

Article

An Investigation of Carbon-Doping-Induced Current Collapse in GaN-on-Si High Electron Mobility Transistors

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Abstract: This paper reports the successful fabrication of a GaN-on-Si high electron mobility transistor (HEMT) with a 1702 V breakdown voltage (BV) and low current collapse. The strain and threading dislocation density were well-controlled by 100 pairs of AlN/GaN superlattice buffer layers. Relative to the carbon-doped GaN spacer layer, we grew the AlGaIn back barrier layer at a high temperature, resulting in a low carbon-doping concentration. The high-bandgap AlGaIn provided an effective barrier for blocking leakage from the channel to substrate, leading to a BV comparable to the ordinary carbon-doped GaN HEMTs. In addition, the AlGaIn back barrier showed a low dispersion of transiently pulsed I_D under substrate bias, implying that the buffer traps were effectively suppressed. Therefore, we obtained a low-dynamic on-resistance with this AlGaIn back barrier. These two approaches of high BV with low current collapse improved the device performance, yielding a device that is reliable in power device applications.

Keywords: GaN; high electron mobility transistor (HEMT); current collapse

1. Introduction

Gallium nitride (GaN) has attracted considerable attention in power transistor applications because its physical properties theoretically enable superior performance compared with silicon-based power transistors (e.g., Si-based LD-MOSFET), according to the high breakdown voltage (BV) and remarkably low on-state resistance (R_{on}) [1,2]. Obtaining high-quality GaN epilayers on substrates at a reasonable price has been an ongoing challenge. The GaN-on-Si high electron mobility transistors (HEMTs) are available at a relatively low cost and can be used with conventional integrated circuit process tools for fabricating GaN-on-Si power devices. However, devices with low-resistivity substrates tend to leak current from the channel to substrate, resulting in a reduction of BV [3]. The vertical

leakage of GaN-on-Si HEMTs may be effectively eliminated by reducing the density of threading dislocations (TDs) in the GaN epilayers [4] or by increasing the resistivity of the buffer layers [3]. Several high-resistivity buffer layer approaches have been reported, such as thickening the GaN buffer layer [5], removing the substrate [6], using a silicon-on-insulator (SOI) substrate [7], and using high-resistivity carbon-doped buffer layers [8]. Carbon-doped semi-insulating (SI) GaN buffer layers can be obtained by using tetrabromomethane (CBr_4) precursors [9] or by manipulating the growth pressure, V/III ratio, and growth temperature in metal-organic chemical vapor deposition (MOCVD) [10]. A carbon-doped SI GaN buffer layer can enhance the BV for power-switching and microwave applications [11]. However, some previous studies [12,13] have verified that the virtual gate associated with surface traps acts as the dominant mechanism causing current collapse (CC) in AlGaIn/GaN HEMTs. Carbon-doped SI GaN shows poor epitaxial quality because of its low growth temperature and growth pressure [14], which are responsible for the CC through charge trapping in deep levels of the SI buffer layers [15,16]. In general, the deep acceptor traps and deep donor traps coordinate in the GaN buffer layers; this coordination is accompanied by charging/discharging interactions when a high electric field is applied [12,17]. Such interactions are associated with a reduction in BV and correlated inversely with the drain current [12,17]. The CC phenomenon causes devices to perform with low reliability, particularly in power-switching applications. Therefore, overcoming CC problems through reducing the buffer trap density and TDs is essential.

In this paper, we report the growth conditions of carbon-doped GaN spacer layers through CBr_4 precursor doping. Furthermore, carbon-doping-related CC was investigated and discussed in the context of optimizing a GaN-on-Si HEMT to achieve reliable performance, a high BV, and a low CC. The GaN-on-Si HEMT with a low-carbon-doped AlGaIn back barrier shows a comparable BV to that of regular devices, but its CC can be minimized or eliminated.

2. Experimental Section

The epitaxial structure of this HEMT was grown on a 6-inch Si(111) substrate by using the MOCVD system. The buffer layer comprised a 100-nm-thick AlN cladding layer, followed by 100 periods of carbon-doped AlN/GaN (4.5-/20-nm-thick) superlattices (SLs). After the buffer layer was completed, a 1.3- μm -thick GaN spacer layer, 300-nm-thick undoped GaN channel layer, 25-nm-thick $\text{Al}_{0.27}\text{Ga}_{0.73}\text{N}$ barrier layer, and 2-nm-thick undoped GaN capping layer were grown. An unintentionally doped (UID) GaN spacer layer for the Reference sample was grown at 1130 °C. Two intentionally doped GaN spacer layers were grown, one at 1050 °C for Sample A and the other at 1130 °C for Sample B, respectively. The growth temperature of Sample A was relatively low because the CBr_4 precursor requires a low temperature to incorporate carbon into GaN. Furthermore, a 1- μm -thick low-carbon-doped $\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ back barrier layer for Sample C was grown on the top of the SL structure as an alternative spacer design for low CC. The growth pressures of the cladding layer, spacer layer, and barrier layer were fixed in the range from 75 to 100 Torr (10 to 13 kPa). A high-purity GaN channel layer was grown at 1130 °C and 680 Torr (90 kPa). The growth parameters, namely the growth temperature, growth pressure, and growth rate, are listed in Table 1.

