

Enhanced Output Power of GaN-Based Resonance Cavity Light-Emitting Diodes With Optimized ITO Design

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Abstract—We fabricated and measured GaN-based resonant cavity light-emitting diodes with a 30 nm thick Indium tin oxide (ITO) thin film as a transparent contact layer. Four different ITO structures on p-type GaN samples were deposited by sputter and e-gun, and the corresponding device performance was compared. Each of these four samples has been annealed by its optimal parameters. The ITO thin film deposited by sputter demonstrated better electrical characteristics, surface morphology, specific contact resistance, and the overall device light output compared to those of the e-gun samples. Between the two sputtered ITO types, the hybrid type shows higher roll-over current density of 14 kA/cm², and the output power is increased from 15 to 39 μW. From statistical data of the 2-D light intensity under the same current, we saw the lateral current spreading of the pure crystalline ITO by sputter is worst. The hybrid type, which combines the crystalline and amorphous ITO, has the best overall performance when we consider all the electrical, optical, and metrology measurements. From these results, we believe the 30 nm thick hybrid ITO thin film has the best potential to be applied in light emitting devices such as light-emitting diodes, laser diodes, etc.

Index Terms—Current spreading, GaN, indium tin oxide (ITO), resonance cavity light-emitting diodes (RCLEDs).

I. INTRODUCTION

GALLIUM NITRIDE (GaN) is an attractive material due to its wide bandgap and its emission in blue-green wavelength which can be applied extensively in the optoelectronic devices including light emitting diodes (LEDs) and laser diodes

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(LDs) [1]–[3]. To fabricate highly efficient optoelectronic devices, electrical contacts to GaN layers (n-type or p-type) play important roles. There are many methods to improve electrical characteristics of the GaN-based devices, such as choices of metal for a stable ohmic contact, a better current spreading layer design, and better epitaxial quality.

However, due to low doping density resulted from high activation energy of the p-type dopant, the electrical conductance of p-GaN contact is worse than that of n-type GaN. Therefore, it is important to find a better conductive layer on p-GaN for current spreading. This layer should not only form good ohmic contacts to p-GaN, but also have higher transparency at emission wavelength. In the past few years, Ni/Au contact was widely used in commercial GaN-based LEDs. The specific contact resistance between p-GaN and metal contact can reach 10^{-2} – 10^{-6} Ω·cm² after annealing. However, the Ni/Au layer has high absorption, and it was reported that the transmittance of Ni/Au only around 60–85% in the wavelength range from 450 to 550 nm [4]. The absorption of contact layer is particularly important for LEDs and LDs because it would decrease the output power. Nowadays, indium tin oxide (ITO) has gradually replaced the conventional metal conductive layer such as Ni/Au due to its high transparency and its low electrical resistivity ($<10^3$ Ω·cm). So far, there have been many studies about the ITO thin film for optoelectronic device application [5]–[8]. In general, ITO is a mixture material of indium oxide (In₂O₃) and tin oxide (SnO₂), and both of them have a wide bandgap (~3.5–4.3 eV) and low electrical resistivity ($2 \sim 4 \times 10^{-4}$ Ω·cm). The oxygen vacancies accompanied with the Sn donor, which are responsible for its high conductivity, but can also lead to non-stoichiometric ITO. In the optical characteristics, ITO shows high absorption in the UV region, high transmittance (~90%) in the visible region, and high reflectance in the infrared (IR) region. In addition, the ITO thin film is thermally stable and has better device reliability compared to the Au-based contact. Due to these unique properties, ITO has been used in a wide range application, such as transparent electrodes for display and solar cell [9], [10], IR reflective mirrors for building and transparent conducting layers for nitride-based devices [11], [12].

