

# Numerical and Experimental Analysis of Cu Diffusion in Plasma-Treated Tungsten Barrier

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This work investigates Cu diffusion in sputtered and  $N_2O$  plasma-treated W films.  $N_2O$  plasma-treated W barrier has a nanostructured surface layer and shows high thermal stability and the best barrier properties. Also investigated herein are the lattice and grain boundary diffusivities extracted from the Cu penetration depth profiles using the Whipple analysis of grain boundary diffusion and Fick's second law of diffusion. Analysis indicates that the diffusion models correlate well with experimental results. © 2004 The Electrochemical Society. [DOI: 10.1149/1.1833631] All rights reserved.

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As device dimensions decrease toward 180 nm and below, the necessity for interconnections with resistivity as low as possible is pressing. Copper is now being used in advanced metallization technology due to its low resistivity and high electromigration and stress migration resistance. However, Cu can diffuse into and react with Si or dielectric materials during annealing, and create deep trap levels that cause degradation of device performance and reliability.<sup>1,2</sup> Therefore, a qualified diffusion barrier inserted between Cu and Si or dielectric materials is necessary for the Cu metallization. Refractory metals and their nitrides are used as diffusion barriers in copper metallization.<sup>3-6</sup> Among these materials, tungsten nitride (WN) has received the most attention owing to its high thermal stability and excellent chemical mechanical polishing (CMP) process compatibility.<sup>7</sup> However, resistivity of tungsten nitride film is higher than that of tungsten film. As the technology node moves to 130 nm and below, a barrier layer with low resistivity is necessary to lower the resistance of the total line interconnect and/or via.

Most refractory metal films used as diffusion barriers in Cu metallization are polycrystalline rather than monocrystalline. Moreover, columnar grain structure is frequently found in sputtered refractory metal and metal nitride films.<sup>8-10</sup> In general, atomic diffusion along grain boundaries is much faster than in the bulk of grains. Grain boundaries may presumably serve as fast diffusion paths for copper. Coupled lattice and grain boundary diffusion is different from lattice diffusion. Whipple had given formulas for the concentration in a semi-infinite region of low diffusion coefficient bisected by a thin well-diffusing slab.<sup>11,12</sup> This is of interest in grain boundary diffusion.

In this study, a method of forming nitrogen and oxygen incorporated W films with low resistivity was investigated. N<sub>2</sub>O plasma was used to post-treat the W diffusion barrier. The effectiveness of asdeposited and N<sub>2</sub>O plasma treated W films as diffusion barriers between Cu and Si was evaluated. A composite diffusion barrier was formed after N<sub>2</sub>O plasma treatment. Cu diffusion in the N<sub>2</sub>O plasma treated W barrier was further analyzed by numerical calculation using Whipple's and Fick's models.

## **Experimental**

Single crystal, (100) orientated silicon wafers were used in this study. Tungsten films of 50 nm were deposited at a power of 1000 W by sputtering. Films were sputtered at room temperature without intentional heating and base pressure was less than  $6 \times 10^{-7}$  Torr. The wafers further received N<sub>2</sub>O plasma treatment in a plasma-enhanced chemical vapor deposition (PECVD) system after W films were deposited. The power and pressure of N<sub>2</sub>O plasma treatment were 200 W and 100 mTorr, respectively. Some wafers were treated

by N<sub>2</sub> or NH<sub>3</sub> plasma for comparison. For easy identification, the untreated, N<sub>2</sub>O, N<sub>2</sub>, and NH<sub>3</sub> plasma-treated W films were denoted as W, W(N<sub>2</sub>O), W(N<sub>2</sub>), and W(NH<sub>3</sub>) barriers in the work. Copper films, 300 nm thick, were deposited on top of the barrier layers by sputtering. The efficiency of the diffusion barrier was analyzed by the variation of sheet resistance and leakage current densities of junction diodes after thermal stressing in N<sub>2</sub> ambient at 500–700°C, *i.e.*, 773–973 K, for 30 min. The wafers were administered a local oxidation of silicon (LOCOS) process to define active regions. The active regions were implanted with  $5 \times 10^{15}$  As<sup>+</sup> ions/cm<sup>2</sup> at energy of 60 keV for n<sup>+</sup>-p junction diodes, and dopants were activated by rapid thermal annealing (RTA) in N<sub>2</sub> ambient at 1050°C for 30 s. Leakage currents of diodes were measured at a reverse bias of 5 V by a HP 4156 semiconductor parameter analyzer. A four-point probe system was employed to measure sheet resistance.

