

# Magnetocaloric Properties of Melt-Spun Fe–Ni–Mn–Ga Ribbons

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The effects of Ni substitution for Fe on phase constitutions, Curie temperature  $T_C$ , and magnetocaloric properties of melt-spun  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 0, 1, 3, 5$  and  $7$ ) ribbons have been investigated. X-ray diffraction results show that the main phase in the  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 0-7$ ) alloy changed with the increase of Ni content from FCC structure for  $x = 0$  into B2 structure for  $x = 1-7$ . Besides, the magnetic phase exhibits phase transition of ferromagnetic into paramagnetic state with increasing temperature for the samples with B2-type structure. The Curie temperature  $T_C$  of these ribbons varies in the temperature range of 232–257 K. The peak values of the maximal magnetic entropy change,  $-\Delta S_M^{\text{max}}$ , are about 1.4–1.6 J/kg/K for Ni-substituted ribbons at a maximum applied field of 30 kOe. On the other hand, the relatively broader temperature range at the half maximum of  $\Delta S_M$  peak ( $\sim 90$  K), low-cost and nontoxic elements make Fe–Ni–Mn–Ga-based ribbons the promising candidates for magnetic refrigeration applications close to room temperature.

**Index Terms**—Heusler alloy, magnetocaloric properties, melt-spun ribbon.

## I. INTRODUCTION

SINCE a large magnetic field-induced strain (MFIS) associated with a rearrangement of martensite variants by an external magnetic field in Ni–Mn–Ga alloys was first reported in 1996, [1] ferromagnetic shape memory alloys (FSMAs) have attracted significant attention due to their interesting physical properties, such as large magnetic-field-induced strain, [1], [2] giant magnetocaloric effects (MCEs), [3], [4] large magnetoresistance (MR), [5], [6] and exchange bias (EB) behavior [7], [8]. These properties make them a promising candidate as potential material for various practical applications in the field of smart, magnetic refrigeration and spintronics.

In contrast to most developed Ni–Mn based Heusler alloys, another representative of the FSMAs, i.e., Fe–Mn based system, has not received much attention up to now, such as Fe–Mn–Ga alloys, which also possess many of the above-mentioned features. Recently, Zhu *et al.* have reported that for a slightly off-stoichiometric  $\text{Fe}_{50}\text{Mn}_{22.5}\text{Ga}_{27.5}$  alloy, a field-induced transformation from a paramagnetic (PM) parent phase to a ferromagnetic (FM) martensite phase takes place at 163 K (on cooling), leading to a large lattice distortion of 33.5%; in the meantime, a large shape memory strain up to about 3.6% is observed due to the martensite transformation (MT) [9]. On the other hand, the giant EB effect was observed in stoichiometric  $\text{Fe}_2\text{MnGa}$  alloy ribbon, because transformation from antiferromagnetic (AFM) to FM phase can be induced by applying a magnetic field or by changing the temperature.

In addition, the EB behavior and enhanced coercivity occur simultaneously, revealing an exchange coupling between the coexisting antiferromagnetic and ferromagnetic phase [10], [11].

In our previous work, we reported phase transformation and EB behavior in as-spun Fe–Mn–Ga ribbons [12]. However, to date, there is no report on the effect of other magnetic elements' (Co or Ni) addition on the structure and magnetic phase evolution of Fe–Mn–Ga melt-spun ribbon systems. In this present work, the effect of Ni substitution for Fe on the crystal structure, magnetic state and magnetocaloric effect of the Fe–Ni–Mn–Ga Heusler alloy ribbons are reported.

## II. EXPERIMENT

The alloys with the nominal composition of  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 0, 1, 3, 5$  and  $7$ ) were prepared using arc melting pure elements ( $> 99.9\%$ ) in a high-purity argon atmosphere. To compensate for Mn losses during processing, an excess of 6 wt.% Mn was added. The ingot was melted three times to ensure homogeneity, and then melt-spun with a single-roll melt-spinner at a wheel linear speed of 15 m/s. The crystal structure of the ribbons was identified by X-ray diffraction (XRD) using  $\text{Cu-K}\alpha$  radiation at room temperature. Magnetic measurements were performed in the temperature interval of 10 – 330 K, and in external magnetic fields up to 30 kOe, using a physical properties measuring system (PPMS, Quantum Design Inc.) platform with a vibrating sample magnetometer module. The magnetic field was applied along the ribbon plane direction. Zero-field-cooled (ZFC) and field-cooled (FC) thermomagnetic curves were recorded at 200 Oe with a temperature heating or cooling rate of 10 K/min. Magnetic phase transition temperature was inferred from the maximum or minimum in the  $dM/dT$  versus  $T$  curve. The maximum magnetic entropy changes  $\Delta S_M(T, H)$