Up to now, there are many methods applied in the deposition of ITO film such as sputter, e-gun evaporation [13], chemical vapor deposition, pulsed laser deposition, etc. In previous reports [14], [15], thick ITO layer by e-gun is commonly applied in the light-emitting devices such as LEDs. Actually, these

devices have better electrical characteristics but higher optical loss. In this report, in order to obtain less optical absorption and better electrical characteristics, the ITO structures were specifically designed, both in thickness and deposition method, to explore the possibility of realizing good electrical contact property. We further measured and investigated the electrical characteristics of these ITO structures on p-GaN layer samples by circular transmission line model (CTLTM) method that can identify the lower specific contact resistance between contact layer and surface of samples by different anneal parameters [16]. From these results, we demonstrated superior optical and electrical characteristics of light emitting devices based on specific ITO design with higher roll-over current density, higher output power, and better current spreading mechanism than conventional designs.

II. EXPERIMENT

The Mg-doped p-GaN layer samples and resonance cavity light emitting diodes (RCLEDs) were grown on 2-in (0001) sapphire substrates by metal-organic chemical vapor deposition. The carrier concentration of the p-GaN material is in the range of 10^{17} cm^{-3} . Before we started to deposit the ITO thin film on the samples, the initial clean was required. Acetone (ACE) and isopropyl alcohol (IPA) were used to carry out the inorganic and organic particles on surface together with ultrasonic cleaning. Finally, these samples were rinsed in deionized water (D.I. water) 5 min to remove residual IPA solution and blow-dried with nitrogen environment (N_2).

Second, the ITO thin film was deposited on p-GaN layer samples with $1.5 \mu\text{m}$ u-doped GaN layer underneath to examine the specific contact resistance between contact layers and p-GaN layer samples by using CTLTM. Photolithography and etching process were performed to form CTLTM patterns. The CTLTM patterns after etching and removing the photoresist are shown in Fig. 1. This pattern is a series of rings with the identical inner circles and different gap spacing. These gap spacing were 5, 10, 15, 25, 35, and $45 \mu\text{m}$. The ITO layer in these gap regions was removed during etching process. Then, the samples prepared in previous process were annealed in N_2 using rapid thermal annealing (RTA) system. The annealing temperature and time are varied from 200° to 700° and from 5 to 30 min, respectively. Current-voltage (I - V) measurements were performed by using the probe station and Keithley 238 CW current Source. We could obtain the total resistance of different gap thickness from the I - V curve and calculate the specific contact resistance of different annealing conditions. By these steps, we can obtain the best annealed parameters and apply to these samples and devices.

As shown in Table I, there are four different ITO structures and each group of samples was annealed by RTA. ITO A and B were amorphous structures and evaporated by e-gun with 210 and 30 nm thickness. The thickness of ITO A is designed to match one optical wavelength 430 nm, and it is called conventional and used as a reference. The thickness of ITO B was reduced to 30 nm to avoid additional optical loss. The following two groups of these samples, ITO C and D, were deposited both by sputter with the same thickness of 30 nm. The difference between ITO C and D is the deposition temperature. ITO C was

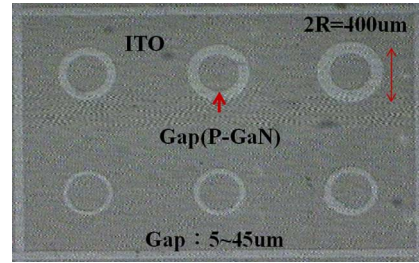


Fig. 1. CTLTM pattern on p-GaN layer sample.

TABLE I
FOUR DIFFERENT ITO STRUCTURES INCLUDING
CRYSTAL [17] AND AMORPHOUS [18]

ITO	Method	Thickness (nm)	Crystallization
A	E-gun	210	Amorphous
B	E-gun	30	Amorphous
C	Sputter	30	Crystalline
D	Sputter	30	10nm amorphous+ 20nm Crystalline

grown under high temperature, and thus, a crystalline ITO layer was formed. On the other hand, 10 nm ITO was first deposited on the substrate of ITO D at room temperature, and then it was heated up to 150°C for the rest of deposition. This two-step transformation of temperature made ITO D own both amorphous and crystalline structures.