Film thickness was measured by a stylus surface profiler and scanning electron microscopy (SEM). X-ray photoemission spectroscopy (XPS) was used to study the bonding structures and chemical binding energies. The microstructure and grain size of the film were examined using transmission electron microscopy (TEM). Structure and crystalline orientation of as-deposited and annealed samples were analyzed by an X-ray diffractometer (XRD) with Cu K $\alpha$  radiation operated at 50 kV and 250 mA. Surface roughness and morphology of the film were observed using a Digital Instruments Nanoscope II model atomic microscope (AFM) with a 0.5 Hz scanning speed in air ambient. Surface morphology was studied by a field-emission scanning electron microscope (FESEM). Compositional depth profiles were measured by secondary ion mass spectrometry (SIMS).

### **Results and Discussion**

To investigate the effects of N2O plasma treatment on W barrier, chemical bonding states of barrier were analyzed by XPS. Figure 1a-c show the W 4f, O 1s, and N 1s spectra of as-deposited and N<sub>2</sub>O plasma-treated W barriers. The W  $4f_{7/2}$  and W  $4f_{5/2}$  peaks are situated at the same position (31.2, 33.4 eV) for two barriers, and the two peaks are characteristics of the W itself.<sup>13</sup> However, two other peaks at binding energies 36.2 and 38.4 eV are observed for the W(N<sub>2</sub>O) barrier. The peaks correspond to binding energies of tungsten oxide and are attributed to oxidation during N2O plasma treatment. The O 1s spectrum of the  $W(N_2O)$  barrier exhibits a strong and broad peak centered at around 531.2 eV, as shown in Fig. 1b. There is almost no peak in untreated W barrier. W-O phases are believed to form at the surface of W(N2O) barrier. The N 1s peak of the  $W(N_2O)$  barrier can be well resolved into two peaks by curve fitting compared to no peak in the N 1s spectrum of the W barrier, as shown in Fig. 1c. These two peaks are centered at 397.5 and 399.3 eV. The weak peak centered at 397.5 eV is consistent with the N 1s binding energy of nitride compound and is also reported by previous research.<sup>14</sup> Another strong peak at  $\sim$ 399.3 eV is observed in N 1s

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Figure 1. (a) W 4f, (b) O 1s, and (c) N 1s XPS spectra of W and W(N\_2O) barriers.







**(b)** 



Figure 2. (a) Cross-sectional bight field TEM image of W barrier. Planeview TEM images and SAD patterns of the (b) W and (c)  $W(N_2O)$  barriers.

spectrum. This indicates that some N atoms do not form strong covalent or ionic bonds with W during N<sub>2</sub>O plasma treatment. Some N atoms or molecules may present in grain boundaries of W. $^{8,15,16}$ 

Figure 2a displays cross-sectional bright field TEM micrograph of as-sputtered W film. Columnar grain structure is observed. Cu diffusion in columnar grains is believed to be relatively easy because columnar grains will provide fast diffusion paths for Cu diffusion. Figure 2b and c display plane-view TEM images and selected area diffraction (SAD) patterns of W and W(N<sub>2</sub>O) barriers. Several sharp rings are observed for untreated W film. This indicates that the as-deposited W film is a polycrystalline structure. The grain size of as-deposited W film is 20–40 nm, as shown in Fig. 2b. The W(N<sub>2</sub>O) barrier has a diffused ring pattern instead of diffraction spots, indicating that the N<sub>2</sub>O plasma treatment causes an amor-



Figure 3. Resistivity and RMS surface roughness of  $W(N_2)$ ,  $W(NH_3)$ , and  $W(N_2O)$  films as a function of plasma treatment time.

phous surface layer upon W film. Grain size of the W(N<sub>2</sub>O) barrier is only 2–5 nm. This indicates that a surface layer with finer grains is formed due to the reactions and bombardments of energetic radicals and ions during plasma treatment. It is reported that the nanostructured amorphous diffusion barrier, defined as a very short-range order single crystal, is highly attractive due to its relatively high thermal stability and its relatively higher resistance against Cu diffusion.<sup>17</sup>