Following the epitaxial growth, fabrication of the HEMT device began with mesa isolation through inductively coupled plasma reactive ion etching (ICP-RIE). The ohmic contacts of the source/drain electrodes were fabricated through photolithography and a lift-off process. A stacking metal system of Ti/Al/Ni/Au (20/120/25/100 nm) was evaporated through electron beam evaporation. After the stacking metal deposition, thermal annealing was employed at 850 °C to form the ohmic contact. The contact resistance of the source/drain electrodes was estimated to be $8.3 \times 10^{-5} \Omega\text{-cm}^2$ (according to transmission line model measurements). A $\text{SiN}_x/\text{SiO}_2$ (20/280 nm) passivation structure was then deposited through plasma-enhanced chemical vapor deposition (PECVD). A stacking metal system of Ni/Au (50/300 nm) was evaporated through electron beam evaporation to serve as the Schottky gate metal. The HEMT device was realized with a 2- μm gate length (L_G), 5- μm source-to-gate distance (L_{SG}), 5 to 20- μm gate-to-drain distance (L_{GD}), and 500- μm gate width (W_G), as presented in Figure 1.

In addition, a two-terminal buffer layer BV test structure was fabricated on this HEMT structure, the source and drain electrodes of which were isolated by 150-nm-deep dry etching. The L_{SD} values were defined as 5, 10, 15, and 20 μm .

Table 1. Growth parameters of the samples grown by metal-organic chemical vapor deposition (MOCVD).

	Layer	Growth Temperature ($^{\circ}\text{C}$)	Pressure (Torr)	Growth Rate ($\mu\text{m/h}$)
	AlN cladding layer	1050	75	0.8
	AlN/GaN SLs	1150	100	2.4
Reference sample	Unintentionally doped GaN spacer layer	1130	100	7.0
Sample A	Carbon-doped GaN spacer layer	1050	100	7.5
Sample B	Carbon-doped GaN spacer layer	1130	100	6.8
Sample C	$\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ back barrier layer	1130	100	2.0
	GaN channel layer	1130	680	6.5
	$\text{Al}_{0.27}\text{Ga}_{0.73}\text{N}$ barrier layer	1130	100	0.5

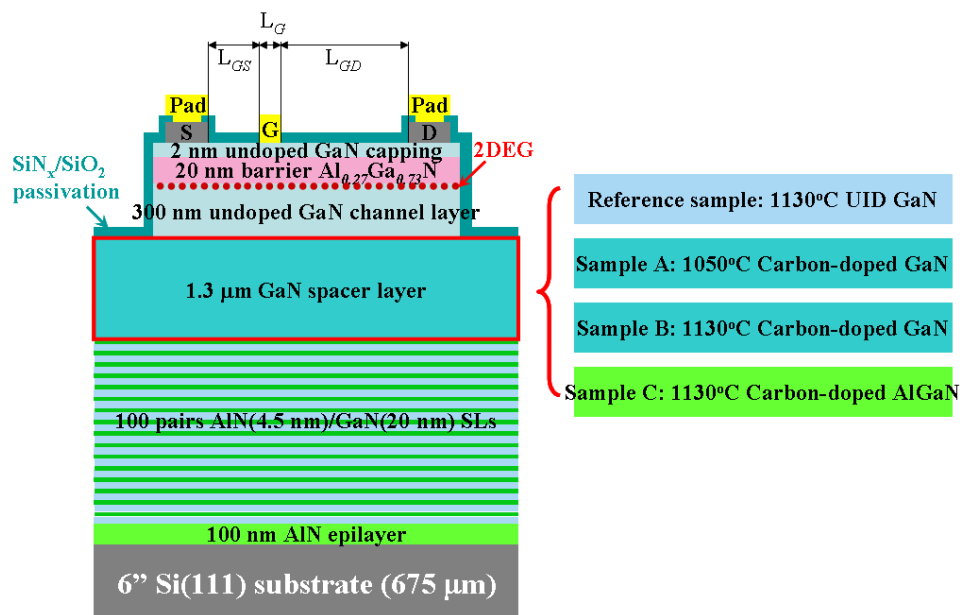


Figure 1. Cross-sectional diagram of an AlGaN/GaN HEMT. The spacer layers were fabricated at 1150 $^{\circ}\text{C}$ as UID GaN (Reference sample), at 1050 $^{\circ}\text{C}$ as carbon-doped GaN (Sample A), at 1130 $^{\circ}\text{C}$ as carbon-doped GaN (Sample B), and at 1130 $^{\circ}\text{C}$ as carbon-doped AlGaN (Sample C).

