



The Influences of Contact Interfaces Between the Indium Tin Oxide-Based Contact Layer and GaN-Based LEDs

Chin-Yuan Hsu,^a Wen-How Lan,^{b,z} and YewChung Sermon Wu^a

^aDepartment of Materials Science and Engineering, National Chiao Tung University, Hsinchu 300, Taiwan

^bDepartment of Electrical Engineering, National University of Kaohsiung, Kaohsiung 811, Taiwan

We have fabricated GaN-based light-emitting diodes (LEDs) using transparent indium tin oxide-based (ITO-based) p contacts. The current-voltage characteristics and life tests of GaN-based LEDs have been studied. LED life tests showed that a pure ITO contact layer had poor reliability at high current stress. We also found that the GaN-based LED could achieve good reliability with a NiO/ITO contact layer. Using transmission electron microscopy and energy-dispersive X-ray spectrometer analyses, we observed In-contained metallic interface between the p-GaN layer and the pure ITO contact layer after annealing at 600°C. It revealed that ITO would react at interface or indiffuse near the interface at 600°C. The LED was degraded with unstable interfaces after life tests (stressed by a 50-mA current injection). To improve the reliability of GaN-based LEDs with the ITO contact layer, we suggest that the NiO layer be used to prevent the reaction and block the leakage pathway.
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GaN-based light emitting diodes (LEDs) operating in the green-to-violet range of the visible spectrum are commercially available and have received much attention. One of the problems in GaN-based devices is the low hole concentration of Mg-doped GaN, which makes it difficult to obtain contact resistance lower than $10^{-4} \Omega \text{ cm}^2$. In order to ohmic contact on p-type GaN, high work function metals such as Ni, Pd, and Pt were applied. The specific contact resistance around 10^{-2} – $10^{-6} \Omega \text{ cm}^2$ can be achieved in the Ni/Au, Pd/Au, Ni/Pt/Au, Pd/Pt/Au, and Ni/Pd/Au series.^{1–4} Among these contacts, the Ni/Au bilayer contact is commonly used as a transparent ohmic contact on p-type GaN due to its low contact resistivity and high transparency.⁵

A high-brightness GaN-based LED is also an interesting issue because of its important role in full-color display and lighting applications. To enhance the output intensity of GaN-based LEDs, it is necessary to reduce the contact resistance and to enhance the transmission efficiency of the upper transparent contact layer (TCL). However, the transmittance of such a conventional Ni/Au contact is only around 60–80% in the 450–550-nm wavelengths. One possible way to solve this problem is to employ transparent indium tin oxide (ITO), instead of Ni/Au, as the p-contact material. ITO is a well-known transparent conducting material with resistivity in the low $10^{-4} \Omega \text{ cm}$ range and with transmittance higher than 90% in the blue wavelength region at optimized conditions.⁶ In fact, ITO has already been used in ZnSe⁷ and AlInGaP-based⁸ LEDs as the current-spreading layer and in AlInGaAs vertical cavity lasers (VCSEL) as an interactivity contact.^{9,10} Recently, several studies have discussed the applications of the ITO contact layer to GaN-based LEDs.^{11–15} Margalith et al. reported the ITO contacted with p-type GaN, but exhibited a higher operating forward voltage for practical LEDs.¹¹ Horng et al. pointed out that Ni-ITO could form good ohmic contact on p-GaN with annealing at 600°C in air.¹²

However, for high-power applications such as projectors and flash lamps, high-power GaN-based LEDs with an ITO p-type contact layer have been studied.¹⁵ Since power dissipation across the p-GaN/metal interface generated Joule heat, failure of LEDs and laser diodes (LDs) was due to indiffusion of the ohmic contact elements along dislocations in the GaN epi layers, leading to an electrical short of the p-n junction.^{16,17} Thus, it is essential to understand the thermal stability and metallurgy of ITO-GaN contact in addition to developing a low-resistance ohmic system.