Figure 3 displays resistivity and root-mean-square (RMS) surface roughness of plasma treated W film as a function of plasma treatment time. Surface roughness reduces apparently after plasma treatment, as shown in Fig. 3. Plasma treatment could sputter the barriers and make them smooth. Sputtering and stuffing effects are believed to occur due to the reactions or bombardments of energetic radicals and ions during plasma treatment. Resistivity increases with increasing plasma treatment time. It is expected that resistivity of W with plasma treatment would increase because a high-resistivity surface layer is formed and thus the effective thickness of the W film with low resistivity reduces. Resistivity of W(N<sub>2</sub>O) barrier is higher than those of the  $W(N_2)$  and  $W(NH_3)$  barriers. High resistivity may be due to the formation of high-resistance W-O compounds in W(N<sub>2</sub>O) barrier, as indicated in XPS analyses. However, the resistivity of W(N<sub>2</sub>O) ( $\sim$ 24  $\mu\Omega$  cm) barrier is still much lower than that of the reactively sputtered WN film (150  $\sim$  200  $\mu\Omega$  cm).<sup>8</sup>

Table I summarizes the properties of W, WN and W(N<sub>2</sub>O) barriers. Table I also lists properties of sputtered Ta and Ti films in literatures<sup>4,6,16,18</sup> for comparison. The resistivities of sputtered W and W(N<sub>2</sub>O) barriers are about 20 and 24  $\mu$ O cm, respectively. The resistivities are very close and much lower than that of the reactively sputtered WN (150–200  $\mu$ O cm),<sup>8</sup> Ta (~160  $\mu$ O cm),<sup>4,16</sup> and Ti (~70  $\mu$ O cm).<sup>18</sup> Hara *et al.* have reported that the agglomeration and adhesion strength of the copper seed layer, its crystallographic orientation along (111), and the resistivity of the subsequent electro-



Figure 4. (a) Variation percentage in sheet resistance of Cu/barrier/Si as a function of annealing temperature. (b) XRD spectra of Cu/W/Si and Cu/W(N<sub>2</sub>O)/Si contact systems after annealing at 700°C for 30 min.

plated copper layer, are affected by the stress in the copper seed layer deposited on the barrier layer.<sup>19,20</sup> Electroplating of Cu layer is difficult on seed layers with rough surface. Surface roughness could be reduced from 2.5 to 0.5 nm by N<sub>2</sub>O plasma treatment, as listed in Table I. Grain size is calculated from plane-view TEM. The asdeposited W film is columnar grain structure with a grain size of 20–40 nm and grain size of the W(N<sub>2</sub>O) barrier is only 2–5 nm. This indicates that nanocrystallization effect would occur due to the reactions and bombardments of energetic radicals and ions during N<sub>2</sub>O plasma treatment. Furthermore, it is reported that the impurities (nitrogen or oxygen) in the films are responsible for the intrinsic compressive stress.<sup>21</sup> In this research, the tensile stress decreases from  $1.9 \times 10^{10}$  to  $1.4 \times 10^9$  dynes/cm<sup>2</sup> as N<sub>2</sub>O plasma treatment also enhances the adhesion between Cu and W(N<sub>2</sub>O) barrier. The adhesion strength of Cu on W(N<sub>2</sub>O) barrier (50–58 Mdynes/cm<sup>2</sup>) is

Table I. Properties of W, WN, and  $W(N_2O)$  diffusion barriers. Properties of sputtered Ta, Ti films are also listed for comparison. Leakage current densities of diodes were measured at a reverse bias of 5 V after annealing at 600°C for 30 min.

|                                    | W                         | W(N <sub>2</sub> O)       | $WN^8$                    | Ta <sup>4,6,16</sup> | Ti <sup>6,18</sup>   |
|------------------------------------|---------------------------|---------------------------|---------------------------|----------------------|----------------------|
| Resistivity (µO cm)                | $\sim 20$                 | ~24                       | 150-200                   | ~160                 | $\sim 70$            |
| RMS roughness (nm)                 | 2.5                       | $\sim 0.5$                | 1-2                       | 4                    | 3.2 - 4.2            |
| Grain Size (nm)                    | 20-40                     | 2-5                       | 5-15                      | 20                   | 10-30                |
| Stress (dynes/cm <sup>2</sup> )    | $1.9	imes10^{10}$         | $1.4 \times 10^{9}$       | $1.5 	imes 10^{10}$       | $2.0 	imes 10^{10}$  | $3.9 \times 10^{9}$  |
| Adhesion                           | poor                      | good                      | poor                      | poor                 | fair                 |
| Leakage current density $(A/cm^2)$ | $\sim 9.0 \times 10^{-4}$ | $\sim 3.0 \times 10^{-9}$ | $\sim 8.5 \times 10^{-6}$ | $2.5 \times 10^{-5}$ | $5.5 \times 10^{-4}$ |



**Figure 5.** Statistical distributions of leakage current densities of copper contacted  $n^+$ -p junction diodes with various diffusion barriers after annealing at (a) 500 and (b) 600°C for 30 min.

better than untreated W (30-35 Mdynes/cm<sup>2</sup>) and other barriers such as Ta and Ti.<sup>6</sup> It is suggested that O or N species on the barrier surface can react with Cu to form more stable interface and thus promote adhesion after N<sub>2</sub>O plasma treatment.