Finally, we deposited four different ITO structures on RCLED which is consisted of $2 \mu\text{m}$ u-doped GaN layer, 29 pairs AlN/GaN distributed Bragg reflectors, 780 nm n-type GaN layer, ten-pair $\text{In}_{0.2}\text{Ga}_{0.8}\text{N}$ /GaN multiquantum wells (MQWs), 200 nm p-type GaN layer, and ten-pair $\text{SiO}_2/\text{TiO}_2$ distributed Bragg reflectors. In addition, glass and silicon wafers were utilized as reference for transmission spectrum and extinction coefficient analysis, separately.

In the following steps, we would investigate the surface morphology and sheet resistance of these ITO designs with atomic forced microscopy (AFM) and four-point probe. The n&k analyzer 1280 was also used to realize the refractive index and extinction coefficient of ITO. The RCLED devices with four different ITO contact layers were fabricated to examine the electrical and optical characteristics. The fabrication process was described as following. First, using regular lithography process, we defined the mesa region and etched deeply to the n-GaN layer by inductive coupled plasma. Second, the 200 nm SiNx film would be deposited on the sample by plasma-enhanced chemical vapor deposition as a current confinement layer. Next, the thin ITO layer was deposited as a current spreading layer. The size of current aperture was defined to be 5, 10, 15, 20, 25, and $30 \mu\text{m}$, respectively. After that, the p-contact metal of Ti/Al and n-contact of Ti/Al/Ni/Au would be deposited by e-gun evaporation. Finally, the ten-pair $\text{SiO}_2/\text{TiO}_2$ dielectric DBR was deposited on the top of the aperture by e-gun system. The structure of our devices is similar to what we reported previously

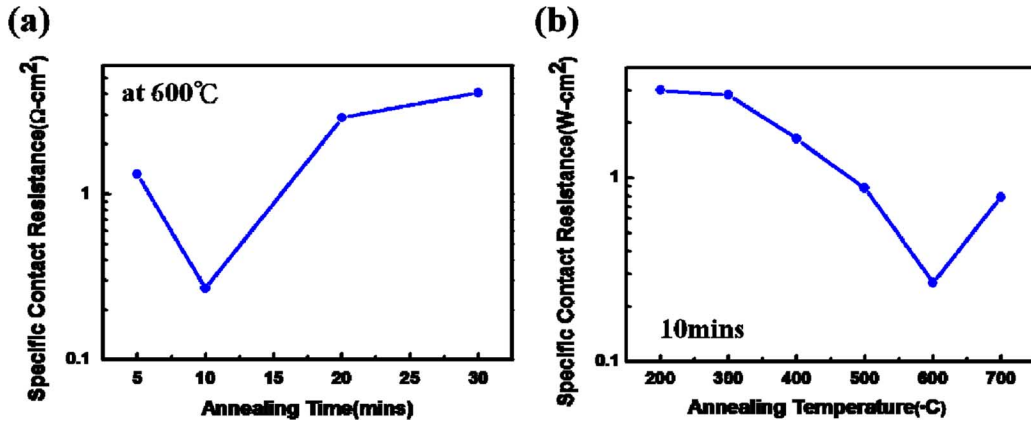


Fig. 2. Specific contact resistance for ITO on p-GaN samples deposited by sputter (a) at fixed annealing temperature of about 600 °C (b) with the same annealing time of 10 min.

[19]. The electroluminescence (EL) characteristics of our devices were measured by the probe station system at different current density. The output power could be obtained from the optical power-meter through an integrated sphere. Current–light output power ($L-I$) and current–voltage ($I-V$) measurements were also performed. In addition, these devices driven by dc current source were analyzed through the charge-coupled device and beam-view instrument. These instruments can show the optical intensity distribution of devices and capture optical intensity distribution of the measured devices. Then, the intensity distribution can be digitalized to a 2-D map of intensity for the current spreading analysis purpose.