In this work, the current-voltage I-V properties of GaN-based LEDs with different TCL (ITO-based) conditions have been studied. The surface morphology change has been characterized by scanning electron microscopy (SEM) and X-ray diffraction (XRD) analysis.

We also discuss the life tests of these LED samples at high current stress, such as leakage current and light output variation. Transmission electron microscopy (TEM) and energy-dispersive X-ray spectrometer (EDS) studies have been used to observe the interface between TCL and p-type GaN. This study can clearly characterize the influences of the thermal stability of metal contact layers on GaN-based LEDs compared with the electrical properties and life tests.

Experimental

The blue GaN-based multiple quantum well (MQW) LED wafers were grown by metallorganic chemical vapor deposition (MOCVD) on c-plane sapphire substrate. Trimethylgallium (TMGa), trimethylindium (TMIn), and ammonia (NH₃) were used as Ga, In, and N precursors, respectively. The layer structure consists of a GaN buffer layer, followed by a 1.5- μm undoped GaN layer, a 3- μm Si-(n) doped GaN layer ($n \approx 1 \times 10^{18} \text{ cm}^{-3}$), the active layer, a 0.12- μm -thick Mg-(p) doped AlGaIn cladding layer ($p \approx 5 \times 10^{17} \text{ cm}^{-3}$), and a Mg-(p) doped GaN contact layer ($p \sim 7 \times 10^{17} \text{ cm}^{-3}$). The active region, consisting of seven 5-nm/15-nm InGaIn/GaN quantum wells, is embedded in the region between p-type and n-type layers.

The LEDs were fabricated using standard lithography. In the first process step, a mesa was defined with standard photolithography and etched down into the n-type region by inductively coupled plasma reactive ion etching (ICP-RIE) technology. The TCL was deposited by E-beam evaporation and defined on the p-GaN region. Table I gives the various TCL conditions of the samples. The Ni/Au (4/3.5 nm) and Ni (4 nm) on LED-C and -D were preannealed at 550°C in air for 15 min, respectively. Then, ITO film (250 nm) was deposited by E-beam evaporation at 300°C in O₂ atmosphere, followed by the annealing process at 600°C in air for 15 min. For n-type GaN, low-resistance ohmic contacts around 10^{-5} – $10^{-8} \Omega \text{ cm}^2$ range have been obtained using Ti/Al metals series.¹⁸ The Ti/Al/Ti/Au (10 nm:400 nm/150 nm/800 nm) metals for the n-contact and bonding pad were then deposited with E-beam

Table I. Various TCL conditions of the LED samples.

LED sample	TCL condition
LED-A	Ni/Au(4/3.5 nm) → annealed at 600°C in air for 15 min
LED-B	ITO(250 nm) → annealed at 600°C in air for 15 min
LED-C	Ni/Au(4/3.5 nm) preannealed at 550°C in air for 15 min + ITO(250 nm) → annealed at 600°C in air for 15 min
LED-D	Ni(4 nm) preannealed at 550°C in air for 15 min + ITO(250 nm) → annealed at 600°C in air for 15 min

^z E-mail: whlan@nuk.edu.tw

evaporation, followed by the annealing process at 300°C with continuous nitrogen flow for 5 min. All the annealing processes were performed in a furnace.

The wafers were then cut into chips, which were packaged onto a transverse optical (TO) can. During the life testing, these chips with TO-can form were stressed by a 50-mA current injection at 25°C and a relative humidity of 40%. The electrical characteristics were measured at room temperature with a HP-4155 I-V analyzer. The SEM surface images were taken with a Hitachi S-4000 instrument. For TEM measurements, the specimens were carried out by JEOL JEM-2010 microscope operated at 200 kV.