Figure 4a shows the variation percentage of the Cu/barrier/Si system after furnace annealing at various temperatures. The variation in sheet resistance is defined as the ratio of  $(R - R_0)$  to  $R_0$ , in which  $R_0$  and R denote the sheet resistance of as-deposited and annealed samples. The results reflect the interactions between Cu and Si indirectly. Resistance increases rapidly at certain temperature because of failure of the diffusion layer and formation of compounds. Sheet resistance of Cu/W(N2O)/Si increases slightly even after annealing at 750°C. However, sheet resistances of samples with other barriers (W, WN,<sup>8</sup> WC<sub>x</sub>,<sup>22</sup> TiC<sub>x</sub>,<sup>23</sup> and TaN<sup>24</sup>) sharply increase after annealing at 600-700°C, indicating that a considerable amount of Cu has already diffused through the barrier layers and resulted in Cu<sub>3</sub>Si compounds, and thus strongly deteriorated the conductivity of the contact system. XRD was further used to detect the structural change in the annealed samples. Figure 4b shows XRD patterns of Cu/W/Si and Cu/W(N2O)/Si systems after annealing at 700°C for 30 min. Peaks of Cu<sub>3</sub>Si compounds are observed for W barrier and the resulting XRD pattern is consistent with variation in sheet resistance. There is no  $Cu_3Si$  peak in  $W(N_2O)$  barrier system, indicating that W(N2O) has an excellent barrier performance. It is noted that there is no Cu-W compound in the XRD spectra, and similar results are found for WN barriers.<sup>8</sup> The failure of W and WN barriers is attributed that Cu atoms diffuse through defects and grain boundaries of the barrier without reacting with the



**Figure 6.** Statistical distributions of leakage current densities of copper contacted  $n^+$ -p junction diodes with various plasma-treated W diffusion barriers after annealing at (a) 500 and (b) 600°C for 30 min.

WN and W film. Failure temperature (variation percentage > 50%) of W(N<sub>2</sub>O) barrier is higher than 750°C and superiors to sputtered WC<sub>x</sub>(~650°C),<sup>22</sup> TiC<sub>x</sub>(~625°C),<sup>23</sup> and TaN(~650°C)<sup>24</sup> barriers.

Barrier performance is also evaluated by the leakage current density of the junction diode. Figure 5 illustrates the statistical distributions of leakage current densities of Cu/barrier/n<sup>+</sup>-p junction diodes measured at reverse bias of 5 V after annealing at 500 and 600°C. The leakage current densities of all diodes are below 10<sup>-8</sup> A/cm<sup>2</sup> before annealing. Most diodes with sputtered W, WN,<sup>8</sup> WC<sub>x</sub>,<sup>22</sup> and TiC<sub>x</sub><sup>23</sup> barriers have leakage current densities higher than 1  $\times$  10<sup>-7</sup> A/cm<sup>2</sup> after annealing at 500°C for 30 min. Diodes with W(N<sub>2</sub>O) barriers retain leakage current densities less than 10<sup>-8</sup> A/cm<sup>2</sup> after annealing at 500°C. Moreover, most diodes with W(N<sub>2</sub>O) barriers retain leakage current densities less than 10<sup>-8</sup> A/cm<sup>2</sup> even after annealing at 600°C. W(N<sub>2</sub>O) show an excellent barrier capability against Cu diffusion compared to W, WN,<sup>8</sup> WC<sub>x</sub>,<sup>22</sup> TiC<sub>x</sub>,<sup>23</sup> and TaN,<sup>24</sup> as shown in Fig. 5.

Although barrier performance of the W film is significantly improved by N<sub>2</sub>O plasma treatment, similar plasma treatments, *e.g.*, N<sub>2</sub> plasma treatment, had been proposed to enhance barrier performance in previous researches.<sup>15,16</sup> W barriers are also treated by N<sub>2</sub> or NH<sub>3</sub> plasma for comparison in the work. Figure 6 exhibits statistical distributions of leakage current densities of Cu/W(N<sub>2</sub>O)/n<sup>+</sup>-p, Cu/W(N<sub>2</sub>)/n<sup>+</sup>-p and Cu/W(NH<sub>3</sub>)/n<sup>+</sup>-p diodes after annealing at 500 and 600°C. All W(N<sub>2</sub>O), W(N<sub>2</sub>), and W(NH<sub>3</sub>) show an enhanced barrier performance compared to untreated W. Moreover, N<sub>2</sub>O plasma treatment has a better barrier improvement than N<sub>2</sub>