III. RESULT AND DISCUSSION

The annealing temperature of the samples evaporated by e-gun was at 430 °C, 1 min by using RTA instrument. The annealing temperature has been optimized for ITO A and ITO B. Fig. 2(a) and (b) shows the results of CTLM measurement for ITO deposited by sputter after annealing by RTA with various parameters under N_2 environment. The annealing temperature in Fig. 2(a) was fixed at 600 °C and the annealing time used in Fig. 2(b) was 10 min. An optimized temperature and annealing time can be found out at 600 °C 10 min under N_2 environment. Therefore, we used these annealing parameters for ITO C and D samples in the following experiment.

To estimate the material absorption characteristics of ITO film, we measured the refractive index and extinction coefficient from the n&k analyzer. The wavelength dependence of refractive index and extinction coefficient for different ITO structures are shown from Fig. 3(a)–(d). The refractive index of GaN-based LEDs with 430 nm is about 2.0. From these figures, the extinction coefficient has a maximum in ultraviolet region because of the interband transition or atomic oscillation [4]. In the visible region, the extinction coefficient is nearly zero and most of light is transparent to most wavelength band. However, the value of absorption in transparent region gradually increases again as wavelength approaches infrared region beyond 800 nm. This increase is due to the vibrational absorption associated with the lattice vibration. The long wavelength absorption can be attributed to the vibrational oscillation in the Lorentz model,

which leads to some loss at this range (especially between visible and IR). The oscillation can come from the bonding between the atoms in the ITO (close to IR range) or from the electronic oscillation in the states (close to visible range). The n&k values in Fig. 3(a) and (b) have larger differences and this could be due to their different grain spacing between larger particles. In Fig. 3(c), the extinction coefficient by sputter is lower than that by e-gun due to the different deposition technology. We believe the lower deposition temperature in the sputter system can help to reduce thermal surface destruction with lower deposition temperature compared to e-gun technology. This feature can provide much better optical characteristics than e-gun technology. The AFM images are shown in Fig. 4. From the AFM results, the surface roughness was measured to be 5.2, 6.6, 0.8, and 0.4 nm with respect to ITO A, ITO B, ITO C, and ITO D, respectively. It shows the surface roughness of ITO C and D is better than ITO A and B. The thin ITO which was deposited by sputter had flatter surface than those deposited by e-gun.

Table II shows the other characteristics of ITO such as sheet resistance, resistivity, and specific contact resistance. The resistivity is calculated from the sheet resistance. The sheet resistance of ITO A is the lowest compared with 30 nm ITO contact layers due to large thickness. Both optical and electrical properties can be affected by the thickness of ITO [20], and from previous results [20], a thickness between 50 and 100 nm should be best for the external quantum efficiency. However, in our case, due to the requirement of optical loss reduction, we picked 30 nm of ITO as our final choice, and its conductivity is still in the acceptable range. This resistance is associated with lateral current spreading through the material and it generally decreases as thin film thickness increases. The decreasing of film resistivity could be due to either the increasing carrier concentration and/or Hall mobility in ITO films [21]. However, the specific contact resistance of 30 nm ITO is slightly lower than ITO A. This result reveals the specific contact resistance is not determined by thin film thickness but annealing conditions [22]. Especially, ITO B has the largest sheet resistance and resistivity. We suppose that it could be as a result of its larger vacant space between ITO particles. The results show the deposition quality of e-gun evaporation still needs to be improved when deposition thickness is thinner.

