# Complex refractive index measurements based on Fresnel's equations and the uses of a lock-in amplifier

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### **ABSTRACT**

A new method for measuring complex refractive index is presented based on Fresnel's equations and the uses of a lock-in amplifier. A lock-in amplifier is introduced into a common path interferometer to measure the product of the amplitude reflection coefficients of s and p polarizations and their corresponding phase difference of a light beam reflected from a medium with complex refractive index. Then, these data are substituted into the special equations derived from Fresnel's equations, the complex refractive index can be obtained by numerical calculations. The resolution of this method is better than 0.01. It has both merits of a conventional common-path interferometer and a heterodyne interferometer. And its validity is demonstrated.

Keywords: complex refractive index, heterodyne interferometry,

## 1. INTRODUCTION

Complex refractive index N(n,k) is an important characteristic constant of thin film materials, where n is the refractive index and k is the extinction coefficient. There are several methods for measuring the complex refractive index of a material, e.g.,  $R - vs - \theta$  (reflectance versus incidence angle) methods<sup>1-6</sup> and ellipsometry<sup>7-8</sup>. In those methods, the reflectances of s- and p- polarizations under several different incident angles or polarization conditions must be measured. So, the measurement processes become tedions.

In this paper, a new method for measuring complex refractive index is presented based on Fresnel's equations<sup>9</sup> and the uses of a lock-in amplifier. Firstly, special equations are derived based on Fresnel's equations. From these equations, it is obvious that the product of amplitude reflection coefficients of s and p polarizations and their corresponding phase difference of a light reflected from a medium with complex refractive index are the function of complex refractive index and the incident angle. Next, a common-path heterodyne interferometer is designed for measuring their relations. The light

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source includes a He-Ne laser and an electro-optic modulator driven by a signal generator. And a lock-in amplifier is used to measure the product of the amplitude reflection coefficients and the corresponding phase difference simultaneously. Then, these data are substituted into the special equations, the complex refractive index can be obtained by numerical calculations. The resolution of this method is better than 0.01. It has both merits of a conventional common-path interferometer and a heterodyne interferometer. And its validity is demonstrated.

## 2. PRINCIPLE

## 2.1 Amplitude reflection coefficients for an absorption material

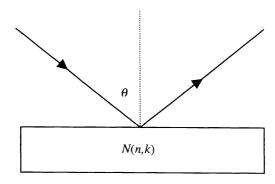


Fig.1 Reflection at the surface of an absoption material.

A ray of light in air is incident at  $\theta$  on an absorption material with a complex refractive index N(n,k), as shown in Fig.1. According to Fresnel's equations<sup>9</sup>, the amplitude reflection coefficients of s and p polarizations can be expressed as

$$r_{s} = \frac{\cos\theta - (u + iv)}{\cos\theta + (u + iv)} = |r_{s}| \exp(i\delta_{s}), \tag{1}$$

$$r_{p} = \frac{N^{2} \cos \theta - (u + iv)}{N^{2} \cos \theta + (u + iv)} = \left| r_{p} \right| \exp(i\delta_{p}), \tag{2}$$

respectively, where

$$u^{2} = \frac{1}{2} \left\{ \left( n^{2} - k^{2} - \sin^{2}\theta \right) + \left[ \left( n^{2} - k^{2} - \sin^{2}\theta \right)^{2} + 4n^{2}k^{2} \right]^{\frac{1}{2}} \right\}, \tag{3}$$

$$v^{2} = \frac{1}{2} \left\{ -\left(n^{2} - k^{2} - \sin^{2}\theta\right) + \left[\left(n^{2} - k^{2} - \sin^{2}\theta\right)^{2} + 4n^{2}k^{2}\right]^{\frac{1}{2}} \right\},\tag{4}$$