3. Results and Discussion

3.1. Strained SLs Buffer Layer of GaN-on-Si Epitaxy

Figure 2a shows bright field transmission electron microscope (TEM) cross-sectional images of the Reference sample with a UID GaN spacer layer. The figure shows TDs of extreme magnitude at the AlN/GaN SL structure. However, the threading dislocation density (TDD) gradually decreased from the carbon-doped AlN/GaN SL structure to the GaN spacer layer. To estimate the TDD, two-beam condition TEM images were captured to determine the TDD [18], as shown in Figure 2b–e. The images in Figure 2b,c were captured from the carbon-doped AlN/GaN SL region, and those in Figure 2d,e were captured from the GaN spacer layer.

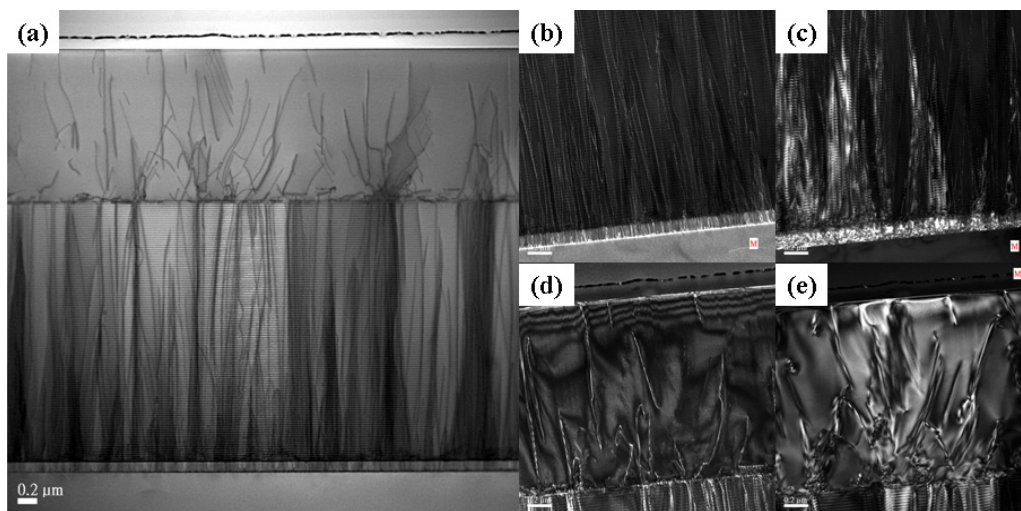


Figure 2. (a) Bright field cross-sectional TEM images with a zone axis where $g = [11-20]$; (b,c) show the TEM two-beam condition dark field images of carbon-doped AlN/GaN SLs with a zone axis, where $g = [0002]$ and $g = [1-100]$, respectively; (d,e) show the TEM two-beam condition images of the GaN spacer layer with a zone axis, where $g = [0002]$ and $g = [1-100]$, respectively.

The total number of TDDs, including edge-type, screw-type, and mixed-type dislocations, were estimated to be higher than 10^{10} cm^{-2} at the region of the carbon-doped AlN/GaN SLs, falling to approximately $5.2 \times 10^9 \text{ cm}^{-2}$ at the region above the carbon-doped AlN/GaN SLs. The densities of the edge-type and mixed-type dislocations in the GaN spacer layer region were estimated to be 3.2×10^9 and $2.0 \times 10^9 \text{ cm}^{-2}$, respectively. The density of the screw-type TDs was estimated to be less than 10^6 cm^{-2} . The total number of TDDs in the GaN spacer layer region was approximately $5.2 \times 10^9 \text{ cm}^{-2}$. The low number of TDDs in the GaN spacer layer might be attributed to the AlN/GaN SLs controlling the stress. Masahiro Ishida *et al.* reported using SLs for stress control in GaN-on-Si epitaxial layers [19]. The total stress was discussed in terms of structural modeling, which considered lattice mismatch, misfit dislocation density, wafer curvature, and coefficient of thermal expansion. Furthermore, an SL stack composed of unreleased AlN and GaN layers with 1% strain release at each pair of SLs was demonstrated, which effectively controlled the compressive stress introduced during growth. Experiments showed that bowing and cracking can be eliminated by introducing SLs into GaN-on-Si epitaxial structures. This implies that TDs tend to release the compressive stress and that TDDs can be reduced. This design factor is crucial for strain control because a high number of TDDs will reduce the BV. Therefore, a GaN epilayer with a low number of TDDs can be grown without the necessary of a thick GaN buffer layer [5].

