$High-Performance SrTiO₃ **MIN** Capacitors$ for Analog Applications

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*Abstract***—TaN***/***SrTiO3***/***TaN capacitors with a capacitance** density of $28-35$ $fF/\mu m^2$ have been developed by using a **high-** κ (κ = 147−169) **SrTiO**₃ dielectric containing nanometer**sized microcrystals (3–10 nm). A small capacitance effective thickness was achieved by reducing the interfacial TaON using N⁺ treatment on the lower TaN electrode during post-deposition annealing. The small (92 ppm***/***V²) voltage coefficient of the capacitance and the 3** \times 10^{−8} A/cm^2 leakage current at 2 V exceed the **International Technology Roadmap for Semiconductors' requirements for analog capacitors at year 2018.**

*Index Terms***—Capacitor, International Technology Roadmap for Semiconductors (ITRS), metal–insulator–metal (MIM), SrTiO³ (STO).**

I. INTRODUCTION

A CCORDING to the International Technology Roadmap
for Semiconductors (ITRS) [1], the capacitance density of future metal–insulator–metal (MIM) capacitors has to increase to help reduce chip sizes and the cost of ICs. Besides the high capacitance density $(\epsilon_0 \kappa/t_d)$ and the limited thermal budget necessary for back-end integration, a low leakage current and a small voltage dependence of the capacitance $(\Delta C/C)$ are also necessary for analog functions. To meet these requirements, high dielectric constant (κ) materials [2]–[19] provide the only solution, since decreasing the dielectric thickness (t_d) to increase the capacitance density degrades both the leakage current and the $\Delta C/C$ performance. Therefore, the high- κ dielectrics used in MIM capacitors have evolved from SiON $(\kappa \sim 4 - 7)$ [3]–[5], Al₂O₃ ($\kappa = 10$) [13], HfO₂ ($\kappa \sim 22$) [7]–[11], Ta₂O₅ ($\kappa \sim 25$) [12], [15] to Nb₂O₅ ($\kappa \sim 40$) [16] or TaTiO ($\kappa \sim 45$) [17]–[19].

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SrTiO₃ (STO) is a potential candidate to increase the κ value beyond 45. It has the well-known perovskite-type structure and has a para-electric phase above 105K and a high κ value of ∼ 300 at room temperature. It is an attractive candidate for DRAM [20]–[24] due to the high charge storage capacity and para-electricity (no fatigue or aging problems). To achieve the high κ value, the STO requires heat treatment at 450 °C– 500 ◦C under an oxygen ambient for crystallization [20]–[23]. Therefore, it also requires a Pt or $RuO₂$ lower electrode [21] to withstand the high temperature oxidation, but the high cost and availability of noble metals pose concerns for mass production.

To address this issue, we have fabricated STO MIM capacitors on a conventional TaN electrode, where a $NH₃$ plasma treatment on the lower TaN has been used to improve the electrode stability and capacitance density degradation by forming interfacial TaON during the postdeposition anneal (PDA). We obtained a 28-fF/ μ m² capacitance density, a small quadratic voltage coefficient of capacitance (α) of 92 ppm/V², and low 3×10^{-8} A/cm² leakage current at 2 V. This performance meets the specifications for analog capacitors as set out by the ITRS for the year 2018.

II. EXPERIMENTAL PROCEDURE

The MIM capacitors were fabricated on a $4-\mu m$ SiO₂ that had been deposited on a Si wafer. The lower capacitor electrodes were formed by depositing $0.05-\mu m$ TaN on a 1- μm Ta layer, where the thick Ta was chosen to reduce the parasitic resistance of the electrode and the TaN served as a barrier layer for the STO. After patterning the lower electrode, the TaN was treated by NH³ plasma nitridation at 100 W to improve the lower interface. The 43- and 55-nm STO (Sr/Ti $= 1.1$) dielectric layers were then deposited using RF magnetron sputtering. This was done using a ceramic STO target in a 4:1 $Ar/O₂$ gas mixture at a total pressure of 10 mtorr. This was followed by 400 ◦C– 450 °C furnace annealing for 30 min to \sim 1 h under an oxygen ambient—for crystallization and quality improvement. Finally, TaN/Al was deposited and patterned to form the top capacitor electrode. Cross-sectional transmission electron microscopy (TEM) and secondary ion mass spectroscopy (SIMS) were used to study the metal interface and dielectric properties. The fabricated MIM capacitors were characterized by $J-V$ and capacitance–voltage $(C-V)$ measurements using an HP4156C curve tracer and HP4284A precision LCR meter, respectively.