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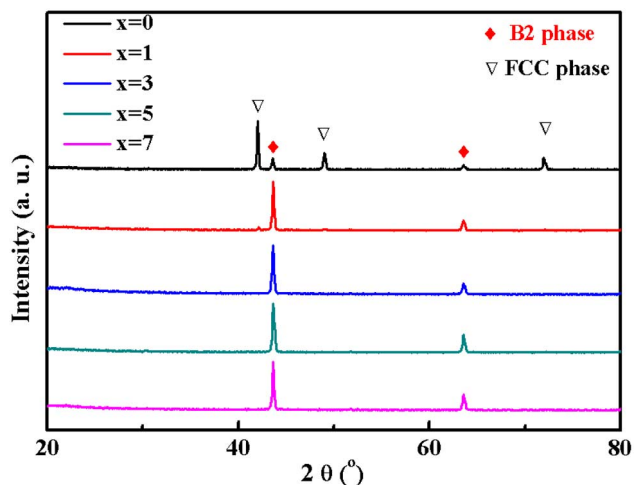


Fig. 1. XRD patterns of the melt spun  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 0, 1, 3, 5$  and  $7$ ) ribbons at room temperature.

were calculated from isothermal magnetization curves using the Maxwell relation [13]

$$\Delta S_M(T, H) = \int_0^H \left( \frac{\partial M}{\partial T} \right)_H dH.$$

### III. RESULTS AND DISCUSSION

Fig. 1 shows XRD patterns of the as-spun  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 0, 1, 3, 5$  and  $7$ ) ribbons at room temperature. The crystal structure of these series ribbons includes two kinds of structures, an ordered face-center-cubic (fcc) lattice of  $L1_2$ -type ( $\text{Cu}_3\text{Au}$ ) for  $x = 0$  and a partially ordered B2 phase for  $x = 1-7$ , respectively. According to the results of previous reports, stoichiometric  $\text{Fe}_2\text{MnGa}$  alloy should have the stable  $L2_1$ -type of structure [14]. However, it was experimentally found that stoichiometric  $\text{Fe}_2\text{MnGa}$  alloy crystallizes in a fcc-type structure [9], [10], [15]. Theoretical results reported by Kudryavtsev *et al.* [16] showed that the  $L2_1$ -type crystal structure with a lattice constant of  $a = 0.57$  nm in  $\text{Fe}_2\text{MnGa}$  is stable with ferrimagnetic order, instead of FM order. On the other hand, stable ordered fcc-type structure with lattice constants of  $a = 0.3644$  nm and  $a = 0.3666$  nm exhibited ferromagnetic and ferrimagnetic order, respectively. In this work, for  $x = 0$  samples, the main phase is found ordered fcc lattice of  $L1_2$ -type ( $\text{Cu}_3\text{Au}$ ), implying that the structure of ordered fcc-type is more stable than  $L2_1$ -type in  $\text{Fe}_2\text{MnGa}$  alloy. However, for alloy ribbons with  $x > 1$ , the main phase of ribbons changes into B2 structure. It is presumed that a chemical disorder B2 phase favors to form due to Ni-added alloy systems consisting of more than three elements [17] and also rapid solidification process.

Fig. 2 shows zero-field cooled (ZFC) and field-cooled (FC) magnetization as a function of temperature  $M(T)$  of  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ribbons with  $x = 0$  and  $1$ . It is seen that the behaviors of these two curves are quite different. For  $x = 0$ , a sudden jump in magnetization with increasing temperature

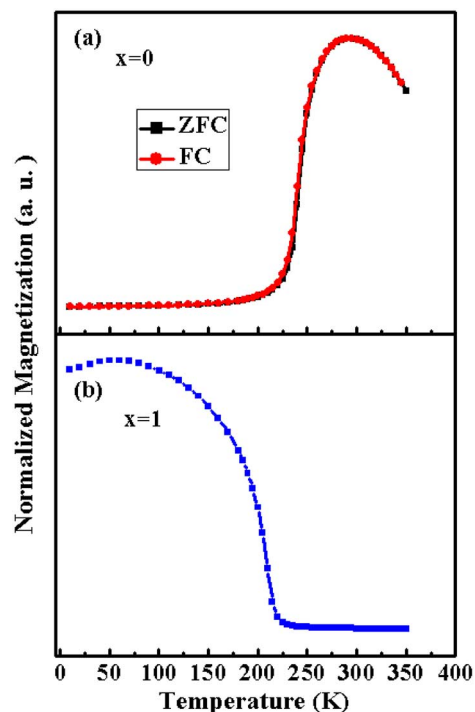


Fig. 2. (a) ZFC and FC magnetization curves as a function of temperature of  $\text{Fe}_{50}\text{Mn}_{25}\text{Ga}_{25}$  and (b) of  $\text{Fe}_{49}\text{Ni}_1\text{Mn}_{25}\text{Ga}_{25}$  ribbons obtained at a field of 200 Oe.