3.2. Carbon-Doping Activities in GaN Spacer Layer

First, the relationship between the carbon-doping concentration and growth temperature of the GaN spacer layer was considered. In the growth stage, the flow rates of CBr_4 and TMG were fixed to ensure that uniform amounts of carbon adatoms were incorporated into the GaN. The V/III ratio was fixed at 3000, and nitrogen was used as the carrier gas at a flow rate of 1000 sccm for the CBr_4 precursor. A secondary ion mass spectroscopy (SIMS) depth profile was employed to determine the carbon-doping concentration of GaN spacer layer. The UID carbon-doping concentration of the Reference sample was less than $5 \times 10^{17} \text{ cm}^{-3}$, implying that the GaN grown under low-pressure conditions remained at a residual carbon-doping concentration. In contrast, the carbon-doping concentration of the GaN channel layer was measured at less than $1 \times 10^{16} \text{ cm}^{-3}$, which was near the detection limit of the SIMS instrument. This implies that the higher growth pressure effectively obtained high-purity GaN, which is consistent with previous studies [20]. Furthermore, the carbon-doping concentration depended

strongly on the growth temperature. Sample A was grown with its intentionally carbon-doped GaN spacer layer at 1050 °C and had a carbon-doping concentration of $2 \times 10^{19} \text{ cm}^{-3}$, whereas Sample B was grown at 1130 °C and had a carbon-doping concentration of $1 \times 10^{18} \text{ cm}^{-3}$. This implies that doping carbon into GaN at a very high growth temperature is infeasible. In [21], D. S. Green *et al.* also found that the substrate temperature will lead to a decreasing in carbon incorporation. Their investigation found a non-linear curve between carbon doping concentration and substrate temperature, which means that more than one process is responsible for the decline of carbon incorporation into GaN at higher temperatures. So far, the mechanism is still unclear due to its lack of more detailed studies, especially in growth of carbon-doped GaN by CBr_4 through MOCVD growth. Here, the AlGaIn back barrier that was grown at a high temperature showed a low carbon-doping concentration of $2 \times 10^{18} \text{ cm}^{-3}$. We anticipated that the low-carbon-doped AlGaIn would serve as a back barrier that keeps lower carbon-induced traps but blocks electron leakage with its high bandgap. Table 2 summarizes the structural characteristics of the samples with different carbon-doping concentrations in the spacer layers. The Hall measurements of the specimens were also investigated and shown in Table 2. The results of the Reference sample, Sample A, and Sample B yielded an electron mobility of $1315 \pm 25 \text{ cm}^2/\text{V}\cdot\text{s}$ and a sheet resistance of $414.2 \pm 10.7 \text{ }\Omega/\text{sq}$. The 2DEG concentration of Sample C is $1.07 \pm 0.02 \times 10^{13} \text{ cm}^{-2}$, which is lower than the value of our conventional HEMTs with GaN spacer. The lower 2DEG density is due to GaN channels potential being pulled up by the AlGaIn spacer, which is similar to a previous report [22]. The raised potential also leads to a positive shift of threshold voltage, which will be discussed later in this paper. X-ray diffraction (XRD) results show that the full width at half maximum (FWHM) gradually increased with the carbon-doping concentration. This feature was attributed to higher carbon-doping concentrations requiring lower growth temperatures. The results indicate that the growth temperature exerts a remarkable effect on the crystalline quality of GaN. Moreover, the higher lattice mismatch between GaN and the AlGaIn back barrier leads to a higher strain, which caused Sample C to return an unusually broad FWHM. An AlGaIn back barrier yielded slightly lower crystalline quality than that of a high carbon-doped GaN spacer. This result is very encouraging, because a high-quality AlGaIn epilayer could markedly alter a device's electrical performance through its carbon-doping regime, particularly by reducing the channel of substrate leakage for high-power HEMT devices.

Table 2. Summary of the structural characteristics of the samples.

Sample	Spacer Layer	Growth Temperature (°C)	Sheet Resistance (Ω/sq)	2DEG Concentration ($\times 10^{13} \text{ cm}^{-2}$)	Carbon-Doping Concentration (cm^{-3})	XRD fwhm (arc sec)	
						(002)	(102)
Reference sample	Unintentionally doped GaN spacer layer	1130	414.2 ± 10.7	1.16 ± 0.02	5×10^{17}	736	910
Sample A	Carbon-doped GaN spacer layer	1050	414.2 ± 10.7	1.16 ± 0.02	2×10^{19}	929	1130
Sample B	Carbon-doped GaN spacer layer	1130	414.2 ± 10.7	1.16 ± 0.02	1×10^{18}	767	943
Sample C	Carbon-doped $\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ back barrier layer	1130	447.4 ± 8.7	1.07 ± 0.02	2×10^{18}	818	1188

