Engineering Science Engineers, Part C: Journal of Mechanical Proceedings of the Institution of Mechanical

<http://pic.sagepub.com/>

DOI: 10.1243/0954406991522707 461 Proceedings of the Institution of Mechanical Engineers, Part C: Journal of Mechanical Engineering Science 1999 213: Z-M Ge, C-S Chen, H-H Chen and S-C Lee **Regular and chaotic dynamics of a simplified fly-ball governor**

> <http://pic.sagepub.com/content/213/5/461> The online version of this article can be found at:

> > Published by: **SSAGE**

<http://www.sagepublications.com>

On behalf of:

[Institution of Mechanical Engineers](http://www.imeche.org/home)

Science can be found at: Additional services and information for Proceedings of the Institution of Mechanical Engineers, Part C: Journal of Mechanical Engineering

Email Alerts: <http://pic.sagepub.com/cgi/alerts>

Subscriptions: <http://pic.sagepub.com/subscriptions>

Reprints: <http://www.sagepub.com/journalsReprints.nav>

Permissions: <http://www.sagepub.com/journalsPermissions.nav>

Citations: <http://pic.sagepub.com/content/213/5/461.refs.html>

>> [Version of Record -](http://pic.sagepub.com/content/213/5/461.full.pdf) May 1, 1999

[What is This?](http://online.sagepub.com/site/sphelp/vorhelp.xhtml)

Regular and chaotic dynamics of a simplified fly-ball governor

Z-M Ge*, **C-S Chen**, **H-H Chen** and **S-C Lee**

Department of Mechanical Engineering, National Chiao Tung University, Taiwan

Abstract: The dynamics of a simplified model of a fly-ball speed governor undergoing a harmonic variation about its rotational speed is studied in this paper. This system is a non-linear damped system subjected to parametric excitation. The harmonic balance method is applied to analyse the stability of period attractors and the behaviour of bifurcations. The time evolutions of the response of the non-linear dynamic system are described by time history, phase portraits and Poincaré maps. The regular and chaotic behaviour is observed by various numerical techniques such as power spectra, Lyapunov exponents and Lyapunov dimension. Finally, the domains of attraction of periodic and stranger attractors of the system are located by applying the interpolated cell mapping (ICM) method.

Keywords: governor, bifurcation, chaos, parametric excitation, cell mapping

National Chiao Tung University, 1001 Ta Hsueh Road, Hsinchu 30050, linear systems. Lau *et al.* [9] developed the incremental *Taiwan, Republic of China.* harmonic balance (IHB) method which also deals

- **NOTATION** θ angle between rod and vertical line
	- λ Lyapunov exponent
	- ξ variable of integration in equation (20)
	-
	- **W** approximate transition matrix
	- ω perturbed frequency of the rotational speed
	- Ω_0 constant rotational speed of the fly-ball

1 INTRODUCTION

 $\begin{array}{ll}\nF & -(2\omega_0\ddot{x}_0 + 2\alpha\dot{x}) \\
g & \text{acceleration of gravity} \\
L & \text{Lagrangian} \\
m & \text{total mass of the fly-ball} \\
M & \text{mass of the collar} \\
P & -\sin x_0\n\end{array}$ oidal forcing and a substantial understanding of the complicated phenomena that can arise from these appar-*R*

length of the rod
 V

Lyapunov function
 w

and speed of the fly-ball
 x

and speed of the fly-ball
 x

and speed of the fly-ball
 x

defined as θ

and α
 α and α and α and α and α are by numerical techniques such as phase portraits, Poincaré maps, power spectrum and Lyapunov exponents $[1-3]$.
Harmonic balance (HB) methods $[6-9]$ are suited to