Figure 7. SIMS distribution profiles of the copper elements in (a) Cu/W/Si and (b) Cu/W(N<sub>2</sub>O)/Si after annealing at 600, 650, and 700°C in N<sub>2</sub> ambient for 30 min.

plasma treatment and N<sub>2</sub> plasma is more effective than NH<sub>3</sub> plasma. It is found that some diodes have leakage current densities higher than  $1\times 10^{-7}~\text{A/cm}^2$  for W(NH\_3) barriers after annealing at 500°C. Most diodes with W(N2O) barriers retain leakage current densities less than 1  $\times$  10<sup>-8</sup> A/cm<sup>2</sup> and large leakage current densities in range of  $10^{-7}$  to  $10^{-4}$  are found for Cu/W(N<sub>2</sub>)/n<sup>+</sup>-p and  $Cu/W(NH_3)/n^+$ -p diodes after annealing at 600°C. Enhancing performance of the W(N<sub>2</sub>O) barrier is attributed to combined effects of nitridation and oxidation during N2O plasma treatment. N2O is a strong oxidizing agent and energetic oxygen radicals and atoms are more easily produced by dissociation of N<sub>2</sub>O. In contrast, it is less effective to dissociate triple bonds of nitrogen as nitrogen plasma is used to post-treat W barrier. The bond strengths of N-O and N-N are 630.57 and 945.33 kJ/mol. Energetic oxygen radicals and atoms are helpful in formation of an oxygen stuffed layer on the columnargrained W barrier. It will act as a more efficient barrier against the Cu diffusion. N<sub>2</sub> plasma treatment does not induce oxygen stuffed layer on surface of the W barrier and nitrogen radicals and atoms are limited for nitridation and stuffing compared to N2O plasma treatment. Bond strength of N-H is 339 kJ/mol for NH<sub>3</sub> plasma treatment. Although nitridation is expected to occur greatly, no plasma oxidation on W surface occurs and lots of atomic hydrogen will diffuse into the grain boundaries of W due to effective dissociation of NH<sub>3</sub>. Hydrogen will out-diffuse from grain boundaries of plasma-treated W after annealing at a certain temperature, lead to defect sites or carrier trapping sites, and hence, decrease its resistance to copper penetration.



Figure 8. Penetration plots for Cu diffusion into W films at various temperatures of (a) 600, (b) 650, and (c) 700°C. The solid curve is the fitting curve.

Barrier capabilities are further investigated by evaluating Cu diffusion in W and W(N<sub>2</sub>O) barriers. The diffusion of Cu in the temperature range of 600–700°C is evaluated by SIMS and the penetration depth profiles of specimens are indicated in Fig. 7. Relatively low Cu penetration into the W(N<sub>2</sub>O) barrier is detected compared to sputtered W barrier. Because the mixing enthalpy of Cu solute in W is large ( $8.0 \times 10^4$  j/mol), Cu atoms do not intermix with W at high temperature.<sup>25,26</sup> As far as we know, it is relatively difficult for Cu penetration into W barrier by lattice diffusion. However, the diffusion coefficients of Cu in grain boundaries of W barrier are still Table II. Summary of the values of diffusivities, pre-exponential factors, and activation energies for Cu diffusion in W films at various annealing temperatures.

| Sample | T (°C) | $D_{\rm L}~({\rm cm^2/s})$ | $D_{\rm B}~({\rm cm^2/s})$ | $D_{\rm L0}~({\rm cm}^2/{\rm s})$ | $Q_{\rm L}~({\rm eV})$ | $D_{\rm B0}~({\rm cm^{2}/s})$ |
|--------|--------|----------------------------|----------------------------|-----------------------------------|------------------------|-------------------------------|
| W      | 600    | $2.28 \times 10^{-16}$     | $6.47 \times 10^{-14}$     | $1.83 \times 10^{-13}$            | 0.508                  | $1.28 \times 10^{-4}$         |
|        | 650    | $2.60 \times 10^{-16}$     | $1.24 \times 10^{-13}$     |                                   |                        |                               |
|        | 700    | $4.70 \times 10^{-16}$     | $6.05 \times 10^{-13}$     |                                   |                        |                               |

unknown, though the rough estimation has been discussed,<sup>27</sup> and the results are still needed to be further discussed.