Fig. 1. (a) C–V and (b) J–V characteristics of TaN/STO/TaN MIM capacitors processed under various conditions. The 400 ◦C PDA yields a capacitance density of 17 fF/ μ m², which increases to 28 fF/ μ m² for a 450 °C PDA and is better with the N⁺ treatment (35 fF/ μ m²).

III. RESULTS AND DISCUSSION

A. Electrical J*–*V *and* C*–*V *Characteristics*

Fig. 1(a) and (b) shows the $C-V$ and $J-V$ characteristics of TaN/STO/TaN capacitors, respectively, which were processed differently. The capacitance density increased from 17 to 28 fF/ μ m² with increasing O₂ PDA temperature and the use of nitrogen plasma (N^+) treatment on the TaN. At the same time, better frequency dispersion, lower leakage current, and higher breakdown voltage (BV) of the MIM devices were obtained. Application of the N^+ treatment on the lower TaN improved the capacitor density from 28 to 35 $\frac{fF}{\mu m^2}$ and decreased the leakage current by nearly an order of magnitude at < 2 V.

Examination of the device performance at 125 °C [Fig. 2(a)] shows that N^+ treatment still improves the leakage current at positive bias. The leakage current and the capacitance density under various process conditions are summarized in Fig. 2(b). The higher O_2 PDA temperature and N^+ treatment generally improve the leakage current and capacitance density of TaN/STO/TaN capacitors.

Fig. 2. (a) $J-V$ characteristics for the devices in Fig. 1 measured at 125 °C. (b) Comparison of the C–V and J–V characteristics of TaN/STO/TaN MIM capacitors.

Fig. 3. $J-V$ and $C-V$ (insert) characteristics of an STO MIM capacitor using optimum process conditions.

To address the ITRS requirements for low leakage current for analog capacitors (at year 2018), we also fabricated highperformance MIM capacitors of other thicknesses. This was done in an attempt to achieve the ITRS goals of 10 $\text{fF}/\mu\text{m}^2$ density, $J/(C \cdot V) < 7$ fA/(pF \cdot V), and α < 100 ppm/V² [1]. Fig. 3 shows the J–V characteristics of a 28-fF/ μ m² density

Fig. 4. Plot of $\ln(J)$ versus $E^{1/2}$ under electron injection from the (a) bottom and (b) top electrode.

capacitor (inserted figure) with a 55-nm thickness fabricated under the optimal conditions of a 450 \degree C PDA and N⁺-treated TaN. A low leakage current of 3×10^{-8} A/cm² at 2 V was measured, which gives a $J/(C \cdot V)$ of 5.4 fA/(pF \cdot V). This meets the ITRS leakage current requirement at 2018 along with 2.8 times better capacitance density. The leakage current under reverse bias (top electron injection) is markedly higher than that under positive bias (injection from the lower electrode). This may be due to the surface roughness originating from the crystallized STO. However, crystallization is needed for the STO to display a high κ value.

B. Current Conduction Mechanism

To investigate the large leakage current difference for different voltage polarities, we have plotted $ln(J)$ versus $E^{1/2}$ in Fig. 4(a) and (b) for electrons injected from the bottom and top electrodes, respectively. A linear $ln(J) - E^{1/2}$ relation is shown, although a strong process dependence and a different slope are observed. The different slopes in the $ln(J) - E^{1/2}$ plot suggest different current conduction mechanisms. It is known that both Schottky emission (SE) and Frenkel–Poole (FP)

Fig. 5. SIMS profile of STO/TaN with or without N^+ treatment on the lower TaN.

conduction can give such a linear $ln(J) - E^{1/2}$ relation with different slopes (γ) as indicated by [22]

$$
J \propto \exp\left(\frac{\gamma E^{1/2} - V_b}{kT}\right) \tag{1}
$$

$$
\gamma = \left(\frac{e^3}{\eta \pi \varepsilon_0 K_\infty}\right)^{1/2} \tag{2}
$$

where k is Boltzmann's constant, T is the temperature in kelvin, e is the electron charge, ε_0 is the permittivity in vacuum, K_{∞} is the high-frequency dielectric constant (= n^2 , where n is the refractive index), and η is a constant with its value equal to 1 or 4 for FP or SE, respectively. The different slopes γ for the SE and FP cases arise from the different energy barriers V_b , corresponding to the work function of the metalelectrode/dielectric in the SE case or the trap energy level in the dielectric for the FP case. The fits to the experimental data give slopes of 1.58×10^{-5} or 3.16×10^{-5} eV $(m/V)^{1/2}$ for the SE or FP mechanisms, respectively, by using $n = 2.4$ for STO [22], [26] in the above equations.