Results and Discussion

The I-V characteristics of the GaN-based LEDs with various TCL conditions are plotted on a semilogarithmic scale in Fig. 1. In the forward bias region, similar I-V characteristics with the ideality factor (n) around 3.0 can be seen under different TCL conditions. The ideality factors observed are 3.0 for LED-A, 3.3 for LED-B/C, and 3.6 for LED-D. This indicates that the injected carrier recombination current in the space-charge region is a major mechanism of the current transport.¹⁹ For comparison, the dotted line shows a slope with the ideality factor $n = 3$ for room temperature. Thus, similar electron-hole recombination behavior can be expected in these LEDs. From I-V curves, the LEDs (A, B, and C) showed almost the same operating voltage of 3.2 V at a forward current of 20 mA. In the LED-D curve, an increase of the parasitic series resistance and higher operating voltage (approximated 3.6 V) was obtained, which can be attributed to degradation of the TCL ohmic contact on top of the p-type GaN. Figure 2 shows the SEM images and XRD spectra of Ni film on the GaN surface. From Fig. 2a and b, the different surface morphology between as-deposited Ni film and after annealing at 550°C in air can be observed. According to Fig. 2c, the surface morphology change was mainly due to the Ni film being transformed to NiO. This reveals that the TCL of LED-D consisted of a NiO/ITO bilayer, and Ni film preannealed at 550°C in air is transformed to NiO, resulting in increasing contact resistance. In the reverse bias region, the leakage currents ($<1 \mu\text{A}$) at -5 V were slightly different with various TCL conditions.

Figures 3 and 4 show the results of reliability tests by stress at 50 mA and 25°C, conducted on LEDs of the four types shown in Table I. The life tests of reverse leakage current (at -5 V), as shown in Fig. 3, showed that initial leakage currents observed from these LEDs were about the same, consistent with Fig. 1. It was also found that leakage current increased rapidly after 168 h for LED-B. Small increases of leakage currents for LED-A and LED-C were obtained after life tests. In contrast, a slight increase in leakage current could be found from LED-D even with an 840-h burn-in test. In Fig. 4, the life tests of light output variation (at 50 mA) were consistent with

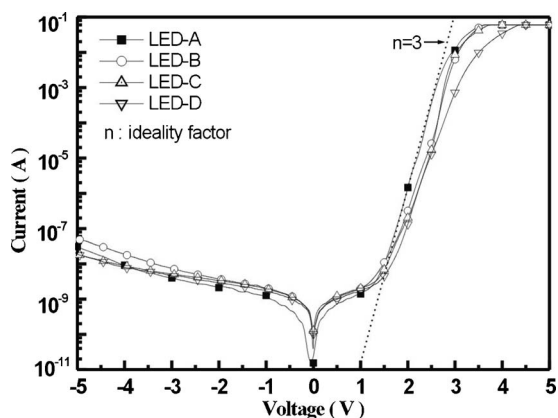


Figure 1. I-V characteristics of GaN-based LEDs with various TCL conditions.