 $\delta_s$  and  $\delta_p$  are the phase shifts of s and p polarizations, and can be expressed as

$$\delta_s = \tan^{-1} \left( \frac{2v \cos \theta}{u^2 + v^2 - \cos^2 \theta} \right), \tag{5}$$

$$\delta_{p} = \tan^{-1} \left[ \frac{2v \cos \theta \left[ n^{2} - k^{2} - 2u^{2} \right]}{u^{2} + v^{2} - \left( n^{2} + k^{2} \right)^{2} \cos^{2} \theta} \right], \tag{6}$$

respectively. Hence, the phase difference of s polarization relative to p polarization is

$$\phi = \delta_s - \delta_p = \tan^{-1} \left( \frac{ad - bc}{ac + bd} \right), \tag{7}$$

where

$$a = 2v \cos \theta,$$

$$b = u^{2} + v^{2} - \cos^{2} \theta,$$

$$c = 2v \cos \theta (n^{2} - k^{2} - 2u^{2}),$$

$$d = u^{2} + v^{2} - (n^{2} + k^{2})^{2} \cos^{2} \theta.$$
(8)

From Eqs.(1) ~ (8), it is obvious that the product  $|r_s||r_p|$  and phase difference  $\phi$  are the functions of n, k, and  $\theta$ . If  $|r_s||r_p|$  and  $\phi$  can be experimentally measured for a given  $\theta$ , then the complex refractive index of the medium can be estimated by solving the following set of simultaneous equations

$$V = V(n, k, \theta), \tag{9}$$

$$\phi = \phi(n, k, \theta), \tag{10}$$

where  $V = |r_s| r_p$ .

# 2.2 Product of amplitude reflection coefficients and phase difference measurements with heterodyne interferometry

Chiu et al. <sup>10</sup> had proposed a method for measuring the refractive index of a transparent material by using the total internal reflection heterodyne interferometry (TIRHI). The schematic diagram of the optical arrangement of our method,

which is based on similar considerations, is designed and shown in Fig.2(a). The linearly polarized light passing through an electro-optic modulator EO is incident on a beam splitter BS and divided into two parts: the reference beam and the test beam. The reference beam passes through an analyzer  $AN_r$ , and enters the photodetector  $D_r$ . If the amplitude of light detected by  $D_r$  is  $E_r$ , then the intensity measured by  $D_r$  is  $I_r = |E_r|^2$ . Here  $I_r$  is the reference signal. On the other hand, the test beam is incident at  $\theta$  on a test material. Finally, the reflected light passes through an analyzer  $AN_r$ , and is detected by another photodetector  $D_r$ . If the amplitude of the test beam detected by  $D_r$  is  $E_r$ , then  $D_r$  measures the intensity  $I_t = |E_t|^2$ . And  $I_t$  is the test signal.

For convenience the +z axis is in the propagation direction and the y axis is in the vertical direction. Let the incident light be linearly polarized at  $45^{\circ}$  with respect to the x axis, the fast axis of EO under an applied electric field be in the horizontal direction, and both the transmission axes of  $AN_r$  and  $AN_t$  be at  $45^{\circ}$  with respect to the x axis. If a sawtooth signal of a frequency f and an amplitude  $V_{\lambda/2}$ , the half-wave voltage of the EO, is applied to the electro-optic modulator, then by using the Jones calculus we can get 11,12

$$I_r = \frac{1}{2} [1 + \cos(2\pi f t - \phi_{BS})], \tag{11}$$

$$I_{t} = \frac{1}{2} \left[ \frac{\left| r_{s} \right|^{2}}{2} + \frac{\left| r_{p} \right|^{2}}{2} + \left| r_{s} \right| \left| r_{p} \right| \cos(2\pi f - \phi) \right], \tag{12}$$

where  $\phi_{BS}$  is the phase difference between s and p polarizations due to the reflection at BS. These two sinusoidal signals are sent to a lock-in amplifier, the product of  $|r_s||r_p|$  and their phase difference

$$\phi' = \phi - \phi_{RS} \,, \tag{13}$$

can be obtained. Next, let the test beam enter the photodetector  $D_t$  directly without the reflection from the test material, as shown in Fig.2(b). The test signal still has the form of Eq.(12), but this time with  $\phi = 0$ . Therefore the phase meter in Fig.2(b) represents  $-\phi_{BS}$ . Substituting  $-\phi_{BS}$  into Eq.(13), we can obtain the phase difference  $\phi$ .