Following the good agreement between measured and calculated data [using (1)], we investigated the dependence of leakage current on process conditions and voltage polarity. For electrons injected from the top TaN electrode, the current conduction mechanism changes from SE at low electric fields to FP at higher fields. The FP-dominated high-field conduction arises because the trapped electrons can gain energy and be emitted from trapped states and contribute to the leakage current. The smaller SE current for the device with lower electrode N^+ treatment is related to the smoother STO/TaN surface, as determined by atomic force microscopy (AFM), where the STO rms roughness improved from 11.2 to 5.9 nm. For the lower electrode injection case, the current conduction mechanism depends on whether the TaN electrode had the N^+ treatment. For the N^+ -treated case, the current conduction mechanism is the same as for top electrode injection, i.e., SE at low field, which changes to FP at high field. However, for the lower TaN electrode without N^+ treatment, the FP mechanism applies

at both low and high fields. These results indicate a higher trap density or deeper trap energies in STO or the STO/TaN interfacial layer when the lower TaN electrode does not have the N^+ treatment.

C. Material Characterization

We measured the SIMS depth profile of the devices to study the origin of the improved leakage current for the N^+ -treated case. As shown in Fig. 5, even under the existing background level of SIMS system, a higher oxygen concentration can be observed in the lower TaN layer without N^+ treatment. The interfacial TaON was formed during STO oxidation annealing but degraded the capacitance effective thickness (CET), capacitance density, and overall κ value. In sharp contrast, the device with N^+ treatment on the lower TaN shows less inter-diffusion and a better interface. In addition, less nitrogen was found in the STO for the treated sample. It is important to note that such an interfacial layer is also responsible to the higher leakage current at low field, as discussed above, and may be due to the higher trap density from the oxygen deficiency as shown by SIMS. This would lead to trap-assisted FP conduction.

The fabricated STO/TaN was also examined by X-ray diffraction (XRD) and TEM. As shown in the XRD spectra of Fig. 6(a), the crystalline phase of STO is dependent on the PDA temperature and time. STO crystallization starts after 450 \degree C PDA, and the degree of crystallization (XRD intensity) increases with increasing PDA time. Because the κ value of perovskite-type STO is known to increase with increasing degree of crystallization, this result explains the larger capacitance density in Fig. 1(a) at higher PDA temperature. The crystallized STO is confirmed by the cross-sectional TEM of Fig. 6(b) and its enlargement in Fig. 6(c). At 43-nm STO thickness, a high κ value of 169 and improved lower STO/TaN interface, compared with previous work [17], were found for the 35-fF/ μ m² density device (0.99 nm CET). The microcrystals, consistent with the XRD measurements, had a grain size of 3–10 nm as indicated in the TEM image. Such micrograined STO is essential in producing thin consistent STO layers for devices [25].

D. ∆C/C*,* α*, and Temperature Coefficient of the Capacitance (TCC)*

 α is an important parameter of MIM capacitors for analog applications. The undesirable voltage dependence can be obtained by fitting the measured $C-V$ characteristics with a secondorder polynomial equation

$$
\Delta C(V) = C_0(\alpha V^2 + \beta V) \tag{3}
$$

where C_0 is the capacitance at 0 V, and α and β represent the quadratic and linear voltage coefficients of capacitance, respectively. Since the effect of the linear β term can be compensated by circuit design using a differential method [27], the α term is the main factor in the voltage dependence. Fig. 7(a) and (b) shows the $\Delta C/C-V$ dependence on N⁺ treatment

 (c)

Fig. 6. (a) XRD spectra of STO after a 400 ◦C–450 ◦C O² PDA. Crystallization of STO was found at 450 °C O₂ PDA. (b) Cross-sectional TEM of STO/N^+ -treated TaN with (c) an enlarged STO image.

