# 5 mm High-Power-Density Dual-Delta-Doped Power HEMT's for 3 V *L*-Band Applications

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Abstract— A high-power-density dual- $\delta$ -doped AlGaAs/InGaAs/GaAs high electron mobility transistor (HEMT) for personal communication applications has been developed. A 5.0 mm gate-width device operating at a drain bias of 3.0 V gave an output power over 1 W. The 1  $\mu$ m gate-length HEMT exhibited a current density of 425 mA/mm at  $V_{\rm gs}=0.5$  V. The maximum transconductance of the device was 270 mS/mm. The effective knee voltage was as low as 0.3 V. At the class AB operation, the HEMT demonstrated an output power density of 200 mW/mm; 64% power-added efficiency and 18.2 dB linear gain at 900 MHz. This is the highest power density of a dual- $\delta$ -doped AlGaAs/InGaAs/GaAs HEMT reported to date for low voltage (3 V) wireless applications.

# I. Introduction

DVANCED high-performance wireless communication systems require high-efficiency power transistors operating at low supply voltage. The advantages of low operation voltage include: (1) reduction of power consumption of the circuits, (2) decreasing the number of the battery cells, and (3) reduction of the size and weight of the systems. Recently, high-efficiency GaAs MESFET's used for cellular telephone applications were reported [1], [2]. However, the operation voltage of these devices is still high (4.7 V). As the operation voltage is lowered, the output power of the devices will drop drastically. In order to increase the output power of the devices operating at 3 V, large peripheries with gate width of 14~16 mm were used [3], [4]. The large gate width of the devices have the following problems: The large gate width increases the chip size and causes a low chip yield which are undesired and unaccepted from the production standpoint of view. Furthermore, increasing in the gate width decreases the output impedance and leads to difficult output matching. The large gate width is also associated with an increase of the total gate leakage current and makes the quiescent gate bias point unstable [5]. In this work, we develop a 5.0 mm gate-width

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high-power-density dual- $\delta$ -doped AlGaAs/InGaAs/GaAs high electron mobility transistor (HEMT) for 3.0 V L-band wireless communication applications. The device when operated at 3.0 V supplied over 1 W output power at 900 MHz. The high output power was achieved by small gate periphery at low operation voltage. The developed HEMT eliminates the problems of large periphery while having the advantages of low operation voltage.

# II. DEVICE FABRICATION

The structure of the dual-δ-doped AlGaAs/InGaAs/GaAs HEMT, as shown in Table I, was grown by molecular-beamepitaxy (MBE) on a (100) semi-insulating GaAs substrate. The structure consists of a 0.6- $\mu$ m-thick undoped GaAs buffer layer, a 20-periods undoped AlGaAs/GaAs superlattice buffer, then an undoped GaAs buffer again. The active part of the structure is an 85 Å In<sub>0.21</sub>Ga<sub>0.79</sub>As channel layer sandwiched between an upper 35 Å undoped Al<sub>0,21</sub>Ga<sub>0,79</sub>As layer and a lower 40 Å undoped GaAs layer. The two dimensional electron gas (2-DEG) was formed in the pseudomorphic InGaAs channel by electron transfer from silicon  $\delta$ -doping above and below the InGaAs layer. The dual-δ-doped structure provides high carrier concentration in the InGaAs channel and leads to high current density and high transconductance  $(g_m)$  which benefits the power performance of the device. An undoped Al<sub>0.21</sub>Ga<sub>0.79</sub>As Schottky barrier layer was grown on the upper  $\delta$ -doping layer to obtain high gate-to-drain breakdown voltage  $(BV_{ad})$ . Both high current density and high breakdown voltage are important for a power device. Finally, a heavily Si-doped  $(5 \times 10^{18} \text{ cm}^{-3})$  GaAs cap layer was formed to provide the good ohmic contact and reduce the source resistance. The fabricated device had a total gate width of 5.0 mm with 1.0  $\mu$ m gate length for each finger, as shown in Fig. 1. The device isolation was accomplished by wet etching with HF:H2O2:H2O etchant. The ohmic metal, Au/Ge/Ni, was deposited by electron-beam evaposition followed by rapid thermal annealing at 300°C for 10 s. The 1.0-\mum-long Ti/Pt/Au gate was defined by the standard photolithography. Silicon nitride (Si<sub>3</sub>N<sub>4</sub>) was used for device passivation.

# III. DEVICE PERFORMANCE

Fig. 2 shows the current-voltage (I-V) characteristics of the 5 mm-wide dual- $\delta$ -doped power HEMT's. The maximum drain current density ( $I_{\rm max}$ ), defined as the drain saturation current density measured at a gate-to-source voltage ( $V_{\rm gs}$ ) of +0.5 V, is 425 mA/mm. The maximum transconductance ( $g_m$ ) is

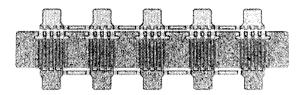


Fig. 1. Photograph of fabricated dual- $\delta$ -doped AlGaAs/InGaAs/GaAs power HEMT with 5-mm gate width and 1- $\mu$ m gate length.

