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Very High Density (44 $fF/\mu m^2$) SrTiO₃ MIM Capacitors for RF Applications

K. C. Chiang,^{a,z} J. W. Lin,^b H. C. Pan,^c C. N. Hsiao,^c W. J. Chen,^d H. L. Kao,^e I. J. Hsieh,^b and Albert Chin^{a,*}

^aDepartment of Electrical Engineering, Nano-Science Technology Center, National Chiao-Tung University, University System of Taiwan, Hsinchu, Taiwan

^bDepartment of Electric Engineering, Chung Hua University, Hsinchu, Taiwan

^cInstrument Technology Research Center, National Applied Research Laboratories, Hsinchu, Taiwan

^dGraduate Institute of Materials Engineering, National Ping-Tung University of Science and Technology, Taiwan

^eDepartment of Electronic Engineering, Chang-Gung University, Hsinchu, Taiwan

We demonstrate a high-performance TaN/SrTiO₃/TaN metal-insulator-metal (MIM) radio-frequency (rf) capacitor with good device integrity of very high capacitance density of 44 fF/ μ m², small voltage linearity α of 54 ppm/V² at 2 GHz, and a small capacitance reduction 3.5% from 100 KHz to 10 GHz. Such large capacitance density can largely reduce the device size used in rf integrated circuits.

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Based on the International Technology Roadmap for Semiconductors (ITRS), continuous down-scaling of the device size of radiofrequency (rf) capacitors is needed to reduce the die size and lower the costs. To meet this requirement, higher capacitance density $(\varepsilon_0 \kappa / t_d)$ is required and using higher dielectric constant (κ) material is the only choice.¹⁻¹⁶ This is because the decreasing dielectric thickness (t_d) results in the degraded device performance of higher leakage current and poorer voltage-dependence of capacitance ($\Delta C/C$). Because the high κ strontium titanate (SrTiO₃)¹⁷⁻¹⁹ dielectric has a very high κ value (reachable to 300) beyond HfO₂ ($\kappa \sim 22 - 24$), Nb₂O₅ ($\kappa \sim 40$),¹¹ TaTiO ($\kappa \sim 45$),^{15,16} or HfTiO, it is important to study the possibility for rf applications. In addition, the SrTiO₃ (STO) is also listed in the DRAM manufacture roadmap, and therefore the STO capacitor may be used for analog, rf, and dynamic random access memory (DRAM) simultaneously to realize low process costs and multifunctional system-on-chip (SoC). In this paper, we have studied STO metal-insulator-metal (MIM) capacitor for rf applications. Very high capacitance density of 44 fF/ μ m², high κ value of 147, and small $\Delta C/C$ of 752 ppm at 2 GHz were obtained at the same time, demonstrating the excellent device performance for rf applications.

Experimental

After depositing 2 μ m of SiO₂ on Si wafer, the lower capacitor electrode was formed using plasma vapor deposited (PVD) TaN/Ta bi-layers. After patterning the bottom electrode, the TaN was treated by NH₃ plasma nitridation. Largely improved interfacial TaON formation, oxygen deficiency, and capacitance density degradation were achieved after post-deposition anneal (PDA).²¹ Then, the 26 and 30 nm thick STO layers were deposited on the TaN/Ta electrode by PVD, followed by 450°C PDA for 1 h under oxygen environment. Finally, the TaN/Al was deposited and patterned to form the top capacitor electrode. The fabricated rf MIM capacitors were characterized using an HP4284A precision LCR meter to 1 MHz, and an HP8510C network analyzer for the S-parameter measurements to 10 GHz.8,9 The series parasitic impedance and parallel rf pads were de-embedded from 'through' and 'open' transmission lines,^{15,22} respectively. The capacitance at rf frequency was extracted from the measured S-parameters using an equivalent circuit model.^{8,9,15,16} respectively. The capacitance at rf frequency was ex-

Results and Discussion

Figures 1a and b show the capacitance-voltage (C-V) and current-voltage (J-V) characteristics of STO MIM capacitors, re-



Figure 1. (a) C-V and (b) *J-V* characteristics of STO MIM capacitors. The C-V results from 100 kHz to 1 MHz are measured from LCR meter and the data from 0.2 GHz to 10 GHz was obtained from the S-parameters. High capacitance density of 44 and 49 fF/ μ m² were measured with low leakage density of 5 × 10⁻⁷ and 6 × 10⁻⁶ A/cm².

^{*} Electrochemical Society Active Member.

^z E-mail: gorden.ee91g@nctu.edu.tw



Figure 2. Measured and simulated $J-E^{1/2}$ of STO MIM capacitors.

spectively. Very high capacitance density of 44 and 49 fF/ μ m² or capacitance-equivalent thickness (CET) of 0.78 and 0.70 nm were measured with low leakage of 5×10^{-7} and 6×10^{-6} A/cm², respectively. Such small CET is useful for ITRS 45 nm node DRAM at year 2010. The leakage current under positive bias (electron injected from bottom TaN) is slightly lower than that under reverse bias (electron injected from top TaN). This may be due to the rough top STO surface from STO crystallization, which creates localized higher electric field in top TaN/STO. The surface roughness between dielectric and electrode is usually responsible for asymmetric performance of MIM capacitors.²³ In addition, note that the leakage current of 5×10^{-7} A/cm² is low enough for rf integrated circuit (IC) applications due to the very high capacitance density of 44 fF/ μ m²: for a typically large 1 pF capacitor used in rf IC, the leakage current is as low as 0.1 pA at 1 V and significantly lower than the leakage current of sub-100 nm transistors.²² Furthermore, a near constant capacitance value with little voltage and frequency dependence is obtained for the STO MIM capacitor, which is important for rf IC under large voltage swing condition.