3.3. Breakdown Voltage Discussion

In this section, we discuss the BV improvement from the carbon-doped GaN spacer layer. The Si GaN spacer layer is responsible for blocking electron leakage punchthrough from channel to substrate when a high voltage is supplied. The two-terminal BV is defined as the supplied voltage for leakage currents up to $10 \text{ }\mu\text{A}/\text{mm}$. As shown in Figure 3a, the buffer BVs of the Reference sample and Sample B saturate at approximately 800 V when the L_{SD} is larger than $15 \text{ }\mu\text{m}$. This means that the buffer leakage is severe because these samples exhibit low resistivity of the buffer layers due to lower carbon-doping concentrations. The BV shows strong dependence on the carbon-doping concentration in the GaN

spacer layer, except for Sample C. The carbon-doping concentration of Sample C was not higher than that of Sample A, but the high bandgap of the AlGaIn back barrier blocks electron leakage to the substrate. Therefore, we could obtain a comparable BV even if a sample was grown at an excessively high temperature with inefficient carbon incorporation into the AlGaIn. This is crucial because we expected that a higher growth temperature would reduce the number of buffer traps, leading to improvements regarding the CC phenomenon. Furthermore, the buffer BV could be functionally fitted to L_{SD} , which could extract the dominant mechanism of the BV for a HEMT device. The fitting results of Sample A and Sample C suggest that the BV is proportionate to L_{SD} , because $BV \approx L_{SD}^{1.5}$ for both samples, with R^2 values of 0.99. This dependence implies that space-charge-limited (SCL) transport [23] is present in the leakage current. According to a previous study [2], SCL transport theory implies that the supplied voltage between the source and drain can be expressed as $V = \sqrt{8J/9\epsilon\mu}L_{SD}^{1.5}$, where ϵ and μ are the dielectric constant and effective carrier mobility including the trapping effect, respectively. The leakage is denoted as J . However, the SCL transport of our devices was investigated through three-terminal device measurements to confirm the presence of SCL transports in these devices.

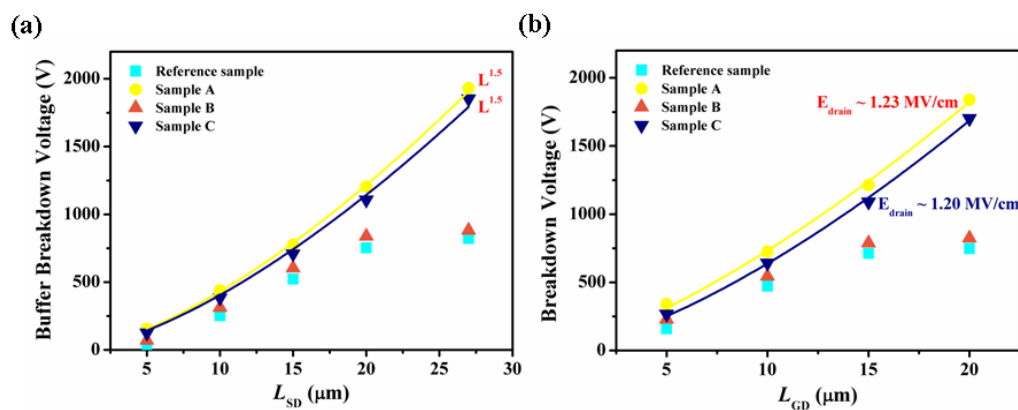


Figure 3. (a) Two-terminal buffer BV vs. L_{SD} for HEMT samples. (b) Three-terminal BV vs. L_{GD} for HEMT samples. The BV was captured for leakage currents up to 10 iA/mm with different distances between pads.

The three-terminal off-state BV was defined as V_{DS} at I_{DS} equal to 10 μ A/mm with $V_{GS} = -10$ V. Sample A, with a higher carbon-doping concentration in the spacer layer, demonstrated a high BV of 1839 V. Considering Sample A, Sample B, and the Reference sample, the BV gradually diminished as the carbon-doping concentration decreased in the spacer layer. This is consistent with our previous discussion of the two-terminal BV measurement result, which was attributed to the improvement in buffer layer isolation. Furthermore, Sample C shows a BV that is higher than 1702 V with an AlGaIn back barrier. The electric field at the Schottky gate contact is considered to explain the SCL transport model. The comparison of the BV vs. L_{GD} could be functionally fitted as $V_{DS} \sim V_{DG} = A \left[\sqrt{(2L_{GD}/A + E_{in}^2)^{1.5}} - E_{in}^3 \right] / 3$, where $A = \mu\epsilon/J = 0.00579$ to $0.00627 \mu\text{m}^3/\text{V}^2$, and E_{in} is the electric field at the gate electrode. By means of E_{in} and A , we could obtain the electric field at the drain electrode by $E_{drain} = \sqrt{2(L_{GD}/A) + E_{in}^2}$ [2]. At a 20- μ m distance, the electric fields of L_{GD} at the drain electrode are between 1.23 and 1.20 MV/cm for Sample A and Sample C, respectively. These electric fields are substantially smaller than the critical electric field of GaN, implying that the BVs of our devices are not limited by impact ionization—even the high-resistivity buffer layer was inserted [2].