 $\bar{\epsilon}$ perturbed coefficient of the rotational speed strongly non-linear systems. Ling and Wu [8] have dev-*The MS was received on 2 May 1997 and was accepted after revision* eloped the fast Galerkin (FG) method which provides *for publication on 30 July 1998*. *for publication on 30 July 1998.* an efficient and accurate basis for the analysis of non- ** Corresponding author: Department of Mechanical Engineering,* harmonic balance (IHB) method which also deals

incrementation is followed by a Galerkin approximation. a variation when the load of the engine changes; hence These methods are applied to parametric studies for the the governor must change speed with variation in load. purpose of seeking parameter diagrams by changing the It is assumed that the fly-ball governor rotates at consystem parameters in turn. The multivariable Floquet stant speed and undergoes a variation with a harmonic theory [**6**, **7**] is applied to analyse the stability of periodic term, i.e. $w = \Omega_0 - \bar{\varepsilon}\Omega_0 \cos \omega t$, and then (1) becomes solutions through the module of eigenvalues of the associated monodromy matrix of the system.

It is well known that different initial conditions may lead to different attractors in a non-linear system. Often, stable and unstable attractors are coexistent. The attractors and corresponding basins of attraction of Often, stable and unstable attractors are coexistent. The where $2\alpha = c/m$, $\gamma = g/R$, $f = \Omega_0^2$. For simplicity, the $\bar{\varepsilon}^2$ attractors and corresponding basins of attraction of term is neglected, $x = \theta$ is defined and a non-linear system can be located by the method of becomes interpolated cell mapping [**9**, **10**], which has been demonstrated over the past few years to high advantage *in exploring global non-linear behaviour.* The domains of attraction of the period and chaotic attractor with
respect to initial conditions are investigated by inter-
polated cell mapping techniques in this paper.

The fly-ball speed governor (Watt governor) is shown in Parametrically excited dynamic system (3) with the Fig. 1. For simplicity, it is assumed for the system that: chosen parameters

- 1. The masses of the collar and of the rods are neglected.
- 2. Viscous damping in the rod bearing of the fly-ball is presented by damping constant c .

$$
\ddot{\theta} + \frac{c}{m}\dot{\theta} + \frac{g}{R}\sin\theta = \frac{w^2}{2}\sin 2\theta\tag{1}
$$

In most cases the governor is required to rotate at constant speed and the governing device should therefore

Fig. 1 Physical model of a fly-ball governor system Lyapunov fractal dimension).

Proc Instn Mech Engrs Vol 213 Part C C03497 © IMechE 1999

with strong non-linearities. In the IHB method the govern 'isochronously'. However, the speed will undergo

$$
\ddot{\theta} + 2\alpha \dot{\theta} + \gamma = \frac{f}{2} \sin 2\theta - \bar{\varepsilon} f \cos \omega t \sin 2\theta + O(\bar{\varepsilon}^2)
$$
\n(2)

$$
\ddot{x} + 2\alpha \dot{x} + \gamma \sin x = \frac{f}{2} \sin 2x - \bar{\varepsilon} f \cos \omega t \sin 2x \qquad (3)
$$

2.2 Lyapunov exponents and Lyapunov dimension 2 FLY-BALL GOVERNOR WITH A SIMPLE

MODEL The Lyapunov exponents for the system under consideration can be obtained numerically. The algorithm for calculation of the Lyapunov exponents has been **2.1 Mathematical model** described in detail by Wolf *et al.* [**11**].

$$
\ddot{x} + 1.4\dot{x} + 4\sin x = \frac{f}{2}(1 - \cos 8t)\sin 2x \qquad (\bar{\varepsilon} = 0.5)
$$
\n(4)