To study the current conduction mechanism of TaN/STO/TaN MIM capacitors, we have plotted $\ln(J)$ vs $E^{1/2}$ in Fig. 2. Here, both Schottky emission (SE) and Frenkel-Poole (FP) conduction can give a linear $\ln(J)-E^{1/2}$ relation with different slopes (γ), as shown by

$$J \propto \exp\left(\frac{\gamma E^{1/2} - V_b}{kT}\right)$$
[1]

$$\gamma = \left(\frac{e^3}{\eta \pi \varepsilon_0 K_\infty}\right)^{1/2}$$
[2]

where K_{∞} is the high-frequency dielectric constant (= n^2 ; n is the refractive index and equals to 2.4 for STO^{18,19}), and η is a constant with value of 1 or 4 for FP or SE, respectively. From the good matching between measured and Eq. 1 calculated data, the current conduction mechanism changes from SE at low electric fields to FP at higher fields.

To investigate the device rf characteristics of STO MIM capacitors, the S-parameters were measured. Figure 3a shows the measured S-parameters for TaN/STO/TaN capacitors, and the capacitance value is extracted by using the equivalent circuit model shown in Fig. 3b. The MIM capacitor is modeled by R_p and C, where the R_p originates from the high- κ dielectric loss. In addition, the R_s , L_{s1} , and L_{s2} represent the parasitic impedances in the coplanar transmission line used for rf measurements. Good matching between measured and modeled S-parameters are shown in Fig. 3a, indicating the good accuracy for capacitance extraction at rf regime beyond the limited 1 MHz of LCR meter.

The obtained capacitance density is plotted in Fig. 4a. Small capacitance reduction of only 3.5% to 10 GHz is indicative of the



Figure 3. (a) Measured and simulated two-port S-parameters for STO MIM capacitors, from 500 MHZ to 10 GHz and (b) equivalent circuit model for capacitor simulation in rf regime.

good device performance over the whole intermediate frequency (IF) to rf range.^{6,7} However, such extracted capacitance density at the rf regime is not sensitive enough to calculate the small $\Delta C/C$ variation, important for precision capacitors operated under large signal swing. We have used the previous circuit-theory-derived equation⁸ to calculate the $\Delta C/C$ -V from measured S-parameters and the results are shown in Fig. 4b. The measured $\Delta C/C$ -V can be fitted with a second order polynomial equation, where linear (β) and quadratic (α) voltage coefficients of $\Delta C/C$ were obtained. Because the β effect can be canceled by circuit design using differential method, α is the key parameter to cause the unwanted voltage-dependent $\Delta C/C$. The obtained $\Delta C/C$ and α are also plotted in Fig. 4a. Fortunately, both α and $\Delta C/C$ decrease with increasing frequency into the rf region, which is attributed to the trapped carriers being unable to follow the high-frequency signal with typical carrier lifetimes in the range ms to $\mu s.^{8,9,15,16}$ Therefore, high capacitance density of 44 fF/ μ m², small $\Delta C/C$ of 752 ppm, and low α of 54 ppm/V² at 2 GHz are important for high-speed rf IC applications.

The device quality (*Q*) factor and corresponding capacitance extracted from the circuit model⁶ using the S-parameters at rf frequencies is shown in Fig. 5a. Note that a good *Q*-factor >50 is obtained for rf application before resonant frequency (f_r) of ~13 GHz, where the relative low f_r is due to the large capacitance. Furthermore, because the advanced ICs are usually operated at higher temperature due to power dissipation, the temperature-coefficient on capacitance (TCC) is another important factor. Figure 5b shows the TCC obtained from normalized capacitance of STO capacitor as a function of temperatures. Again, the TCC decreases with increasing frequency with TCC values close to previous TiTaO devices.¹⁵



Figure 4. (a) Frequency dependent capacitance density, $\Delta C/C$, and α for a STO MIM capacitor biased at 1.5 V. The data for frequencies >1 MHz was obtained from the S-parameters. (b) The $\Delta C/C$ -V characteristics of a STO MIM capacitor at rf regime.

Conclusions

Very high 44 fF/µm² capacitance density, small capacitance reduction of 3.5% to 10 GHz, and a small α of 54 ppm/V² at 2 GHz were simultaneously achieved in TaN/STO/TaN capacitors processed at 450°C and important for rf application. This high-density MIM capacitor is important for down-scaling the capacitance size and integration with DRAM.

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Figure 5. (a) Q-factor of TaN/STO/TaN MIM capacitors biased at 1.5 V (b) The temperature-dependent normalized capacitance (TCC) with different frequency. The capacitor size is $20 \times 20 \ \mu m$.

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