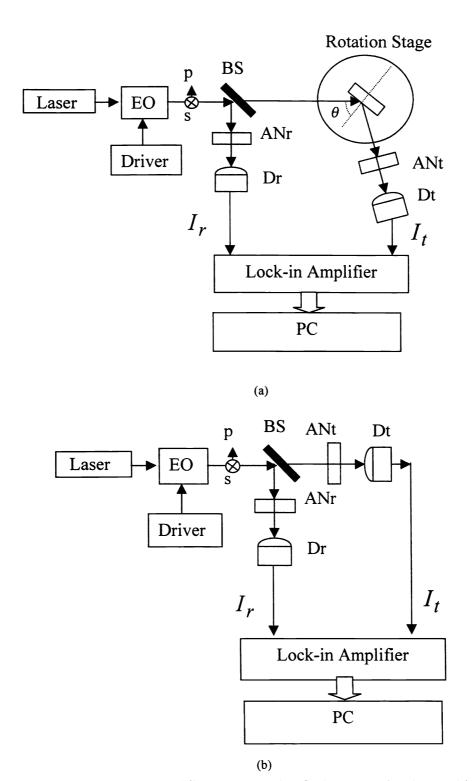


Fig.2 Schematic diagram for measuring the phase differences owing to the reflection at (a) an absorption material, and (b) BS.EO: electro-optic modulator; BS: beam-splitter; AN: analyzer; D: photodetector;  $I_i$ : reference signal;  $I_i$ : test signal; PC: personal computer.

### 3. EXPERIMENTS AND RESULTS

To show the feasibility of this technique, the complex refractive index of nickel (Ni) was measured. A He-Ne laser with 632.8nm wavelength and an electro-optic modulator (Model PC200/2, manufactured by England Electro-Optics Developments Ltd.) with a half-wave voltage 170V were used in this test. The frequency of the sawtooth signal which was applied to the electro-optic modulator was 800 Hz. A high precision rotation stage ( $PS - \theta - 90$ ) with angular resolution of  $0.005^{\circ}$  manufactured by Japan Chuo Precision Industrial Company Ltd. was used to mount and rotate the test material. And a high-resolution lock-in amplifier was used to measure the product of  $|r_s||r_p|$  and the phase difference  $\phi$ . In addition, a personal computer was used to record and analyze the data. The experimental conditions and results are summarized in Table 1. The average experimental value of the complex refractive indices of Ni is N(Ni) = 1.98 + i3.76.

## 4. DISCUSSIONS

From Eqs.(8) and (9), we can get

$$\Delta n \approx \frac{\left|\frac{\partial \phi}{\partial k}\right| \Delta V + \left|\frac{\partial V}{\partial k}\right| \Delta \phi}{\left|\frac{\partial V}{\partial n} \frac{\partial \phi}{\partial k} - \frac{\partial \phi}{\partial n} \frac{\partial V}{\partial k}\right|},\tag{14}$$

and

$$\Delta k \approx \frac{\left|\frac{\partial \phi}{\partial n} \middle| \Delta V \middle| + \left|\frac{\partial V}{\partial n} \middle| \Delta \phi \middle|}{\left|\frac{\partial V}{\partial n} \frac{\partial \phi}{\partial k} - \frac{\partial \phi}{\partial n} \frac{\partial V}{\partial k}\right|},\tag{15}$$

where  $\Delta n$  and  $\Delta k$  are the errors in n and k, and  $\Delta V$  and  $\Delta \phi$  are the errors of the product of  $|r_s||r_p|$  and the phase difference  $\phi$ , respectively. The errors of phase differences include the angular resolution of a lock-in amplifier, the second harmonic error of the product of the phase differences include the angular resolution of a lock-in amplifier, the second harmonic error of the product of the phase differences include the angular resolution of a lock-in amplifier, the second harmonic error of the product of  $|r_s||r_p|$  and the phase decorporate of the product of  $|r_s||r_p|$  and the phase difference of the product of  $|r_s||r_p|$  and the phase decorporate of the product of  $|r_s||r_p|$  and the phase difference of the product of  $|r_s||r_p|$  and the phase difference of the product of  $|r_s||r_p|$  and the phase difference of the product of  $|r_s||r_p|$  and  $|r_s||r_p|$  are nearly equal to 0.001 and 0.03°, respectively. Consequently, the curves of measurement resolution versus incident angle  $\theta$  for  $\Delta n$  and  $\Delta k$  can be obtained by substituting these data into Eqs.(14) and (15). The results are shown in Fig. 3. Obviously, the best resolution can be obtained as  $\theta$  is in the neighborhood near 70°. And  $\Delta n$  and  $\Delta k$  corresponding to our experimental conditions are calculated and added into Tab.1.