3.4. HEMT Electrical Properties

The performance of the HEMT devices was characterized through an electrical analysis. Figure 4a shows the transfer characteristics of the devices. The subthreshold drain leakage current at the off-state is more than one and a half orders of magnitude lower in Sample C with the AlGaIn back barrier, as compared with the Reference sample with the UID GaN spacer. This current was attributed to the reverse bias Schottky contact of the gate, which means that the lower buffer leakage was obtained in Sample C. Sample A shows the lowest off-state subthreshold drain leakage current due to its highest carbon-doping concentration into the GaN spacer, which is consistent with the BV results. In addition, the threshold voltage was shifted from -4.62 V to -4.35 V, which is related to the lower density of 2DEG [22]. However, the hysteresis $I_{DS}-V_{GS}$ curves of the Reference sample and Sample C are shown in the inset of Figure 4a, respectively. We can observe that a larger positive shift of the hysteresis $I_{DS}-V_{GS}$ curve in the Reference sample, which implies that a higher trap density leads to the transient phenomenon in the Reference sample but we can not conclude what kind of the traps. Figure 4b shows the on-state $I_{DS}-V_{DS}$ characteristics for Sample A and Sample C. Both specimens had $L_G/L_{GD} = 2/20$ μm . At $V_{GS} = 0$ V, the $I_{DS,max}$ reached 240 and 215 mA/mm for Sample A and Sample C, respectively. From the previous results, the specific on-state resistance (*spec. R_{on}*) at $V_{GS} = 0$ V was 5.1 $\text{m}\Omega\text{-cm}^2$ for Sample A and 7.2 $\text{m}\Omega\text{-cm}^2$ for Sample C. The smaller drain current in the device with the back barrier resulted from the lower density of 2DEG and the subsequent higher threshold voltage. Therefore, the higher sheet resistance will lead to a higher on-resistance for the HEMT with the AlGaIn back barrier [24]. To investigate the relationship between the carbon-doped buffer layer and the CC phenomenon, the dynamic on-state resistance is discussed. Hot electrons can overcome the energy barrier and thereby escape from the 2DEG channel, but subsequently become trapped by defects [25,26]. Such defects come not only from surface states, but also from intrinsic defects (e.g., TDs, V_N). Trapping electrons on the surface would deplete the channel carrier concentration, resulting in a virtual gate as well as a reduction in the drain current [27,28]. Although the trapping at the surface or inside the AlGaIn barrier layer is crucial to CC, the electrons trapped in the GaN buffer by charging/discharging from deep traps are also responsible for CC. As shown in Figure 4c,d, the CC phenomenon was clearly observed in both Sample A and Sample C. Pulsed $I_{DS}-V_{DS}$ characteristics were extracted from the off-state with a quiescent gate bias (V_{GSQ}) of -5 V to an on-state at 0 V in 500 ns and a separation of 1 ms. The quiescent drain bias (V_{DSQ}) was swept from 0 to 40 V (in 10 V increments). The dynamic on-resistance of Sample A increased from 5.1 $\text{m}\Omega\text{-cm}^2$ to 12.68 $\text{m}\Omega\text{-cm}^2$ as the V_{DSQ} was swept from 0 to 40 V. In contrast, the dynamic on-resistance of Sample C increased from 7.2 $\text{m}\Omega\text{-cm}^2$ to 14.44 $\text{m}\Omega\text{-cm}^2$. The dispersion of dynamic on-resistance for Sample A is 2.48 times that for the static state but 2.00 times that for Sample C, a smaller dispersion between $V_{DSQ} = 0$ to 40 V was obtained from Sample C. Both Sample A and Sample C were passivated by the same $\text{SiN}_x/\text{SiO}_2$ ($20/280$ nm) layers; hence, the surface trap-induced CC was improved and the dynamic on-resistance was in the same situation. Here, the dynamic on-resistances show different dispersions, implying that another cause led to CC. Therefore, the pulsed $I_{DS}-V_{DS}$ characteristic cannot clearly identify the location of traps in HEMT structures because the electrons are trapped not only by buffer traps, but also by surface traps under relatively high stress [28]. Therefore, we require another measurement to investigate the location of the traps.