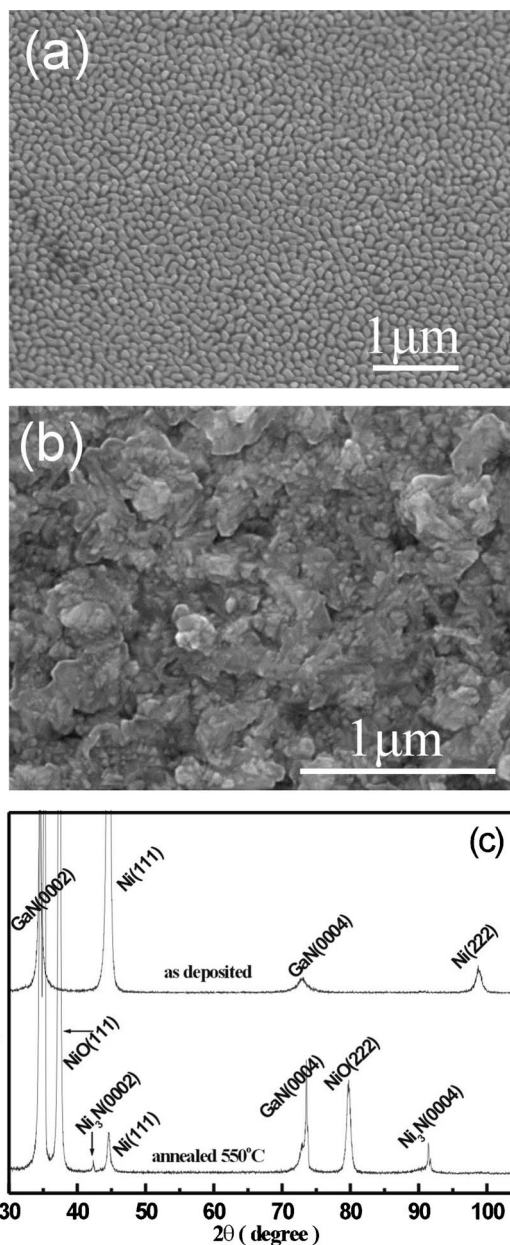


Figure 2. SEM images and XRD spectra of Ni film on GaN surface: (a) surface morphology of as-deposited Ni film on GaN, (b) after annealing at 550°C in air for 15 min, and (c) XRD spectra of as-deposited Ni film and after annealing.

the life tests of reverse leakage current. It could be observed that the optical output power was deteriorated by 10.8% for LED-B. Figures 3 and 4 show that GaN-based LEDs with ITO upper contact were unreliable after a longer burn-in test (stressed by 50 mA). Compared with only an ITO contact layer (LED-B), the NiO/ITO contact layer (LED-D) was stable even with an 840-h burn-in test. These results are probably due to the NiO barrier layer that blocks the leakage pathway. Recently, Weidemann et al. have demonstrated that preferential oxidation of threading dislocations (TDs) causes selective passivation of leakage current paths.²⁰ Thus, the NiO thin film in this case may prevent metal indiffusion along defects or dislocations.

To further understand and confirm the influences of the contact interfaces between contact layers and the p-type GaN layer, we carried out TEM and EDS studies. Figure 5 shows the cross-sectional micrograph of the LED structure before coating contact metal (TCL). The straight TDs were definitely seen in the LED structure.

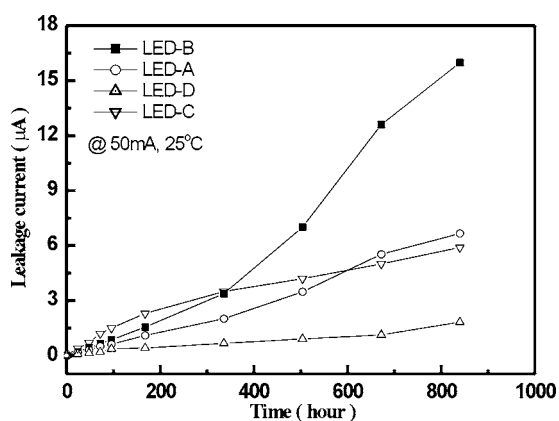


Figure 3. Life tests of reverse leakage current (at -5 V) from GaN-based LEDs with various TCL conditions.

It was observed clearly that the upper p-GaN layer was flat and intact. In the image of the LED-B structure as shown in Fig. 6, ITO film contact on the p-GaN layer was obviously exhibited. In contrast with Fig. 5, the interface geometry changed substantially when it was annealed at 600°C . Numerous nanoscale dark points formed in the GaN just under the interface. It appears that the interface between the ITO layer and p-GaN had been transformed after annealing at 600°C . Under higher magnification, as shown in Fig. 7, the interface should be observed more clearly. The chemical compositions of the exposed regions, marked as "a" in Fig. 7, were analyzed by EDS. The Ga, In, and Sn peaks were detected as shown in Fig. 8a. In the p-GaN layer, marked as "b" in Fig. 7, only the Ga peak was observed, as shown in Fig. 8b. The Au and Cu signals are the background and copper ring, respectively. According to the results of EDS analyses, it is clearly indicated that ITO can react with p-GaN not only at TD (or V-defects) interfaces but also at other interfacial regions. A similar phenomenon in interfacial reactions of Ti/n-GaN contacts at elevated temperature has been reported.²¹ According to the above-mentioned results, we suggest that the ITO layer can react with the p-GaN layer to easily form an In-Ga solid solution near the interface due to the lower eutectic temperature (15.3°C) of the Ga-In phase system. In contrast, Ni film on p-GaN was preannealed at 550°C in air to transform discontinuous NiO film. The discontinuous NiO film may prevent the ITO film from covering completely. The ITO film can also react with the p-GaN layer at partial interface, but part of the TD (or V-defects) interfaces may not react due to NiO protection.

