channel estimation is used. The $f_{d} T$ of fading channels is 0.000723 in this simulation. All receivers in this simulation adopt pilot symbols for channel estimation and a Rake structure for the multipath fading channel. The SRM receiver does not need an additional training sequence by setting the tap weight of a desired user to 1 in the initial state.

Fig. 3 shows a comparison of BER performance among three CDMA receivers, in which the MMSE receiver models the modified MMSE receiver in [1] with a fractionally spaced filter with a tap spacing four times smaller than the chip duration. Setting $E_{b} / N_{0}$ to 15 dB , the MMSE receiver achieves 5.8 dB gain in BER over that of a conventional receiver (MF), while the SRM receiver has gain of 17.8 dB . Another simulation result shows that the SRM receiver also outperforms other receivers in a lower signal-to-interference ratio ( $K=25$ ).

From the results, it is clear that the SRM receiver significantly outperforms all other MMSE receivers. A potential issue is that the SRM receiver requires a function-based base station structure, which needs a high-speed router to link between each functional module.

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## Transformation from 512-point transform coefficients to 256 -point transform coefficients for Dolby AC-3 decoder

Szu-Wei Lee and Chi-Min Liu
The Dolby AC-3 standard defines 512 -point and 256 -point transforms to provide high audio quality when signals rapidly change in time. This authors provide theoretical derivations and proofs for the transformation from 512-point transform coefficients to 256 -point transform coefficients.

Introduction: The Dolby AC-3 is currently the HDTV audio standard and is widely used in DVD films [1]. While the AC-3 draft has been frozen, the standard defines one 512-point (referred to as the long transform) and two 256 -point transforms (referred to as the first and second short transforms) to improve coding quality for signals which rapidly change in time. However, since the transforms are of differing lengths, this increases the difficulty of implementing channel operations in the frequency domain. Channel operations, such as downmixing and channel reduction, are linear operations that mix numbers of channels to another channel. The objectives of performing channel operations in the frequency domain are frequency selection for flexible computational complexity, and equalisation for sound enhancement. Since the transforms adopted in AC-3 can be 512 -point or 256 -point, channel operations cannot mix the channels encoded by the short transforms with those encoded by the long transform. This Letter develops a transform matrix, denoted by $V$, to transform the coefficients of the long transform to those of the short transforms. As a result, the channels encoded by the long transform are pre-processed by matrix $V$ so that channel operations can mix them with those encoded by the short transforms.

Overview of AC-3 transform process: The long transform is the time domain aliasing cancellation (TDAC) filter bank proposed in [2], but the short transforms are slightly different. Fig. 1 outlines the AC-3 transform process. The transform process comprises four modules: overlapping-windowing (OW), forward modified discrete cosine transform (MDCT), backward MDCT and windowing overlapping-and-adding (WOLA)


Fig. 1 Transform process of AC-3

For forward transforms, each audio block containing 512 overlapping samples, which overlaps the second half of the previous audio block, is multiplied by analysis window $h(n)$ to produce 512 windowing samples. The 512 windowing samples can be transformed by either one $256 \times 512$ forward MDCT (hereafter referred to as $L$ ) for the long transform, or two $128 \times 256$ forward MDCTs (referred to as $S_{1}$ and $S_{2}$ ) for the short transforms. As a result, the forward transforms produce 256 frequency coefficients or two sets of 128 frequency coefficients.

For backward transforms, the 256 frequency coefficients are transformed by a $512 \times 256$ backward MDCT (referred to as $L^{+}$), or the two sets of 128 frequency coefficients are transformed by two $256 \times 128$ backward MDCTs (referred to as $S_{1}{ }^{+}$and $S_{2}{ }^{+}$). The backward MDCTs result in 512 windowing samples. The 512 windowing samples are multiplied by synthesis window $f(n)$ to produce 512 overlapping samples. The first half of the 512 overlapping samples are then overlapped and added to the second half of the previous 512 overlapping samples. Finally, the 256 time samples are reconstructed.

Notation: $L^{+}$is a $512 \times 256$ matrix and each entry $n k$ of $L^{+}$is defined by

$$
\left\langle L^{+}\right\rangle_{n k}=\cos \left(\frac{\pi}{1024}(2 n+1)(2 k+1)+\frac{\pi}{4}(2 k+1)\right)
$$

We further decompose $L^{+}$into two square matrices, i.e.

$$
L^{+}=\left[\begin{array}{l}
L_{1}^{+} \\
L_{2}^{+}
\end{array}\right]
$$

where $L_{1}{ }^{+}$and $L_{2}{ }^{+}$are $256 \times 256$ matrices. $S_{1}{ }^{+}$and $S_{2}{ }^{+}$are $256 \times$ 128 matrices. Each entry $n k$ of $S_{1}{ }^{+}$is defined by

$$
\left\langle S_{1}^{+}\right\rangle_{n k}=\cos \left(\frac{\pi}{512}(2 n+1)(2 k+1)\right)
$$

and each entry $n k$ of $S_{2}^{+}$is defined by

$$
\left\langle S_{2}^{+}\right\rangle_{n k}=\cos \left(\frac{\pi}{512}(2 n+1)(2 k+1)+\frac{\pi}{2}(2 k+1)\right)
$$