is observed. In addition, the magnetization curves recorded in field-cooled and field-warmed procedures are almost overlapped around the magnetic phase transition, indicating the second-order nature of the magnetic transitions. The structure and magnetic phase transition of the ribbons with  $x = 0$  are consistent with previous work [12], that is, magnetic phase transition of fcc structure from antiferromagnetic (AFM) to FM with increasing temperature. For Ni-added ribbons with  $x = 1$ , it exhibits a magnetic phase transition at  $T_C = 232$  K, which corresponds to Curie temperature of B2-type phase change from FM to PM state.

The temperature dependence of magnetization  $M(T)$  curves of  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 1-7$ ) ribbons, measured in an applied field of 1 kOe and temperature range from 190 to 380 K, are shown in Fig. 3(a), and their corresponding  $dM/dT$ -versus- $T$  curves are shown in Fig. 3(b). The Curie temperature  $T_C$  values, obtained from the  $M$ - $T$  curves, are summarized in Table I. From the results of Fig. 3, it can be found that the  $T_C$  and magnetization of B2 phase are increased with increasing Ni concentration. In B2-type structure, the magnetic moments depend mainly on anti-parallel coupling of Mn atoms and Fe atoms. Hence, a part of Fe replaced by Ni might reduce the exchange coupling of Fe and Mn atoms, leading to the enhancement of magnetization and Curie temperature.

The isothermal magnetization curves for  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 1-7$ ) ribbons are measured with an increasing magnetic field in a wide temperature range. The MCE as a function of temperature and magnetic field was calculated from the isothermal magnetization curves using the Maxwell relation under 0-30 kOe magnetic field changes. The  $M$ - $H$  curves of representative  $\text{Fe}_{49}\text{Ni}_1\text{Mn}_{25}\text{Ga}_{25}$  ribbons

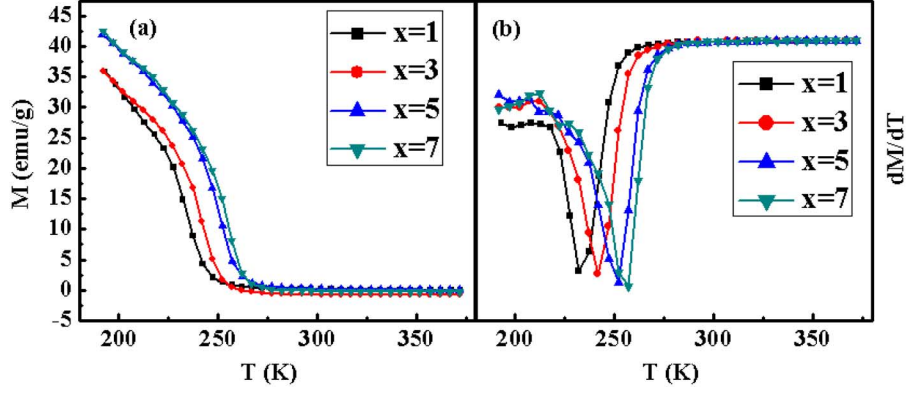


Fig. 3. Magnetization curves as a function of temperature of  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 1, 3, 5, 7$ ) ribbons obtained at a field of 1 kOe. (b) Corresponding  $dM/dT(T)$  curves.

TABLE I  
NOMINAL COMPOSITION, CURIE TEMPERATURE OF MAGNETIC PHASE TRANSITION ( $T_C$ ), MAXIMAL MAGNETIC ENTROPY CHANGES, ( $-\Delta S_M^{\max}$ ) AND RELATIVE COOLING POWER (RCP) AT MAGNETIC FIELD CHANGE OF 30 kOe OF  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  RIBBONS

X	Nominal composition	$T_C$ (K)	$-\Delta S_M^{\max}$ (Jkg/K)	RCP (Jkg)
1	$\text{Fe}_{49}\text{Ni}_1\text{Mn}_{25}\text{Ga}_{25}$	232	1.6	147.2
3	$\text{Fe}_{47}\text{Ni}_3\text{Mn}_{25}\text{Ga}_{25}$	242	1.4	126
5	$\text{Fe}_{45}\text{Ni}_5\text{Mn}_{27}\text{Ga}_{23}$	252	1.5	135
7	$\text{Fe}_{43}\text{Ni}_7\text{Mn}_{27}\text{Ga}_{23}$	257	1.5	130.5