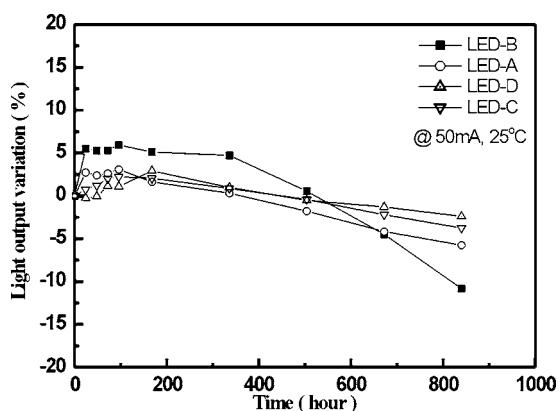


Figure 4. Life tests of light output variation from GaN-based LEDs with various TCL conditions.

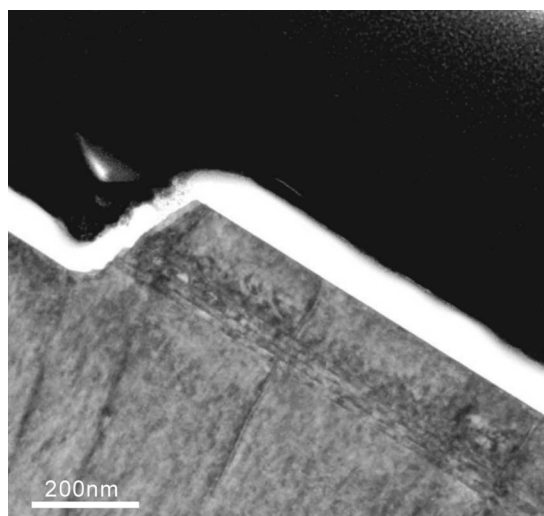


Figure 5. Cross-sectional bright-field TEM micrograph of the LED structure before coating contact metal (TCL).

In our previous study,¹⁶ it was clearly indicated that GaN was decomposed and reacted primarily on GaN dislocations with the Ni/Au contact layer at higher temperatures. It also revealed that the migration and indiffusion of Ni and Au along the TDs cause the short-circuit characteristics of the p-n junction at high temperatures. In another study,²² it was found that In and Sn diffused into the LED structure with defects such as TDs or V-pits. The defects provide leakage paths to cause short circuits in p-n junctions at high annealing temperatures. Thus, we consider that In (or Sn) would also indiffuse along the TDs during high current stress, resulting in degradation. Based on the results obtained in this study, we suggest that the LED-B was degraded with unstable interfaces after life tests (stressed by a 50-mA current injection). The ITO reacts with the p-GaN layer to form an In-Ga solid solution near the interface, easily resulting in metal (In or Sn) indiffusion during burn-in tests. The LED-D has good reliability due to the NiO barrier layer. The barrier layer can prevent ITO film from reacting with GaN at TD positions and may block the metal indiffusion along dislocations.