Whipple had given formulas for the concentration in a semiinfinite region of low diffusion coefficient bisected by a thin welldiffusing slab. Because our source condition is close to infinite one, the Whipple's solution is used for profile analysis.<sup>11</sup> The key result of Whipple's solution is

$$D_{\rm B}\delta = 0.661 \left( -\frac{\partial \ln(\bar{C})}{\partial y^{6/5}} \right)^{-5/3} \left( \frac{4D_{\rm L}}{t} \right)^{1/2}$$
[1]

where  $\overline{C} = C/C_s$ , *C* represents the concentration in a section at a depth *y* µm from the original surface,  $C_s$  is the surface concentration, *t* is the annealing time, and *d* is the grain boundary width.  $D_L$  and  $D_B$  present the diffusion coefficients in the lattice and the grain boundary. Figure 8 displays the concentration profiles obtained from diffusion of Cu in W barriers at various temperatures in the standard coordinates  $\ln \overline{C} vs. y^{6/5}$ . Based on Eq. 1 and provided that  $D_L$  is known,  $\delta D_B$  can be determined by measuring the slope from the linear region in the  $\ln \overline{C} vs. y^{6/5}$  plots. The value of  $D_L$  can be found from the initial part of the concentration profile. Under the assumptions of a semi-infinite system and constant source at the surface, the boundary conditions applied to solve Fick's diffusion equation are

$$C = C_s, \quad y < 0, \quad t = 0$$
 [2]

$$C = 0, \quad y > 0, \quad t = 0$$
 [3]

An error function solution can be expressed by the equation

$$C(y, t) = C_{s} \operatorname{erfc}\left(\frac{y}{2\sqrt{D_{L}t}}\right)$$
[4]

where the error function was fitted to the initial part of the concentration profiles and extrapolated to zero thickness y = 0 in the case of subtracting the grain boundary contribution. The results are shown in Table II, and the derived value of  $D_{\rm L}$  was used to calculate  $\delta D_{\rm B}$ . To obtain a value  $D_{\rm B}$ , a grain boundary width must be assumed, it is reasonable to assume a width of about two atom layers,  $\delta = 5 \times 10^{-8}$  cm.<sup>28,29</sup>



**Figure 9.** The Arrhenius plot of the grain boundary diffusivity  $D_{\rm B}$  for Cu diffusion in W films.

Based on the numerical calculation, a satisfactory fitting to the experimental depth profile can be obtained.<sup>10</sup> The temperature dependence of the grain boundary diffusivity in W barrier can be expressed by the Arrhenius relation of  $D_{\rm B} = D_{\rm B0} \exp(-Q_{\rm B}/kT)$ , as plotted in Fig. 9, where  $D_{\rm B0}$  is the pre-exponential factor,  $Q_{\rm B}$  is the activation energy for grain boundary diffusion, k is the Boltzmann constant, and T is annealing temperature. Also, the temperature dependence of the lattice diffusivity in W barrier can be expressed by the Arrhenius relation of  $D_{\rm L} = D_{\rm L0} \exp(-Q_{\rm L}/kT)$ , where  $D_{\rm L0}$  and  $Q_{\rm L}$  are pre-exponential factor and activation energy for lattice diffusivities, pre-exponential factors, and activation energies are summarized in Table II. The D values of Cu in sputtered W films are smaller than those in CVD-W films, but the magnitudes are in the same order. In addition, the activation energy of Cu diffusion in sputtered W films is somewhat larger than that in CVD-W films.<sup>27,30</sup>

Similar numerical analysis can be applied to evaluate the effects of Cu diffusion in W(N<sub>2</sub>O) barriers. As mentioned previously, N<sub>2</sub>O plasma treatment causes an amorphous surface layer upon the W film. This is the case of a semi-infinite medium which has a skin or surface layer W(N<sub>2</sub>O)<sub>1</sub> having diffusion properties different from those of the rest of the medium W(N<sub>2</sub>O)<sub>2</sub>. The subscripts 1 and 2 denote the amorphous surface layer and the rest in the W(N<sub>2</sub>O) barrier. Thus, suppose in the semi-infinite region  $-h < y' < \infty$ , the lattice diffusion coefficient is  $D_{L1}$  in the region  $-h < y' < \infty$ , the lattice diffusion coefficient is  $D_{L1}$  in the region  $-h < y' < \infty$ , the interface to be  $C_1 = C_2$ , y' = 0 and  $D_{L1}\partial C_1/\partial y' = D_{L2}\partial C_2/\partial y'$ , y' = 0 the solution to the problem of zero initial concentration and the surface y' = -h maintained at constant concentration  $C_0$  is given as<sup>12</sup>

$$C_{1} = C_{0} \sum_{n=0}^{\infty} \alpha^{n} \Biggl\{ \operatorname{erfc} \frac{(2n+1)h + y'}{2\sqrt{D_{L1}t}} - \alpha \operatorname{erfc} \frac{(2n+1)h - y'}{2\sqrt{D_{L1}t}} \Biggr\}$$
[5]



Figure 10. The Arrhenius plot of the lattice diffusivity  $D_{\rm L}$  for Cu diffusion in W films.