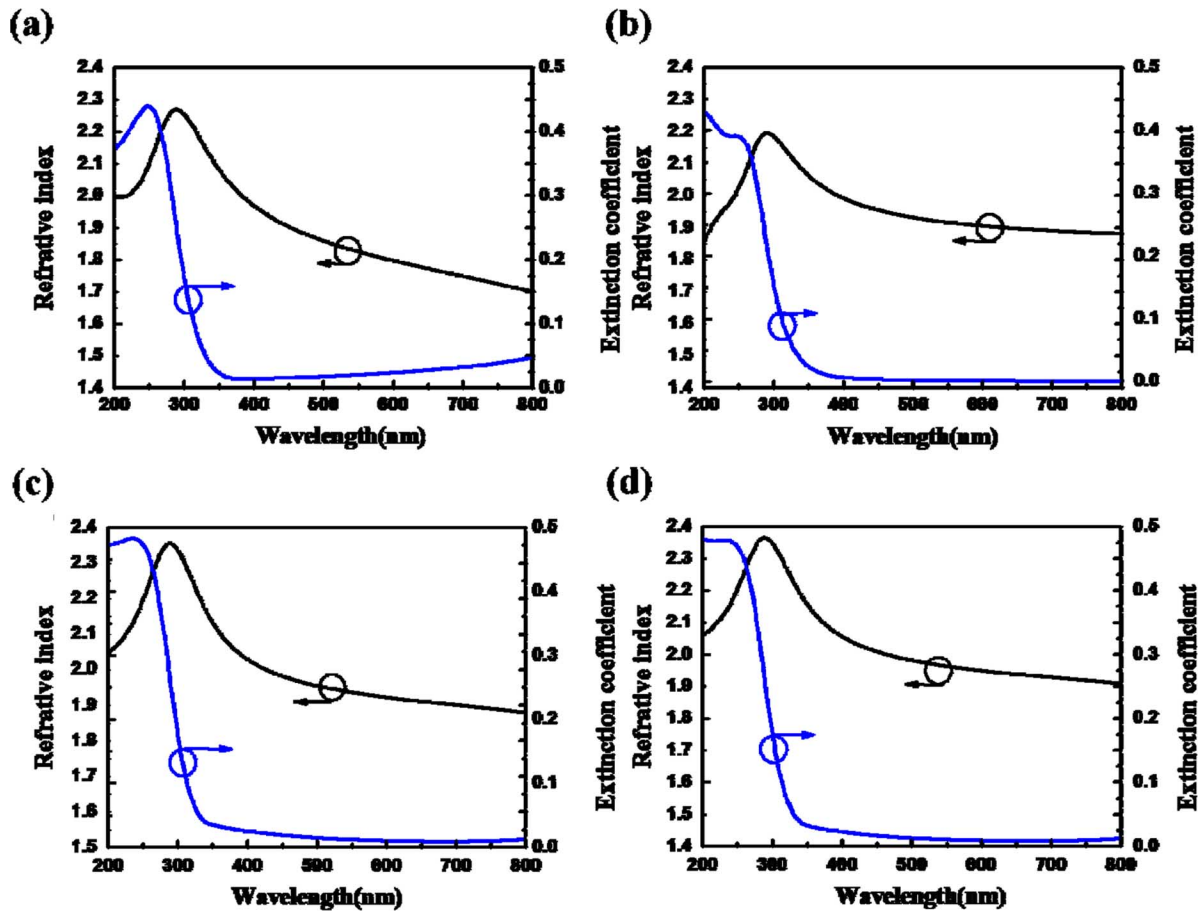


Fig. 3. Refractive index and extinction coefficient curves of (a) ITO A, (b) ITO B, (c) ITO C, and (d) ITO D, respectively.

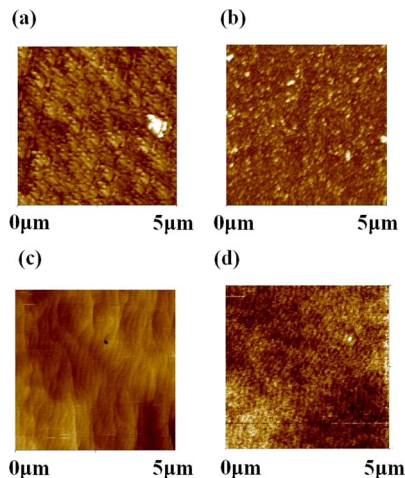


Fig. 4. AFM images of (a) ITO A, (b) ITO B, (c) ITO C, and (d) ITO D, respectively.