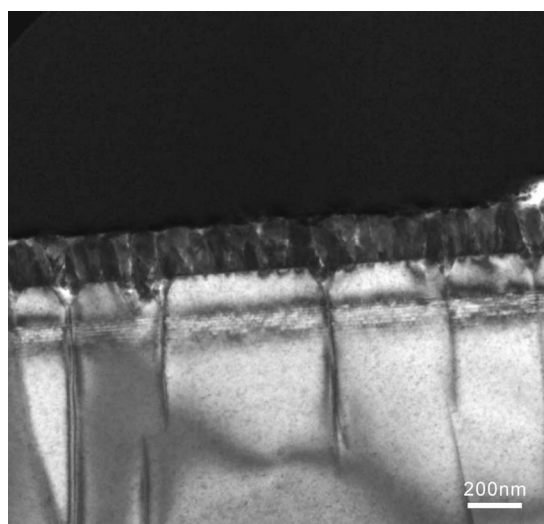


Figure 6. Cross-sectional bright-field TEM micrograph of the LED-B structure.

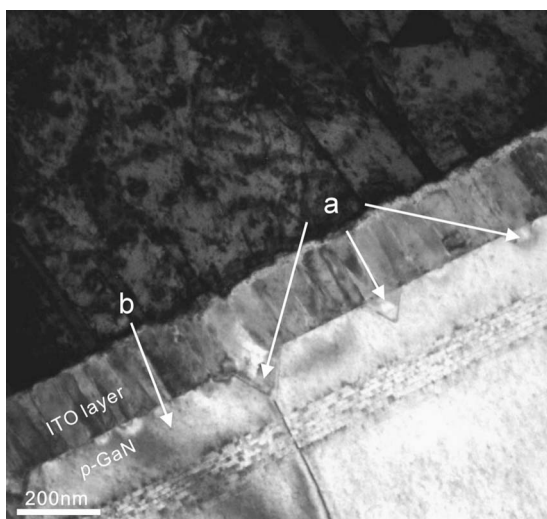


Figure 7. Cross-sectional bright-field TEM micrograph of the LED-B structure with higher magnification image.

Conclusions

We have investigated the influences of contact interfaces between the ITO-based layer and GaN LEDs. In-containing metallic interfaces were observed between the p-GaN and the pure ITO contact layer by TEM and EDS analyses. The GaN-based LED with a pure ITO contact layer had poor reliability at high-current-injection life tests. Furthermore, we also found that the GaN-based LED could achieve good reliability with the NiO/ITO contact layer. These results imply that the ITO would react at interface or indiffuse near the interface at 600°C. The indium (or Sn) would diffuse into an active region along the TDs easily during high-current-injection life tests. To improve the reliability of GaN-based LEDs with the ITO contact layer, a NiO layer could be used to prevent the reaction and block the leakage pathway.

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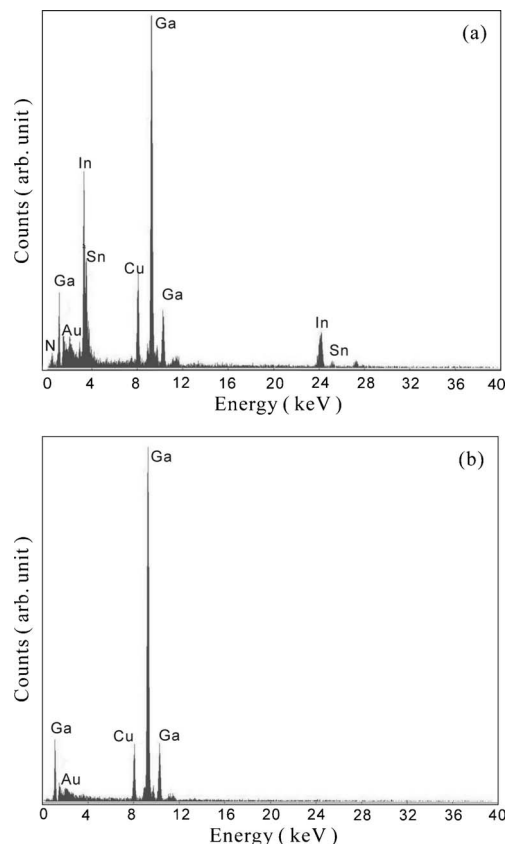


Figure 8. EDS spectra obtained from different regions: (a) at “a” of Fig. 7 and (b) at “b” of Fig. 7.

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