TABLE I
DEVICE STRUCTURE OF HEMT

PROFILE	THICKNESS
N <sup>+</sup> GaAs	400Å
undoped AlGaAs	350Å
Si delta-doping	
undoped AlGaAs	35Å
undoped InGaAs	85Å
undoped GaAs	40Å
Si delta-doping	
undoped AlGaAs	200Å
undoped GaAs	500Å
undoped AlGaAs/GaAs supperlattice	
undoped GaAs	
semi-insulating GaAs substrate	

270 mS/mm. These values are higher than those of MESFET's  $(I_{\rm max}=312~{\rm mA/mm},~g_m=106~{\rm mS/mm})$  [3] and HFET's  $(I_{\rm max}=220~{\rm mA/mm},~g_m=200~{\rm mS/mm})$  [5]. Both the higher drain current density and transconductance are attributed to the dual- $\delta$ -doped HEMT structure. The pinch-off voltage  $(V_p)$  of the HEMT's is about  $-1.7~{\rm V}$ . The effective knee voltage, defined as the drain bias  $(V_{\rm ds})$  value when the drain current  $(I_{\rm ds})$  becomes 100 mA/mm with  $V_{\rm gs}=+0.5~{\rm V}$ , is 0.3 V which is comparable to and even lower than the reported values [3]–[5]. The on resistance, defined as  $V_{\rm ds}/I_{\rm ds}$  with  $V_{\rm gs}=0~V$ , is about 3.3 ohms-mm. The gate-to-drain breakdown voltage, defined at a gate current of 1 mA/mm, is more than 14 V. This value is competitive to those of HFET's and MESFET's  $(BV_{\rm gd}=10~{\rm V})$  [4], [6], [7].

The S-parameter measurements of the devices were performed from 0.5 to 10 GHz for the 1 mm-wide devices using an automatic network analyzer. Based on the S-parameter data, the unity short-circuit current-gain frequency ( $f_t$ ) and the maximum frequency of oscillation ( $f_{\rm max}$ ) can be computed. The  $f_t$  and  $f_{\rm max}$  estimated at  $V_{\rm gs}=-0.6$  V and  $V_{\rm ds}=3.0$  V are 19 GHz and 58 GHz, respectively.

Power performance of the HEMT's was measured at 900 MHz with a drain bias of 3.0 V. The device was operated under the class AB condition with a bias drain current of 0.3 A. The power characteristics were measured by a power tuning system, in which the input and output tuners with variable capacitors and inductors were used to provide the conjugate matched input and load impedances for the optimum power performance. The 5 mm-wide device exhibits an output power over 1 W, corresponding to a power density over 200 mW/mm. This is the highest power density ever achieved with power devices at such a low operation voltage. The power-added efficiency of 64% and the linear gain of 18.2 dB were obtained

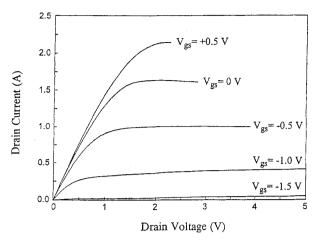


Fig. 2. Typical current-voltage characteristics of 5 mm-wide dual- $\delta$ -doped power HEMT.

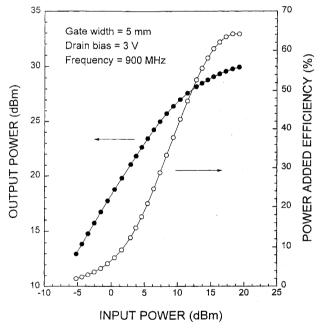


Fig. 3. Output power and power-added efficiency as a function of input power for 5 mm-wide dual- $\delta$ -doped AlGaAs/InGaAs/GaAs power HEMT at 900 MHz and drain bias of 3.0 V.

at 900 MHz. The output power and power-added efficiency as a function of the input power are depicted in Fig. 3. The most significant results in this work is that the high performance of the output power, the power-added efficiency, and the linear gain is achieved by the small gate periphery. This feature leads to high yield, low cost, and easy impedance matching.

The load-pull measurement of the 5 mm HEMT at 900 MHz was accomplished by the power tuning system and the automatic network analyzer. The load impedance associated with the optimum power performance at a drain bias of 3.0 V is  $Z_L=7.82-j2.4$  ohms ( $\Gamma_L=0.731\ \angle-173.62^\circ$ ). This load-pull data can be used to build up a power module for low voltage wireless communication applications.

The developed high-power-density dual- $\delta$ -doped Al-GaAs/InGaAs/GaAs HEMT demonstrated good potential for the applications of analog cellular phone systems, such as AMPS (Advanced Mobile Phone Service), ETACS (Enhanced Total Access Communication System), etc. The HEMT can be applied to the output stage of the analog cellular phone power module, in which the device operates at the class AB condition to supply high output power in the active mode and maintain low power consumption in the standby mode.

# IV. CONCLUSION

A high-power-density dual- $\delta$ -doped AlGaAs/InGaAs/GaAs HEMT has been developed. A 5.0 mm gate-width device operating at a drain bias of 3.0 V supplies over 1 W output power at 900 MHz. The 1  $\mu$ m gate-length HEMT exhibited a current density of 425 mA/mm (at  $V_{\rm GS}=0.5$  V), a maximum transconductance of 270 mS/mm. The effective knee voltage was as low as 0.3 V. At 900 MHz, the HEMT demonstrated an output power density of 200 mW/mm, a power-added efficiency of 64% and linear gain of 18.2 dB. These outstanding performance was due to the high current density and high electron mobility of the dual- $\delta$ -doped HEMT device. This is the highest power density reported for 3 V L-band wireless applications. The high output power achieved by small gate periphery leads to high yield, low cost, and easy impedance

matching. The optimized dual- $\delta$ -doped AlGaAs/InGaAs/GaAs structure demonstrates excellent power performance and is a potential candidate for low voltage wireless communication applications.

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