Figure 11. Penetration plots for Cu diffusion into W(N<sub>2</sub>O) films at various temperatures of (a) 600, (b) 650, and (c) 700°C. The solid curve is the profile calculated from Eq. 5 and 6.

$$C_{2} = \frac{2kC_{0}}{k+1} \sum_{n=0}^{\infty} \alpha^{n} \operatorname{erfc} \frac{(2n+1)h + ky'}{2\sqrt{D_{L1}t}}$$
[6]

where  $k = \sqrt{D_{L1}/D_{L2}}$ ,  $\alpha = (1 - k)/(1 + k)$ The thickness *h* of the surface layer W(N<sub>2</sub>O)<sub>1</sub> is about 3 nm from high-resolution TEM micrograph. Both diffusion coefficients can be obtained by numerical calculation. The values of  $D_{L1}$  and  $D_{L2}$  can be roughly estimated from fitting of experimental concentration profiles using an error function solution such as that in Eq. 4. The estimated values are used as the initial guess of  $D_{L1}$  and  $D_{L2}$ and further substituted into the Eq. 5 and 6 to obtain concentrations  $C_1$  and  $C_2$ , respectively. To quickly obtain the numerical convergence, the high order terms are neglected in the Eq. 5 and 6 during the calculation. It is found that the calculated error is smaller than  $10^{-4}$  as n = 4. The asymptotic solutions of lattice diffusion coefficients can be obtained by steep-descent method and fitting of the experimental concentration profile. Figure 11 shows experimental and calculated concentration profiles. The derived values of  $D_{L1}$  and  $D_{L2}$  are listed in Table III.

Similarly, grain boundary diffusion coefficients  $D_{B2}$  in W(N<sub>2</sub>O)<sub>2</sub> region can be determined from the derived lattice diffusion coefficient  $D_{L2}$  and the slope in  $\ln \bar{C}$  vs. y'<sup>6/5</sup> plots. Figure 12 displays experimental concentration profiles for Cu diffusion in W(N<sub>2</sub>O) barriers at various annealing temperatures in the standard coordinates  $\ln \bar{C}$  vs.  $v'^{6/5}$ . The derived grain boundary diffusion coefficients  $D_{\rm B2}$ are listed in Table III. Table III summaries the values of diffusion coefficients and pre-exponential factors for Cu diffusion in W(N2O) barriers. Other barrier materials in literatures are also listed for comparison.<sup>27,30,31</sup> The  $W(N_2O)$  barrier shows small lattice diffusion coefficients compared to W2N, W, and TiB2 barriers. The variation of  $D_{L2}$  with temperature is slight for the W(N<sub>2</sub>O) barrier, indicating that the W(N<sub>2</sub>O) barrier has better thermal stability.

One significant finding in the present study is that some atomic nitrogen and oxygen will react with W, segregate at grain boundaries of W film as impurities, and act as a stuffing agent to block fast diffusion path during N2O plasma treatment. Nitrogen addition will stuff the grain boundaries of W and nitrify tungsten to form tungsten nitride, as shown in XPS analyses of Fig. 1c. Similar nitridation effect had been reported by Hara *et al.*<sup>32</sup> A TiN barrier was formed at the surface of the Ti layer in high-pressure ammonium ambient. Figure 13 shows cross sections of the interfacial structures of Cu/ W/Si and Cu/W(N<sub>2</sub>O)/Si samples before and after annealing. The as-deposited W barrier has a columnar grain structure as shown in Fig. 13a. The failure of W barrier is attributed to the Cu diffusion through the columnar W to form Cu<sub>3</sub>Si after annealing at 700°C for 30 min. Grain boundary diffusion coefficients are  $6.5 \times 10^{-14}$  $\sim 6.1 \times 10^{-13}$  cm<sup>2</sup>/s using Whipple analysis of grain boundary

Table III. Summary of the values of diffusivities, and pre-exponential factors for Cu diffusion in W(N<sub>2</sub>O) films and at various annealing temperatures. Other barrier materials are also listed for comparison.