Because it is difficult to verify whether CC has been induced by surface traps or buffer layers, pulsed I_D transients were captured for Sample A and Sample C. Figure 5 shows CC recovery *versus* device conductance as a function of stress time. The measurement started with the device in the off-state at $V_{GS} = -5$ V and a V_{DS} of 50 V; the device was left in the off-state for 1000 s, after which the HEMT was pulsed back to the on-state (linear region) of $V_{GS} = 0$ V, $V_{DS} = 1$ V for 10 ms; measurements were performed of the drain current and I_D as functions of time (1000 s). Sample C showed a relatively small change compared with Sample A, which was consistent with dynamic on-resistance measurements. The results imply that there were traps in these HEMT structures, but the information was insufficient for clearly identifying the trap locations. Next, a V_{SUB} of -200 V was supplied, and pulsed I_D transient

currents were recorded, as shown in Figure 5 (dashed lines). The substrate bias provided an electric field and then attracted electrons from the channels to the buffer traps. The pulsed I_D transient current with substrate bias is a favorable analysis method for identifying buffer traps, but it also shows the differences between two kinds of specimens [29]. The larger dispersion of I_D transient current for Sample A implies that the buffer trap-induced CC will lead to a gradual change in the I_D transient current [12,28,29]; that slow change is related to all defects associated with the low-temperature growth of carbon-doped GaN spacer layers. In contrast, a low-carbon-doped AlGaN back barrier was grown at a higher temperature, leading to fewer traps and obtaining low dispersion in the I_D transient current under substrate bias. This result implies that the buffer traps affecting the CC behaviors of GaN-on-Si HEMTs may result from incorporating carbon into GaN to isolate the channel from substrate leakage at high electric fields.

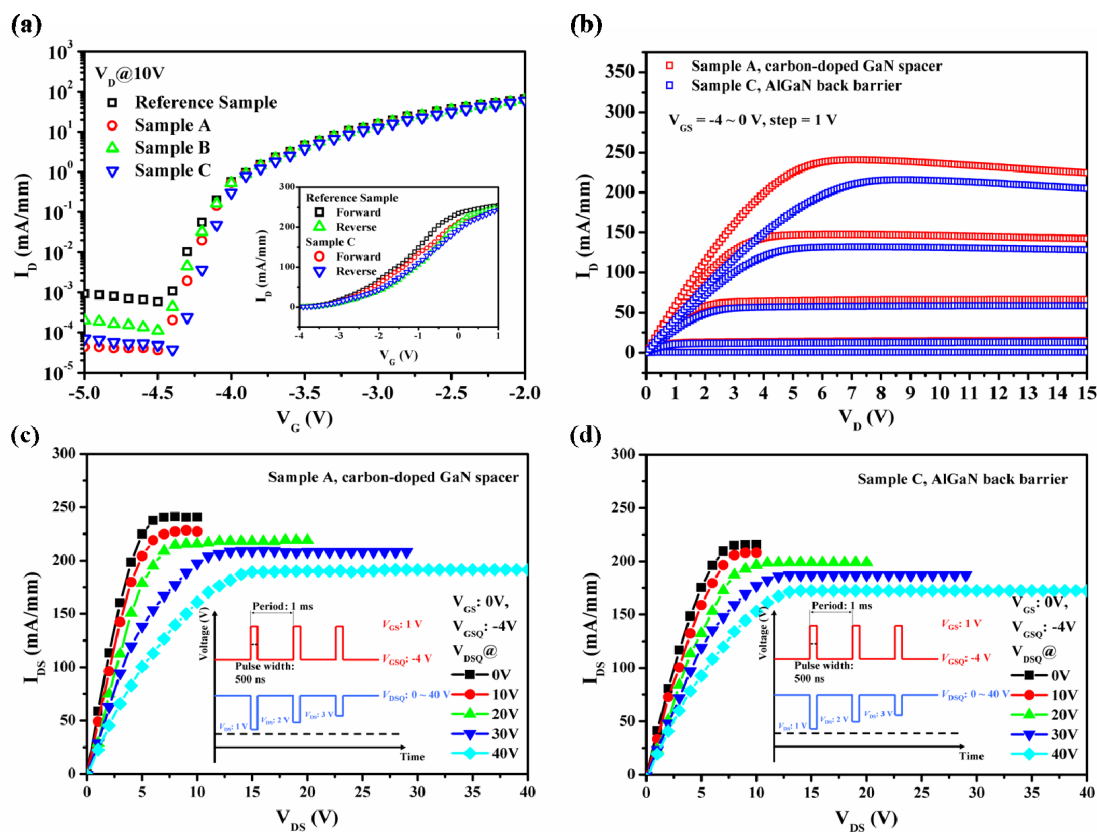


Figure 4. (a) DC I_{DS} – V_{GS} characteristics for all specimens. The hysteresis I_{DS} – V_{GS} curves for the Reference sample and Sample C are shown in the inset. (b) DC I_{DS} – V_{DS} characteristics for Sample A and Sample C. Pulsed I_{DS} – V_{DS} characteristics for (c) Sample A and (d) Sample C. Pulsed I_{DS} – V_{DS} characteristics were extracted from a quiescent gate bias (V_{GSQ}) of -5 V to an on-state at 0 V in 500 ns and a separation of 1 ms. Afterward, the quiescent drain bias (V_{DSQ}) was swept from 0 to 40 V (in 10-V increments).