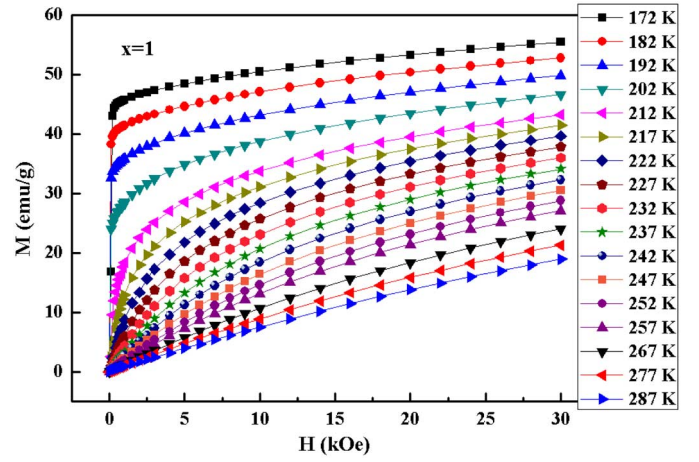


Fig. 4. Isothermal magnetization curves of  $\text{Fe}_{49}\text{Ni}_1\text{Mn}_{25}\text{Ga}_{25}$  ribbons obtained for a field change of 30 kOe.

obtained for a field change of 30 kOe are shown in Fig. 4. The maximal magnetic entropy changes of  $-\Delta S_M$ , as a function of Ni content  $x$ , are listed in Table I. The Ni substitution alters the magnetocaloric properties around the transition temperatures. The peak values of the maximal magnetic entropy changes,  $-\Delta S_M^{\max}$ , are about 1.4-1.6 Jkg/K for Ni-substituted ribbons, at a maximum applied field of 30 kOe. The change in  $-\Delta S_M$  should be caused by a change of magnetization around the transition temperatures. The difference in the magnetization can be ascribed to the exchange interaction on the magnetic moments of Fe and Mn atoms in Ni-Mn-based alloys. Hence, any change of the positions in B2 lattices caused by Ni addition could modify the strength of the interactions, leading to different magnetic exchanges in the phases, resulting in the change of magnetic entropy changes  $-\Delta S_M$  and  $T_C$ .

Another important parameter for magnetic refrigeration is the refrigeration capacity (RC), which is measured in literature by different methods [18]. The RC value represents how much heat can be transferred between cold and hot sinks in an ideal refrigerant cycle, [18] which is of practical significance. In present work, the RC values are estimated using the relative cooling power (RCP), which is given by the product of the  $\Delta S_M(T)$  maximum ( $\Delta S_M^{\max}$ ) and full width at half maximum of  $\Delta S_M^{\max}$  ( $\delta T_{\text{FWHM}}$ ), i.e.,  $\text{RCP} = -\Delta S_M^{\max} \times \delta T_{\text{FWHM}}$ . The RCP is approximately 4/3 times larger than the cooling

capacity for the same temperature interval. The RCP values for each of the  $\Delta S_M$  peaks of  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 1-7$ ) ribbons are also listed in Table I. The values of the RCP for  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 1-7$ ) ribbon samples are located in the range of 126-147.2 Jkg for a magnetic field change of 30 kOe, which is much larger than those of iron-based  $\text{Fe}_{60}\text{Cr}_{14}\text{Nb}_3\text{Si}_{13}\text{B}_9\text{Cu}_1$  alloy (87.3 Jkg) [19]. Therefore, despite relatively lower peak values of  $-\Delta S_M$ , but the relatively broader temperature range of the half maximum of  $\Delta S_M$  peak ( $\sim 90$  K), low-cost, nontoxic elements and simple synthesis procedures still make Fe-Ni-Mn-Ga-based ribbons promising candidates for magnetic refrigeration applications close to room temperature.

#### IV. CONCLUSION

The effect of Ni substitution for Fe in  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 0-7$ ) ribbons on the structure, magnetic phase transition and magnetocaloric properties has been reported. The experimental results show that the main phase of ribbons is changed with Ni concentration from the ordered fcc structure for  $x = 0$  into B2-type structure for  $x = 1-7$ . A proper addition of Ni can improve the magnetic coupling between magnetic atoms, leading to enhanced both magnetization and Curie

temperature. The maximum values of the magnetic entropy changes  $-\Delta S_M^{\max}$  are 1.6, 1.4, 1.5 and 1.5 J/kg K at 232, 242, 252 and 257 K for  $x = 1, 3, 5,$  and  $7,$  respectively, under applied magnetic field of 30 kOe. The moderate  $\Delta S_M$  and RCP values and low cost elements suggest that  $\text{Fe}_{50-x}\text{Ni}_x\text{Mn}_{25}\text{Ga}_{25}$  ( $x = 1-7$ ) ribbons may be promising substances for magnetic refrigeration materials working in the temperature interval range of 200 – 300 K.

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