and capacitance density, respectively. Good fits to (3) were obtained in all the cases and yielded α . The N⁺ treatment can dramatically reduce α from 1978 to 542 ppm/V² at 1 MHz. This significantly better α is consistent with the improved leakage current and interface properties shown above. An even better α was measured as the STO thickness was increased, although a trade-off of the capacitance density is needed. Under the best conditions—450 °C PDA and N⁺-treated lower TaN—a small α of 92 ppm/V² was obtained in a 28-fF/ μ m² capacitor. This meets the ITRS specifications for year 2018 with nearly

Fig. 7. $\Delta C/C-V$ characteristics for STO MIM capacitors and the dependence on (a) plasma nitridation on the lower TaN and (b) different capacitance densities of 28–49 fF/ μ m². (c) Frequency dispersion of the 28-fF/ μ m² density capacitor.

three times better capacitance density. The frequency dispersion of the capacitance can have a significant impact in precision analog circuit applications [28]. As shown in Fig. 7(c), significantly better frequency dispersion of the capacitance was

Fig. 8. (a) Temperature-dependent normalized capacitance for MIM capacitors with or without plasma nitridation of the lower TaN. (b) α , TCC, and CET as a function of various treated MIM capacitors.

measured for positive bias than negative bias. This is consistent with the lower leakage current in the lower electrode injection case and may be due to the better STO/TaN interface, as discussed above.

Since modern ICs usually operate at elevated temperature, TCC is important. Fig. 8(a) shows the temperature dependence of the normalized capacitance for STO MIM capacitors with and without plasma treatment. TCC increases with increasing temperature but decreases with increasing frequency [7]. It is also strongly dependent on processing conditions. As summarized in Fig. 8(b), higher PDA temperatures and N^+ treatment improved the TCC characteristics. This is similar to the α improvement, which suggests that the primary mechanism determining the TCC is also trap related.

E. Performance Comparison

Fig. 9 shows the dependence of α as a function of CET or the inverse capacitance density $(1/C)$. An exponential decrease of α with increasing CET or $1/C$ was observed for the Ta₂O₅ [12], HfO_2 [10], Tb-doped HfO_2 [8], TiTaO [18], and STO MIM capacitors. This is due to the trap-related leakage current

Fig. 9. ∆C/C−1/C plot of TaN/STO/TaN and various high-κ MIM capacitors. The exponential decrease with increasing $1/C$ is important for designing capacitors for different applications.

TABLE I COMPARISON OF VARIOUS HIGH-κ CAPACITORS. TaN/STO/TaN CAPACITOR SHOWS THE BEST PERFORMANCE, EXCEEDING THE REQUIREMENTS OF THE ITRS FOR 2018

	ITRS ω	Ta_2O_5	Tb-HfO ₂	HfO ₂	TiTaO	This work
	2018	[12]	[8]	[10]	$[17]$	
C Density $(fF/\mu m^2)$	10	9.2	13.3	12.8	10.3	28
J(A/cm ²)		2×10^{-8} (1.5V)	1×10^{-7} (2V)	8×10^{-9} (2V)	1.2×10^{-8} (2V)	3×10^{-8} (2V)
$J/(C\cdot V)$	$<$ 7	14.5	38	2.9	5.8	5.4
$(fA/[pF\cdot V])$		@1.5V	@2V	@2V	@2V	@2V
α (ppm/V ²)	α < 100	3580	2667	1990	89	92

that also has an exponential dependence on CET [7]. For the same CET or capacitance density value, the STO device has the lowest α . This is due to the high κ value of 147–169, which exceeds the $\kappa \sim 22-45$ values for HfO₂, Ta₂O₅, and TiTaO. The $\alpha-1/C$ dependence is important in choosing the required C density and also in meeting the analog specifications of a low α .

The important device parameters for the analog capacitors are summarized in Table I. Among the various high- κ capacitors, the TaN/STO/TaN capacitor shows the best performance, meeting the ITRS requirements for 2018 and with 2.8 times better capacitance density.

IV. CONCLUSION

Using micro-crystallized high- κ SrTiO₃ and a N⁺ treatment on the lower TaN, TaN/STO/TaN capacitors show good device integrity along with 28-fF/ μ m² capacitance density, an α of 92 ppm/V², and leakage current of 3×10^{-8} A/cm² at 2 V. These data exceed the ITRS specifications for analog capacitors for 2018 and have the advantage of simple dielectric processing without requiring noble metal electrodes.

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