Then, these four different ITO structure were applied on RCLEDs and the samples are named RCLED A, RCLED B, RCLED C, and RCLED D, respectively. The performance of $L-I$ curves and $I-V$ curves was measured by the probe station and the results are shown in Fig. 5(a) and (b). From these figures, because the surplus nonrecombination carriers become thermalized in the MQW region, the devices would be damaged

TABLE II
ELECTRICAL CHARACTERISTICS OF DIFFERENT ITO STRUCTURES

ITO	Sheet resistance (Ω/\square)	Resistivity ($\Omega\text{ cm}$)	Specific contact resistance (Ωcm^2)
A	16.8	3.7×10^{-4}	0.245
B	706	2.1×10^{-3}	0.136
C	283.8	8.52×10^{-4}	0.0541
D	313	9.39×10^{-4}	0.132

and reduced the recombination efficiency due to higher junction temperature when the output power reaches a maximum value and gradually decay. In Fig. 5(a), the rollover current density of RCLED A, RCLED B, RCLED C, and RCLED D are 10.5, 12.5, 13.6, and 13.9 KA/cm^2 , respectively. These values exhibits that the effect of heat dissipation of ITO deposited by sputter is better than that by e-gun and the performance of the devices with the RCLED A structure is the worst one. This might be caused by the heat which cannot be easily dissipated from the thick ITO film. Fig. 5(b) shows the $I-V$ curve in each RCLED devices. The turn-ON voltage of RCLED D is about 3 V which is lowest in these devices. In contrast, the turn-ON

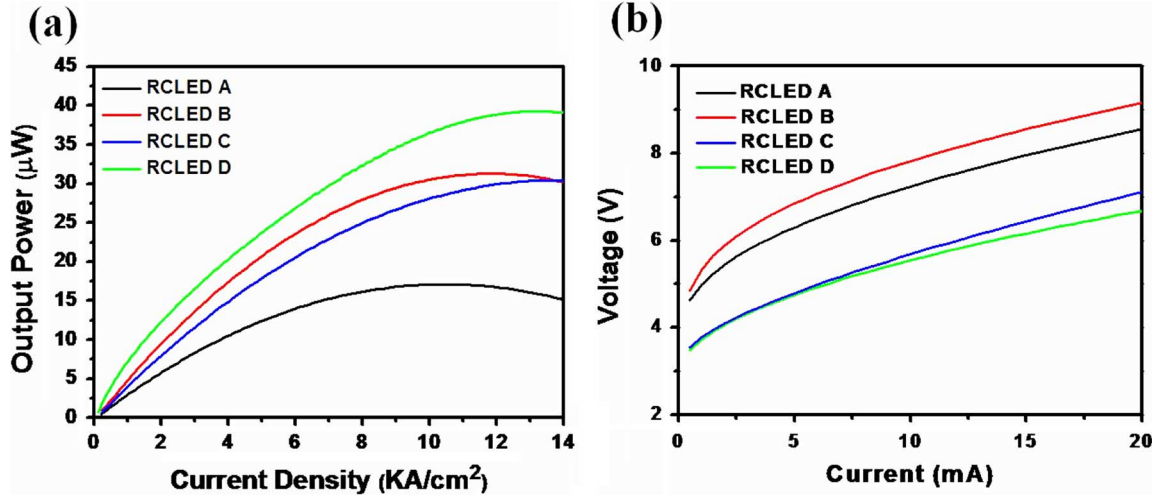


Fig. 5. (a) $L-I$ curves and (b) $I-V$ curves of different ITO layers on RCLEDs.