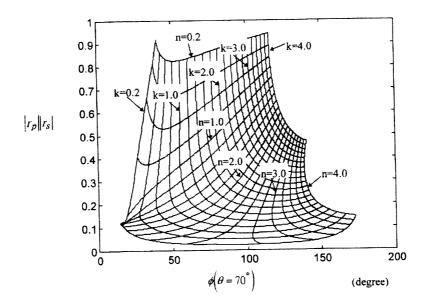


Fig. 3 Curves of measurement resolution versus  $\theta$  for  $\Delta n$  and  $\Delta k$  of nickle.

θ	60°	70°	80°
$ r_s  r_p $	0.609	0.571	0.585
φ	144.75°	121.01°	73.80°
n	1.9807	1.986	1.993
k	3.766	3.765	3.760
$\Delta n$	6.8×10 <sup>-3</sup>	6.4× 10 <sup>-3</sup>	7.1×10 <sup>-3</sup>
$\Delta k$	7.1×10 <sup>-3</sup>	5.6× 10 <sup>-3</sup>	4.0×10 <sup>-3</sup>

reference values<sup>13</sup>: N(Ni)=1.98+i3.74

Table 1: Experimental conditions and measurement results.

To investigate the effects of experimental conditions on the measurements, the relation curves of  $|r_s| r_p$  versus  $\phi$  for

 $\theta = 70^{\circ}$  are shown in Fig. 4. In the figure, the values of n and k are between 0.2 and 4.0 in 0.2 steps. According to Humphreys-Owen<sup>4</sup>, the sensitivity to the experimental conditions is indicated by the spacing between contours — if the spacing is large, the sensitivity is good and vice versa. It is obvious that our experimental conditions are useful if n and k are small. For good sensitivity, it is better to choose optimum incidence angles with the method proposed by Logofatu *et al.*18. In additions, curves of cinstant n and k as functions of k0 are shown in Fig. 5. We obtained them by

substituting the experimental conditions  $\theta = 70^{\circ}$ ,  $\Delta V = 0.001$ , and  $|\Delta \phi| = 0.03^{\circ}$  into Eqs. (14) and (15). In this figure, the values of n and k are 0.5 to 4 in steps of 0.5. It can seen that both  $\Delta n$  and  $\Delta k$  are smaller than  $1 \times 10^{-2}$ .

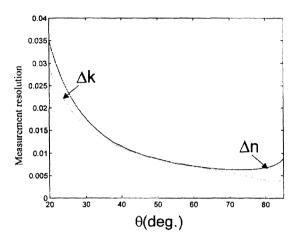


Fig. 4 Curves of constant n and k as a function of  $|r_s||r_p|$  and  $\phi$  at  $\theta = 70^\circ$ , where the values of n and k are between 0.2 and 4 in 0.2 steps.

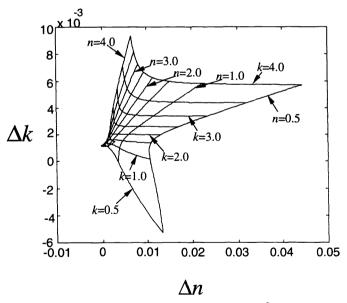


Fig.5 Curves of constant n and k as a function of  $\Delta n$  and  $\Delta k$  at  $\theta_1 = 60^\circ$  and  $\theta_2 = 80^\circ$ , where the values of n and k are between 0.5 and 4 in 0.5 steps.