The Lagrange equation is derived as follows: possesses three Lyapunov exponents. Figures 2a and b indicate the Lyapunov exponents of the system under various parameters to determine the occurrence of chaotic motion. From Fig. 2a the exponents are

$$
\lambda_1 = -0.1663
$$
, $\lambda_2 = 0$, $\lambda_3 = -1.2337$

and from Fig. 2b the exponents are

$$
\lambda_1 = 0.7035
$$
, $\lambda_2 = 0$, $\lambda_3 = -2.1035$

In this linear damping case the sum of all three Lyapunov exponents is equivalent to the negative damping coefficient in the system, which is independent of the initial conditions and time [**12**]. Thus, the sum of the three Lyapunov exponents for these two cases is always −1.4. The largest Lyapunov exponent is plotted in Fig. 3 with *f* ranging from 0 to 30. It is clear that, when *f* is small, λ_1 is negative and the system is periodic. Furthermore, the values of the exponents approach zero as the solutions change their types. When *f* is increased to 20.76, λ_1 changes from negative to positive values; this is the critical point for the onset of chaotic motion. It is noted that in some intervals of large *f*, for example $f = 22.12$, the exponent becomes negative again and the system is then periodic (see Table 1, where d_f is the

Fig. 2 Lyapunov exponents as a function of the number of drive cycles for (a) $f = 19$ and (b) $f = 23$

Fig. 3 Largest Lyapunov exponent as a function of *f*

solved by the fourth-order Runge–Kutta numerical inte-

phase portraits and Poincaré maps show that the system gration method. The results obtained by Poincaré maps is period 2*T* motion. When $\bar{f}=20.2$ the system is in comparison with phase trajectories are shown in period 8*T* motion, with eight Poincaré points. It can be

2.3 Poincaré map, phase portraits, time history and Figs 4a to f. Note that a pair of period 2*T* motions arise **power spectrum analysis** and invert each other from these figures. One of the orbits that the trajectories are attracted to depends on For each initial condition, differential equation (4) is where the initial conditions are located. When $f = 19$ the

Table 1 Lyapunov exponents and Lyapunov dimension for band power spectrum with some spikes on it, which condifferent values of f in equation (4) firms a chaotic motion of the system.

	14	19	19.5	20.3	25
λ_1 λ $\Sigma_i \lambda_i$ $d_{\rm f}$	-0.1212 -1.2788 -1.4 Period T	-0.1678 -1.2322 -1.4 Period 2T	-0.1297 -1.2703 -1.4 Period $4T$	-0.0246 -1.3753 -1.4 Period 8T	0.69 -2.09 -1.4 2.33 Chaotic

strange attractors for $f = 20.37$ have two inverse chaotic of motion. After that, the system is assumed to be in the attractors, but these two independent attractors are steady state, the velocity for the next 200 points is plotted destroyed when $f = 23$.

19, 20 and 23 are shown in Figs 5a to f. It is clear that in the bifurcation diagram. The solution is a stationthe spectrum of a periodic motion consists only of dis-
ary point at the origin until $f = 4.14$ and supercritical crete frequencies, whereas the spectrum of a chaotic bifurcation occurs. After this bifurcation, a period 1*T* motion is not composed solely of discrete frequencies attractor is generated. When *f* grows through 14.38, a but has a continuous, broad band nature. This noise- symmetry-breaking bifurcation takes place and each like spectrum is characteristic of chaotic systems. From period 1*T* orbit bifurcates into a period 2*T* attractor. Fig. 5b it can be observed that a strong peak occurs at When $f = 19.37$ a period 4*T* solution is generated. After the fundamental frequency together with superharmonic that, there occurs a cascade of period doubling from $f =$ frequencies. The presence of the spectral line at half the 19.37 to 20.36, through which periods of the periodic fundamental frequency shows that the period has now motions become longer and longer: $T \times 2^n$ ($n = 0, 1, \ldots$). doubled, as indicated in Fig. 5d. When the value of f is When $f = 20.36$ the chaotic motion appears. It is noted increased to 23, the response has a continuous, wide that within the chaotic region there is a small interval in

firms a chaotic motion of the system.

