[0029] To demonstrate the feasibility of this method for the sensing fiber shorter than the product of (c/n) times the optical pulsewidth, the sensing fiber of 1-m is used as shown in FIG. 1(b). In the experimental setup of FIG. 1(b), four separate sections of the test SMF are arranged. Moreover, these four SMF sections are the first 9.473-km SMF remained on the original spool, the subsequent 28-m SMF with low-level tension, the sensing 1-m SMF in the oven, and the final 20-m SMF with low-level tension. The BOTDR parameters are consistent with those in the above experiment. Using this signal processing method, FIG. 6 shows the measured results of the change in Brillouin frequency

shift and the corresponding calculated results of temperature along the fiber for oven temperatures at 45.1 and 47.1° C. and reference fiber section at 20° C. for 1-m sensing fiber. After substituting the measured results into Eq. (3) and (4), the positions (t_d) of the 1-m sensing fiber are calculated as 9501.7 and 9501.6 m for oven temperatures at 45.1 and 47.1° C., respectively. In addition, the sensing fiber lengths (d) are derived as 1.1 m for oven temperature 45.1 and 47.1° C. Also from these calculations, the sensing temperature for oven temperature at 45.1 and 47.1° C. are 45.0 and 47.2° C., respectively. Consequently, the temperature measurement with spatial resolution of 20-m, temperature resolution of 1° C. and sensing range of 9500 m is retrieved by using this Brillouin-spectrum decomposing method under the condition of 100-ns pulsewidth laser source.

[0030] The invention being thus described, it will be obvious that the same may be varied in many ways. Such variations are not to be regarded as a departure from the spirit and scope of the invention, and all such modifications as would be obvious to one skilled in the art are intended to be included within the scope of the following claims.

What is claimed is:

1. A method for distributed temperature measurement based on decomposing spectra of spontaneous Brillouin scattered signals, comprising the steps of:

supplying a laser source with an optical pulse to an optical fiber and obtaining a first Brillouin spectrum $A(t_0)$ at a referenced temperature;

obtaining the Brillouin spectrum $A(t_1)$ and $A(t_2)$ in a temperature overlapped region of the optical fiber;

measuring the real temperature change according to using the Brillouin spectra $A(t_0)$, $A(t_1)$, $A(t_2)$ and a weighting factor $W(t_i-t_d)$ with respect to the optical pulse enter a fiber section of the optical fiber with a length of d ;

determining a real Brillouin spectrum profile B and the Brillouin frequency shift ν_B of the fiber section according to the length of d and the corresponding weighting factor $W(t_i-t_d)$ and the measured Brillouin spectra $A(t_0)$, $A(t_1)$, $A(t_2)$; and

obtaining a temperature distribution according to Brillouin frequency shifts ν_B of the real Brillouin spectrum profile B .

2. The method as claimed in claim 1, wherein the step of supplying the laser source includes supplying a long-pulsewidth laser.

3. The method as claimed in claim 1, further comprising the step of applying a Brillouin optical-time-domain reflectometer (BOTDR) to measure the Brillouin spectra $A(t_i)$.

4. The method as claimed in claim 1, wherein the relation of the length (t_i-t_d) , the Brillouin spectra $A(t_0)$, $A(t_1)$, $A(t_2)$ and weighting factor $W(t_i-t_d)$ is given by

$$A(t_0) \cdot \left[1 - W(t_2 - t_d) + \frac{W(t_2 - t_d) \cdot (1 - W(t_1 - t_d))}{W(t_1 - t_d)} + A(t_1) \cdot \frac{W(t_2 - t_d)}{W(t_1 - t_d)} - A(t_2) \right] = 0.$$

5. The method as claimed in claim 1, wherein the step of determining the real Brillouin spectrum profile B is given by

$$B = \frac{A(t_1) - A(t_0) \cdot (1 - W(t_1 - t_d))}{W(t_1 - t_d)}.$$

6. The method as claimed in claim 1, wherein the sample interval is short enough to achieve $t_2 - t_d < d/(c/n)$, wherein c is the velocity of light in a vacuum and n is a refraction of index.

7. The method as claimed in claim 1, wherein the weighting factor $W(t_i - t_d)$, ranged from 0 to 1.

8. The method as claimed in claim 1, wherein the more precision Brillouin spectra takes approximation of the equation with two unknown curve.

9. A method for distributed temperature measurement, comprising the steps of:

providing a reference fiber to obtain Brillouin frequency shifts and an average, and to build a weighting factors chart;

supplying a laser source with an optical pulse to an optical fiber and obtaining a first Brillouin spectrum $A(t_0)$ at a referenced temperature;

obtaining the Brillouin spectrum $A(t_1)$ and $A(t_2)$ in a temperature overlapped region of the optical fiber;

taking a real temperature change according to the Brillouin spectra $A(t_0)$, $A(t_1)$, $A(t_2)$ and a first equation with respect to the optical pulse enter a fiber section of the optical fiber with a length of d;

determining a real Brillouin spectrum profile B of the fiber section according to the length of d and a corresponding weighting factor $W(t_i - t_d)$ of the weighting factors chart and a second equation; and

obtaining a temperature distribution according to Brillouin frequency shifts of the real Brillouin spectrum profile B.

10. The method as claimed in claim 9, wherein the step of supplying the laser source includes supplying a long-pulse-width laser.

11. The method as claimed in claim 9, wherein the Brillouin frequency shift in overlapped region of the optical fiber is increased by distance increase and obtains the the Brillouin spectrum $A(t_1)$ and $A(t_2)$.

12. The method as claimed in claim 9, wherein the first equation is

$$A(t_0) \cdot [1 - W(t_2 - t_d) +$$

$$\frac{W(t_2 - t_d) \cdot (1 - W(t_1 - t_d))}{W(t_1 - t_d)} + A(t_1) \cdot \frac{W(t_2 - t_d)}{W(t_1 - t_d)} - A(t_2) = 0.$$

13. The method as claimed in claim 9, wherein the second equation is

$$B = \frac{A(t_1) - A(t_0) \cdot (1 - W(t_1 - t_d))}{W(t_1 - t_d)}.$$

14. The method as claimed in claim 9, wherein the sample interval is short enough to achieve $t_2 - t_d < d/(c/n)$, wherein c is the velocity of light in a vacuum and n is a refraction of index.

15. The method as claimed in claim 1, wherein the weighting factor $W(t_i - t_d)$, is ranged from 0 to 1.

16. The method as claimed in claim 1, wherein the more precision Brillouin spectra takes approximation of the equation with two unknown curve.

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