### 5. CONCLUSION

Based on Fresnel's equations and the uses of a lock-in amplifier, a new method for measuring the complex refractive index is proposed. The product of the amplitude reflection coefficients of s and p polarizations and their phase difference of a light beam reflected from a complex refractive index are measured with a lock-in amplifier in a common-path interferometer. Then these data are substituted into the special equations derived from Fresnel's equations, and the complex refractive index of the material can be estimated. Its resolution is better than 0.01. It has both merits of a conventional common-path interferometer and a heterodyne interferometer, such as, simple optical setup, easy operation, high stability, high measurement accuracy, and rapid measurement. Its validity has been demonstrated.

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#### REFERENCES

- 1. E. D. Palik, Handbook of optical constants of solids, (Academic Press. Inc., New York, 1985), pp. 69-87.
- 2. I. Simon, "Spectroscopy in infrared by reflection and its use for highly absorbing substances," J. Opt. Soc. Am., 41, 336-345 (1951).
- 3. D. G. Avery, "An improved method for measurements of optical constants by reflection," *Proc. Phys. Soc. Landon Sect.* B., 65, 425-428 (1952).
- 4. S. P. F. Humphreys-Owen, "Comparison of reflection methods for measuring optical constants without polarimetric analysis, and proposal for new methods based the Brewster angle," *Proc. Phys. Soc.*, 5, 949-957 (1961).
- 5. W. R. Hunter, "Error in using the reflectance vs angle of incidence method for measuring optical constants," J. Opt. Soc. Am., 55, 1197-1204 (1965).
- 6. W. R. Hunter, "Optical constants of metals in the extreme ultraviolet I. A modified critical-angle technique for measuring the index of refraction of metals in the extreme ultraviolet," J. Appl. Phys., 34, 15-19 (1964).
- 7. R. M. A. Azzam, "Simple and direct determination of complex refractive index and thickness of unsupported or embedded thin films by combined reflection and transmission ellipsometry at 45° angle of incidence", J. Opt. Soc. Am, 73, 1080-1082, (1983).
- 8. J. Lekner, "Determination of complex refractive index and thickness of a homogeneous layer by combined reflection and transmission ellipsometry," J. Opt. Soc. Am. A, 11, 2156-2158(1994).
- 9. M. Born and E. Wolf, Principles of Optics, 6th ed. (Pergamon, Oxford, Uk, 1980), pp. 40.
- 10. M. H. Chiu, J. Y. Lee, and D. C. Su, "Refractive-index measurement based on the effects of total internal reflection and the uses of heterodyne interferometry," *Appl. Opt.*, **36**, 2936-2939 (1997).
- 11. D. C. Su, M. H. Chiu, and C. D. Chen, "Simple two frequency laser," Prec. Eng., 18, 161-163 (1996).
- 12. M. H. Chiu, C. D. Chen, and D. C. Su, "Method for determining the fast axis and phase retardation of a wave plate", J. Opt. Soc. Am. A, 13, 1924-1929 (1996).

- 13. E. D. Palik, Handbook of optical constants of solids, (Academic Press. Inc., New York, 1985), pp. 285 and 323.
- 14. N. M. Oldham, J. A. Kramar, P. S. Hetrick, and E. C. Teague, "Electronic limitations in phase meter for heterodyne interferometry," *Prec. Eng.*, 15, 173-179 (1993).
- 15. J. M. De Freitas and M. A. Player, "Importance of rotational beam alignment in the generation of second harmonic errors in laser heterodyne interferometry," *Meas. Sci. Technol.*, 4, 1173-1176 (1993).
- 16. W. Hou and G. Wilkening, "Investigation and compensation of the nonlinearity of heterodyne interferometers," *Prec. Eng.* **14**, 91-98 (1992).
- 17. A. E. Rosenbluth and N. Bobroff, "Optical sources of nonlinearity in heterodyne interferometers," *Prec. Eng.* 12, 7-11 (1990).
- 18. P. C. Logofatu, D. Apostol, V. Damian, and R. Tumbar, "Optimum angles for determining the optical constants from reflectivity measurements," *Meas. Sci. Technol.*, 7, 52-57 (1996).