2.4 Bifurcation diagram

The bifurcation diagrams in Figs 6 and 7 show the long-term values of the angular displacement and angular velocity respectively, obtained by the fourthorder Runge–Kutta numerical integration algorithm, plotted against the dimensionless excitation amplitude $f \in [0, 30]$, in which the incremental value of *f* is 0.01. seen that with $f = 20.37$ and $f = 23$ the steady state At each value of *f* the first 300 points of the Poincaré
Poincaré orbits of chaotic systems are distinctive. The maps are discarded in order to exclude the transient maps are discarded in order to exclude the transient state The time history and power spectrum analysed for $f =$ is plotted. The period doubling route to chaos is shown

Proc Instn Mech Engrs Vol 213 Part C C03497 © IMechE 1999

Fig. 4 Phase portraits and Poincaré points for (a) $f = 19$; (b) $f = 20.2$; (c), (d) $f = 20.37$; and (e), (f) $f = 23$

sudden end of the chaotic attractor appears at $f = 25.95$. becomes

2.5 Incremental harmonic balance method

be obtained by the IHB method [13], which can deal computer implementation. Here the dimensionless time

which the motion abruptly becomes periodic again. The $\tau = \omega t$ is defined, $\bar{\varepsilon} = 0.5$ and $\beta = f/2$. Equation (3) then

$$
\omega^2 \ddot{x} + 2\alpha \omega \dot{x} + \gamma \sin x - \beta (1 - \cos \tau) \sin 2x = 0 \qquad (5)
$$

where $(·)$ represents a derivative with respect to the The steady state periodic solutions of equation (3) can dimensionless time. The first step in this method is a σ (τ) denote the with strong non-linearity very well and is convenient for current solution of equation (5) corresponding to the , γ_0 and β_0 . A neighbouring

Fig. 5 Time history and power spectrum: (a), (b) period 2*T* motion for $f = 19$; (c), (d) period 4*T* motion for $f = 20$; (e), (f) chaotic motion for $f = 23$

Proc Instn Mech Engrs Vol 213 Part C C03497 © IMechE 1999

Fig. 6 Bifurcation diagram for the Poincaré points of angular displacement

Fig. 7 Bifurcation diagram for the Poincaré points of angular velocity

solution is obtained by adding small increments to the current solution:

$$
x = x_0 + \Delta x, \qquad \omega = \omega_0 + \Delta \omega
$$

$$
\gamma = \gamma_0 + \Delta \gamma, \qquad \beta = \beta_0 + \Delta \beta
$$
 (6)

For a small increment Δx , the non-linear terms sin *x* and $\sin 2x$ of equation (5) can be written as first-order Taylor expansions:

$$
\sin x = \sin x_0 + \cos x_0 \Delta x
$$

$$
\sin 2x = \sin 2x_0 + 2 \cos 2x_0 \Delta x
$$
 (7)

all the non-linear terms, the linearized incremental equa-

$$
\omega_0^2 \Delta \ddot{x} + 2a \omega_0 \Delta \dot{x} + g_1(x_0, \tau) \Delta x
$$

\n= $R + \Delta \omega F + \Delta \gamma P + \Delta \beta Q$ (8) are also called the Floque

$$
g_1(x_0, \tau) = \gamma_0 \cos x_0 - 2\beta_0 (1 - \cos \tau) \cos 2x_0 \tag{9}
$$

$$
R = -[\omega_0^2 \ddot{x}_0 + 2\alpha \omega_0 \dot{x} + g_2(x_0, \tau)] \tag{10}
$$

$$
g_2(x_0, \tau) = \gamma_0 \sin x_0 - \beta_0 (1 - \cos \tau) \cos 2x_0 \tag{11}
$$

$$
F = -(2\omega_0 \ddot{x}_0 + 2\alpha \dot{x})\tag{12}
$$

$$
P = -\sin x_0 \tag{13}
$$

$$
Q = (1 - \cos \tau) \sin 2x_0 \tag{14}
$$

cedure (see the Appendix). parameters.