$S_{1}$ and $S_{2}$ are transpose matrices of $S_{1}+$ and $S_{2}{ }^{+}$, respectively, with dimensions $128 \times 256$. H and F are $512 \times 512$ diagonal matrices with entries $\langle H\rangle_{n n}=h(n)$ and $\langle F\rangle_{n n}=f(n)$. Also, partitioning matrices $H$ and $F$ into two parts yields

$$
H=\left[\begin{array}{cc}
H_{1} & 0 \\
0 & H_{2}
\end{array}\right] \quad \text { and } \quad F=\left[\begin{array}{cc}
F_{1} & 0 \\
0 & F_{2}
\end{array}\right]
$$

$Y_{f}$ is a $256 \times 1$ vector denoting the frequency coefficients of the long transform. $Y 1_{f}$ and $Y 2_{f}$ are $128 \times 1$ vectors, where $Y 1 f$ denotes the frequency coefficients of the first short transform, $Y_{f}$ denotes the coefficients of the second short transform, and subscript $f$ is the block number. $X_{f}$ and $\tilde{X}_{f}$ represent the original and reconstructed time domain signals, respectively.

Derivation: Since the transforms adopted in the AC-3 satisfy the perfect reconstruction constraint, the original time domain signal $X_{f}$ can be obtained from the synthesis signal $\tilde{X}_{f}$, i.e.

$$
X_{f}=\tilde{X}_{f}=\left[\begin{array}{l}
\tilde{X} 1_{f} \\
\tilde{X} 2_{f}
\end{array}\right]
$$

and

$$
\begin{gather*}
\tilde{X} 1_{f}=\left\{\begin{array}{l}
F_{1} \cdot L_{1}^{+} \cdot Y_{f}+F_{2} \cdot S_{2}^{+} \cdot Y 2_{(f-1)} \\
\text { if previous block adopts short transforms } \\
F_{1} \cdot L_{1}^{+} \cdot Y_{f}+F_{2} \cdot L_{2}^{+} \cdot Y_{(f-1)} \\
\text { if previous block adopts long transform }
\end{array}\right.  \tag{1}\\
\tilde{X} 2_{f}=\left\{\begin{array}{c}
F_{2} \cdot L_{2}^{+} \cdot Y_{f}+F_{1} \cdot S_{1}^{+} \cdot Y 1_{(f+1)} \\
\text { if next block adopts short transforms } \\
F_{2} \cdot L_{2}^{+} \cdot Y_{f}+F_{1} \cdot L_{1}^{+} \cdot Y_{(f+1)} \\
\text { if next block adopts long transform }
\end{array}\right. \tag{2}
\end{gather*}
$$

Theorem (i): The following matrices, $Z_{1}, Z_{2}, Z_{3}$ and $Z_{4}$, are zero matrices, where $Z_{1}, Z_{2}, Z_{3}$ and $Z_{4}$ are defined by $Z_{1}=S_{1} \cdot H_{1} \cdot F_{2}$ $S_{2}{ }^{+}, Z_{2}=S_{1} \cdot H_{1} \cdot F_{2} \cdot L_{2}{ }^{+}, Z_{3}=S_{2} \cdot H_{2} \cdot F_{1} \cdot S_{1}{ }^{+}$, and $Z_{4}=S_{2}$ $H_{2} \cdot F_{1} \cdot L_{1}{ }^{+}$.

Proof of theorem ( $)$ : Let $z 1(k 1, k 2)$ be the entry of the matrix $Z_{1}$, i.e.

$$
\begin{align*}
z 1(k 1, k 2)= & \sum_{n=0}^{255} \cos \left(\frac{\pi}{1024}\left(4 k_{1}+2\right)(2 n+1)\right) h(n) f(256+n) \\
& \times \cos \left(\frac{\pi}{1024}\left(4 k_{2}+2\right)(2 n+1+256)\right) \tag{3}
\end{align*}
$$

Since the analysis window $h(n)$ and synthesis window $f(n)$ are equal and have the symmetry property, eqn. 3 can be rewritten as

$$
\begin{align*}
& z 1(k 1, k 2)= \\
& \sum_{n=0}^{255}\left[h(n) h(256-1-n) \cos \left(\frac{\pi}{1024}\left(4 k_{1}+2\right)(2 n+1)\right)\right. \\
& \left.\quad \times \cos \left(\frac{\pi}{1024}\left(4 k_{2}+2\right)(2 n+1+256)\right)\right] \tag{4}
\end{align*}
$$

We now partition the summation term in eqn. 4 into two groups. Each has 128 terms.