Poor crystal quality is the most critical drawback of GaN-on-Si HEMTs. Heterostructures grown on Si substrates contain very high numbers of TDs and produce defects because of the high lattice mismatch. Those defects act as deep traps on the GaN surface or in the buffer layers. Some unexpected effects, such as the vertical leakage, reduction in BV, and CC, are strongly presumed to be related to those defects [30,31]. Electrons captured in or escaping from those traps result in destructive phenomena because of the charging/discharging activities in those traps. In this research, a low-carbon-doped AlGaN back barrier was employed to instead of a high-carbon-doped GaN spacer layer. The results show that the BV for an HEMT with an AlGaN back barrier is comparable to

that for a device with a conventional carbon-doped GaN spacer layer. Although the carbon-doping concentration of the AlGaIn back barrier was less than that of a carbon-doped GaN spacer layer, the higher bandgap of AlGaIn provides an effective barrier for blocking current leakage from the channel to the substrate. The most crucial point is that an AlGaIn back barrier that has been grown at a high temperature shows a lower dispersion of pulsed I_D transient current under substrate bias, which means that the buffer traps are effectively suppressed. Therefore, we obtained a lower dynamic on-resistance by using AlGaIn back barriers in the HEMTs. These two approaches improve device performance and provide an effective and easy means for preventing undesirable phenomena and producing reliable devices for high-power applications.

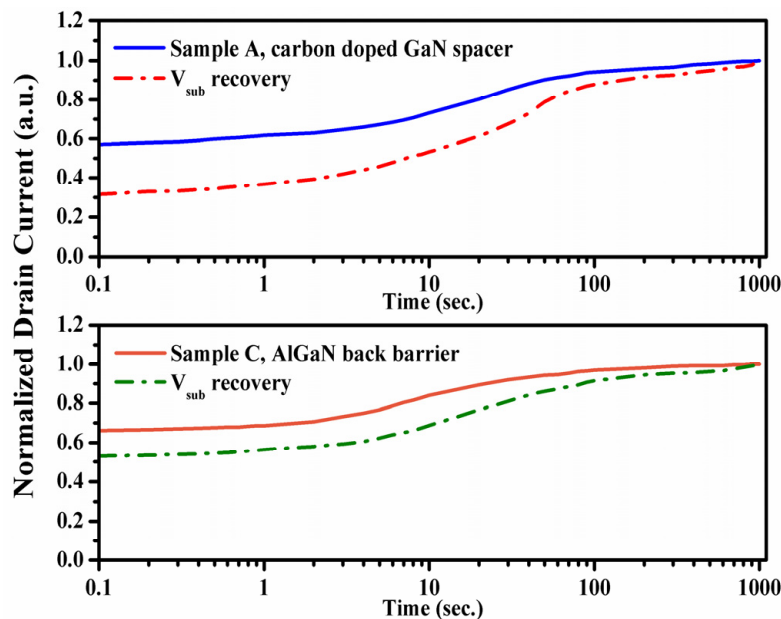


Figure 5. Normalized current recovery of device conductance as a function of time. The solid lines show the pulsed I_D transient currents. The dashed lines show conductance recovery after supplying a substrate bias of $V_{SUB} = -200$ V.

4. Conclusions

We demonstrated the structural design of a GaN-on-Si HEMT with a high BV and low CC. The structural analysis shows that the strain and TDD were well-controlled through AlN/GaN SLs. An alternative AlGaIn back barrier was grown at a high temperature and with a low carbon-doping concentration but with high crystal quality. The BV of the GaN-on-Si HEMT with the AlGaIn back barrier was 1702 V, which is comparable to the BV of regular HEMTs with carbon-doped GaN spacer layers. The pulsed I_D - V_D characteristics of our devices show low dynamic on-resistance, which correlated with improved crystal quality. A low dispersion of transiently pulsed I_D was observed under substrate bias, which means that the buffer traps were effectively suppressed by the AlGaIn back barrier grown at a high temperature. The two features of the AlGaIn back barrier lead to a high BV and low CC. The reported method is a very simple and effective ways for fabricating high-BV GaN-on-Si HEMTs for high-power applications.

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