tion $x_0(\tau)$ has been determined and its local stability is

$$
x = x_0 + \delta x \tag{15}
$$

Inserting equation (15) into equation (5) and neglecting the terms of higher order in δx , the linear variational equation is obtained with periodic coefficients in the fol-
 3 GOVERNOR WITH AN ATTACHED COLLAR
 MASS *M*
 MASS *M*

$$
\omega^2 \delta \ddot{x} + 2a\omega \delta \dot{x} + g_1(x_0, \tau) \delta x = 0 \tag{16}
$$

$$
\dot{\mathbf{X}} = \mathbf{A}(\tau) \mathbf{X} \tag{17}
$$

$$
\mathbf{X} = [\delta \mathbf{x}, \delta \dot{\mathbf{x}}]^{\mathrm{T}}, \qquad \mathbf{A}(\tau) = \begin{bmatrix} 0 & 1 \\ A_{21} & -2a/\omega \end{bmatrix}
$$

$$
A_{21} = -\frac{g_1(x_0, \tau)}{\omega^2}
$$
(18)

Since x_0 is a periodic function of time τ with a period $=\frac{1}{2}$ Since x_0 is a periodic function of time τ with a period $T_q = 2q\pi$, the coefficient matrix $A(\tau)$ has the same period (21)

Proc Instn Mech Engrs Vol 213 Part C C03497 © IMechE 1999

, i.e. $A(\tau + T_q) = A(\tau)$. The stability of a linear periodic system is analysed by the multivariable Floquet– Lyapunov theory with an efficient numerical scheme for computing the transition matrix at the end of one period, $\Phi(T_a, 0)$. Here, the approximate transition matrix

(6)
$$
\Phi(T_q, 0) \text{ is given by the following:}
$$
\n
$$
\text{and} \qquad \Phi(T_q, 0) = \prod_{i=1}^{N_k} \left(\mathbf{I} + \sum_{j=1}^{N_j} \frac{(\Delta_i \mathbf{B}_i)^j}{j!} \right) \tag{19}
$$

$$
\mathbf{B}_{k} = \frac{1}{\Delta_{k}} \int_{\tau_{k-1}}^{\tau_{k}} \mathbf{A}(\xi) d\xi
$$
\n
$$
\sin x = \sin x_{0} + \cos x_{0} \Delta x
$$
\n
$$
\sin 2x = \sin 2x_{0} + 2\cos 2x_{0} \Delta x
$$
\n
$$
\cos 2x = \cos 2x_{0} \Delta x
$$
\n
$$
\cos 2x = \cos 2x - \cos 2x - \cos 2x - \cos 2x = 0
$$
\n(20)

 Δx (7) where N_k is the number of intervals in each period *T*; N_j is the number of terms in the approximation of the Substituting equations (6) and (7) in (5) and neglecting constant matrix \mathbf{B}_i exponential; the *k*th interval is k and its size by $\Delta_k = \tau_k - \tau_{k-1}$; in the *k*th \lim_{k+1} tion is obtained: interval the periodic coefficient matrix $A(\tau)$ is replaced

 σ , τ) Δx **D**
 σ The eigenvalues of the monodromy matrix $\Phi(T_q, 0)$ $= R + \Delta \omega F + \Delta \gamma P + \Delta \beta Q$ (8) are also called the Floquet multipliers (ρ_1 , ρ_2) which can where θ and θ determine the stability of steady state solution. If all the modules of the eigenvalues ρ_k are smaller than unity, the *g* solution is stable. If the module of one of the eigenvalues $R = -[\omega_0^2 \ddot{x}_0 + 2\alpha \omega_0 \dot{x} + g_2(x_0, \tau)]$ (10) ρ_k is larger than unity, the solution is unstable. When (τ) (10) ρ_k is larger than unity, the solution is unstable. When
an eigenvalue ρ_k passes through the unit circle, bifur-) cation occurs.