$$
\begin{align*}
& z 1(k 1, k 2)= \\
& \sum_{n=0}^{127}\left\{h(n) h(256-1-n) \cos \left(\frac{\pi}{1024}\left(4 k_{1}+2\right)(2 n+1)\right)\right. \\
& \left.\quad \times \cos \left(\frac{\pi}{1024}\left(4 k_{2}+2\right)(2 n+1+256)\right)\right\} \\
& +\sum_{n=128}^{255}\left\{h(n) h(256-1-n) \cos \left(\frac{\pi}{1024}\left(4 k_{1}+2\right)(2 n+1)\right)\right. \\
& \left.\quad \times \cos \left(\frac{\pi}{1024}\left(4 k_{2}+2\right)(2 n+1+256)\right)\right\} \tag{5}
\end{align*}
$$

Replacing the index $n$ in the second group by (255-n), we obtain

$$
\begin{align*}
& z 1(k 1, k 2)= \\
& \sum_{n=0}^{127}\left\{h(n) h(256-1-n) \cos \left(\frac{\pi}{1024}\left(4 k_{1}+2\right)(2 n+1)\right)\right. \\
& \left.\quad \times \cos \left(\frac{\pi}{1024}\left(4 k_{2}+2\right)(2 n+1+256)\right)\right\} \\
& +\sum_{n=0}^{127}\left\{h(n) h(256-1-n) \cos \left(\frac{\pi}{1024}\left(4 k_{1}+2\right)(512-1-2 n)\right)\right. \\
& \left.\quad \times \cos \left(\frac{\pi}{1024}\left(4 k_{2}+2\right)(768-1-2 n)\right)\right\} \tag{6}
\end{align*}
$$

Since the cosine terms satisfy the following properties

$$
\begin{aligned}
& \cos \left(\frac{\pi}{1024}\left(4 k_{1}+2\right)(2 n+1)\right)= \\
& \quad-\cos \left(\frac{\pi}{1024}\left(4 k_{1}+2\right)(512-1-2 n)\right) \\
& \cos \left(\frac{\pi}{1024}\left(4 k_{1}+2\right)(2 n+1+256)\right)=
\end{aligned}
$$

$$
\begin{equation*}
\cos \left(\frac{\pi}{1024}\left(4 k_{2}+2\right)(768-1-2 n)\right) \tag{7}
\end{equation*}
$$

$Z_{1}$ is a zero matrix. For $Z_{2}, Z_{3}$ and $Z_{4}$ the proofs can be carried out similarly.

Theorem (ii): The short transform coefficients can be obtained if the long transform coefficients are known. Specifically, the transform matrix from the coefficients of the long transform to those of the short transforms is described as follows

$$
\left[\begin{array}{l}
Y 1_{f}  \tag{8}\\
Y 2_{f}
\end{array}\right]=V \cdot Y_{f} \quad \text { where } V=\left[\begin{array}{l}
V_{1} \\
V_{2}
\end{array}\right]=\left[\begin{array}{l}
S_{1} \cdot H_{1} \cdot F_{1} \cdot L_{1}^{+} \\
S_{2} \cdot H_{2} \cdot F_{2} \cdot L_{2}^{+}
\end{array}\right]
$$

Proof of theorem (ii): The short transform coefficients can be expressed as

$$
Y_{f}=\left[\begin{array}{ll}
S_{1} & S_{2}
\end{array}\right]\left[\begin{array}{cc}
H_{1} & 0  \tag{9}\\
0 & H_{2}
\end{array}\right] X_{f}
$$

Substituting eqns. 1 and 2 into eqn. 9 and applying theorem (i) yields

$$
\left[\begin{array}{l}
Y 1_{f}  \tag{10}\\
Y 2_{f}
\end{array}\right]=\left[\begin{array}{l}
S_{1} \cdot H_{1} \cdot F_{1} \cdot L_{1}^{+} \\
S_{2} \cdot H_{2} \cdot F_{2} \cdot L_{2}^{+}
\end{array}\right] Y_{f}
$$

Conclusion: In this Letter, we have established the transform matrix that converts the coefficients of long transforms into those of the short transforms. This matrix makes possible the implementation of channel operations in the frequency domain. This work has given the theorems and proofs that support derivation of this matrix.
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## Ultra-low nonlinearity low-loss pure silica core fibre for long-haul WDM transmission

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A new design of pure silica core fibre with an effective area > $110 \mu \mathrm{~m}^{2}$ and attenuation of $0.171 \mathrm{~dB} / \mathrm{km}$ at $1.55 \mu \mathrm{~m}$ has been successfully developed. It exhibits ultra-low nonlinearity and excellent bending loss performance.

Introduction: Recent investigation has shown that a combination of dispersion-unshifted singlemode fibres and dispersion-compensating fibres is one of the most promising transmission line configurations for long-haul WDM (wavelength division multiplexing) transmission systems [ $1-3$ ]. The former fibre, which has relatively large chromatic dispersion at $1.55 \mu \mathrm{~m}$, is effective for reducing fibre nonlinearity effects, such as four-wave mixing, while the latter compensates for the accumulated dispersion. Since dispersioncompensating fibres tend to have slightly higher attenuation than standard fibres, use of low-loss pure silica core fibres (PSCFs) with an attenuation of $0.17-0.18 \mathrm{~dB} / \mathrm{km}$ at $1.55 \mu \mathrm{~m}$ instead of