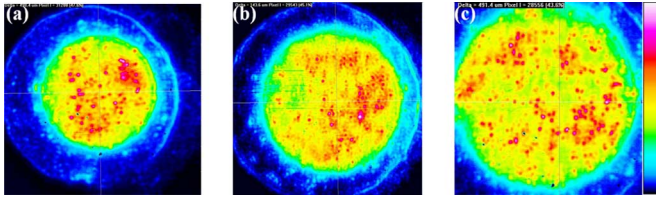


Fig. 6. Device of (a) 20 (b) 25, and (c) 30 μm aperture under same current operation.

voltage of RCLED A and RCLED B are higher than RCLED C and RCLED D. This indicates that the interface between the ITO deposited by e-gun and p-GaN is poor and might hinder the electrical conductivity. Next, we measured 50 devices with current aperture diameter of 25 μm for every deposition condition with 2-D beam intensity profiler (BeamView), and average the intensity over the radius direction. The standard deviation is calculated to be 0.1623 times of the average intensity. There are different aperture sizes of devices made in the same sample. As shown in Fig. 6, the beamview images for device of aperture size 20, 25, and 30 μm show similar result under 10 mA operation. The size of the aperture would not affect the characteristics of ITO in the range of interest. The normalized results in Fig. 7 demonstrate the different current spreading (and thus the LED output light intensity) between cases: while the sample A shows best normalized light output, the sample D is also comparable in terms of intensity uniformity. The insets in Fig. 7 show the intensity distribution of RCLED D under 10 mA current injection. In the other two cases, condition B is acceptable, but with further degradation in the light intensity, and C is not acceptable because of the obvious lack of current lateral spreading. We believe the current-crowding phenomenon and poor conductivity of RCLED C is caused by ion bombardment during the ITO deposition. When the ITO film is deposited on the sample, the p-GaN surface would be slightly damaged. On the other hand, the RCLED D shows uniform current spreading because of the predeposited 10 nm amorphous ITO film whose process is mild and can protect the p-GaN surface. From these data, we can conclude that the new design of ITO D structure

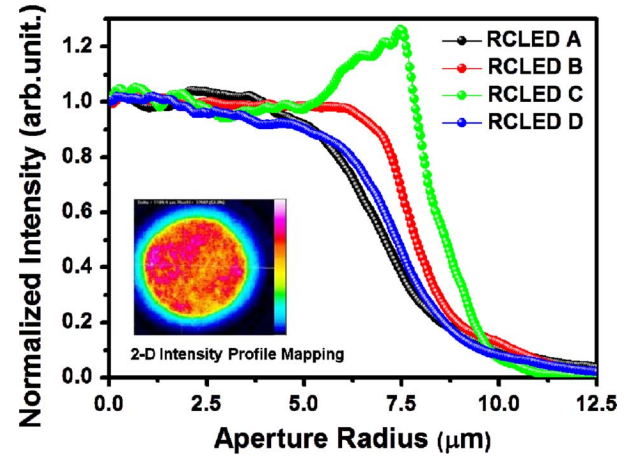


Fig. 7. Integrated intensity distribution from center to edge of the aperture corresponds to RCLEDs. The inset shows the intensity distribution image of the activated device.

can deliver a good turn-ON voltage plus comparable current spreading to the much thicker and conventional ITO (sample A).

IV. CONCLUSION

To summary, we fabricated and measured four different ITO structures deposited by e-gun and sputter on RCLEDs. By means of CTLM measurement, we can identify the sputter process condition for lower specific contact resistance between p-GaN and ITO. Furthermore, we found that ITO thin films with thickness of 30 nm had slightly lower specific contact resistance compared with samples of 210 nm ITO. In EL measurement, RCLED C and RCLED D show better performance in electric characteristics. In addition, the RCLED device using 10 nm amorphous plus 20 nm crystalline ITO especially has the highest output power (39 μW) compared with the conventional RCLED A (15 μW). The 2-D light intensity map reveals that the current spreading through the active region was more uniform and concentrated in the amorphous/crystalline ITO structure design. From these results, we believe this hybrid deposition

technology of ITO has great potential for current-injected light-emitting devices such as LEDs and LDs.

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