|                     |                | $D_{\rm L}  ({\rm cm}^2/{\rm s})$        |                        | $D_{\rm B}~({\rm cm}^2/{\rm s})$ | $D_{\rm L0}~({\rm cm}^2/{\rm s})$ |                        |                                   |  |
|---------------------|----------------|--|------------------------|----------------------------------|-----------------------------------|------------------------|-----------------------------------|--|
| Sample              | $T(^{\circ}C)$ | $D_{L1}$                                 | $D_{L2}$               | $D_{B2}$                         | $D_{ m L0,1}$                     | $D_{ m L0,2}$          | $D_{\rm B0}~({\rm cm}^2/{\rm s})$ |  |
| W(N <sub>2</sub> O) | 600            | $1.17 \times 10^{-16}$                   | $1.58 \times 10^{-16}$ | $4.07 \times 10^{-14}$           | $6.12 \times 10^{-15}$            | $6.43 \times 10^{-15}$ | $9.28 \times 10^{-13}$            |  |
|                     | 650            | $1.45 \times 10^{-16}$                   | $2.04 	imes 10^{-16}$  | $5.37 \times 10^{-14}$           |                                   |                        |                                   |  |
|                     | 700            | $1.76 	imes 10^{-16}$                    | $2.31 \times 10^{-16}$ | $5.57 \times 10^{-14}$           |                                   |                        |                                   |  |
| $W_{2}N^{27}$       | 600            | $1.15	imes 10^{-16}\ 4.52	imes 10^{-16}$ |                        |                                  | $7.00 	imes 10^{-11}$             |                        |                                   |  |
| -                   | 700            |  |                        |                                  |                                   |                        |                                   |  |
| $W^{30}$            | 600            | $2.4 \times 10^{-16}$                    |                        | $1.11 	imes 10^{-13}$            |                                   |                        |                                   |  |
|                     | 700            | 4.5 	imes                                | $10^{-16}$             |                                  |                                   |                        |                                   |  |
| $TiB_2^{31}$        | 500            | $1.4 \times$                             | $10^{-15}$             |                                  |                                   |                        |                                   |  |
| 2                   | 600            | 2.0 	imes                                | $10^{-15}$             |                                  |                                   |                        |                                   |  |
|                     | 700            | 5.3 ×                                    | $10^{-15}$             |                                  |                                   |                        |                                   |  |
|                     | 800            | 5.0 ×                                    | $10^{-14}$             |                                  |                                   |                        |                                   |  |

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Figure 12. Penetration plots for Cu diffusion into  $W(N_2O)$  films at various temperatures of (a) 600, (b) 650, and (c) 700°C. The solid curve is the fitting curve.

diffusion. The barrier capability of the W film against Cu diffusion can be improved by  $N_2O$  plasma treatment. An oxidation and nitridation layer with nanostructured grains is formed on the surface of the stuffed W barrier, as shown in Fig. 13b. Relatively low diffusion coefficients are found. No Cu silicide compound is observed for Cu/W( $N_2O$ )/Si sample after annealing at 700°C for 30 min because nanostructured and stuffed barrier can effectively impede Cu diffusion.



Figure 13. Schematic illustrations of the microstructures of (a) Cu/W/Si and (b) Cu/W( $N_2O$ )/Si samples before and after annealing.

## Conclusion

The effectiveness of W(N<sub>2</sub>O) films as diffusion barriers between Cu and Si has been investigated. W(N2O) films, which have amorphous and nano-grained surface layers, show high thermal stability, low resistivity, low surface roughness, low tensile stress, and better adhesion with Cu. W(N<sub>2</sub>O) barriers show excellent barrier capabilities against Cu diffusion. Cu/W( $N_2O$ )/n<sup>+</sup>-p junction diodes retain leakage current densities less than  $10^{-8}$  A/cm<sup>2</sup> even after annealing at 600°C. Copper diffusion in W and W(N2O) barriers is further analyzed using the Whipple analysis of grain boundary diffusion and Fick's diffusion law. Both lattice and grain boundary diffusivities of Cu diffusion in W and  $W(N_2O)$  barriers are extracted from the Cu concentration profiles after annealing the samples at 600-700°C. Grain boundary diffusion coefficients of Cu in sputtered W films are  $6.5 \times 10^{-14} \sim 6.1 \times 10^{-13}$  cm<sup>2</sup>/s. Relatively low diffusion coefficients are found in W(N2O) barriers because oxidation and nitridation layers with nano grains are formed at the surface of the stuffed W barriers after N2O plasma treatments.

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