The solutions obtained by the IHB method in comparison with those obtained by numerical integration are) shown in Figs 8a to c, in which the symbols $(·)$ indicate the solutions obtained by the IHB method and the full curves indicate solutions obtained by numerical inte-The second step of the IHB method is the Galerkin pro- gration. These solutions agree well for the same

From the Appendix, the *qT* period steady state solu-
The different types of bifurcation can be verified by tion $x_0(\tau)$ has been determined and its local stability is calculating the Floquet multipliers of the monodromy investigated by considering the following perturbed solu-
matrix as a function of parameter f as shown in F matrix as a function of parameter f as shown in Fig. 9. tion: To investigate the bifurcation further, a Poincare´ map is used to display the bifurcation diagram in Fig. 10, which shows the steady state Poincaré map.

The mass of the collar is neglected for simplicity in the previous investigation, and it can be seen from the above Equation (16) can be arranged in matrix form as discussion that the simple model of the governor system exhibits complex non-linear and chaotic dynamics. A where with an attached collar will now be studied.

A₂**1 Problem formulation**

Using Lagrange's equation, the differential equation for the system is derived as follows:

(18)
$$
(1+4\beta\sin^2\theta)\ddot{\theta}+2\alpha\dot{\theta}+2\beta\dot{\theta}^2\sin 2\theta+(1+2\beta)\gamma\sin\theta
$$

$$
=\frac{1}{2}(f-2\bar{\varepsilon}f\cos\omega t)\sin 2\theta\tag{21}
$$

Fig. 8 Comparison between the IHB and numerical integration methods for (a) $f = 19$, (b) $f = 20$ and (c) $f = 20.2$

Fig. 9 Floquet multipliers as a function of *f*

Proc Instn Mech Engrs Vol 213 Part C C03497 © IMechE 1999

Fig. 11 Bifurcation diagram for $\bar{\varepsilon} = 0.3$ with 50 initial conditions

where $\beta = M/m$ (mass ratio), $2\alpha = c/m$, $\gamma = g/R$ and **3.2 Numerical simulations and discussion** $f = \Omega_0^2$

$$
(1 + 4\beta \sin^2 \theta)\ddot{\theta} + 2\frac{\alpha}{\omega}\dot{\theta} + 2\beta\dot{\theta}^2\sin 2\theta + \frac{(1 + 2\beta)\gamma}{\omega^2}\sin \theta
$$

$$
= \frac{1}{2\omega^2}(f - 2\bar{\varepsilon}f\cos\tau)\sin 2\theta
$$
(22)

$$
(1 + 4\beta \sin^2 x)\ddot{x} + 2\frac{a}{\omega}\dot{x} + 2\beta \dot{x}^2 \sin 2x + \frac{(1 + 2\beta)\gamma}{\omega^2}\sin x
$$

$$
= \frac{1}{2\omega^2}(f - 2\bar{e}f\cos\tau)\sin 2x
$$
(23)

parameters fixed. The transition from regular to chaotic $\frac{46.12 \text{ and } 46.68}{46.14 \text{ a window of stable orbits appears}}$ motion is considered for the following values of the parameters of the system:

$$
\beta = 0.2, \qquad \omega = 2, \qquad \frac{2\alpha}{\omega} = 1.
$$

$$
\frac{(1+2\beta)\gamma}{\omega^2} = 4, \qquad \bar{\varepsilon} = 0.3
$$

If $\tau = \omega t$, the dimensionless form of equation (21) is The bifurcation structure of the angular velocity compo-
rewritten as structure in which there are two chaotic regions. The solution is a stationary point at the origin until $f=18.72$ and the system undergoes a supercritical bifurcation, whereupon a time periodic solution that is a period *T* Hopf bifurcation is generated. It is evident that, when *f* grows through 23.1, a symmetry-breaking pitchfork bifurcation takes place and each period 1*T* bifurcates With substitution of $\theta = x$, equation (22) becomes into a subharmonic period 2*T*. These motions then undergo a succession of complete period-doubling cascades (flip bifurcation), which eventually merge into the first chaotic region. The boundary crisis can be observed at $f = 26.58$, where it causes the chaotic attractor to be *f*^{*d*} destroyed and results in a period 1*T* solution. It is clear that there are two narrow windows within the second The number of the parameters affecting the system
response is more than two. For example, let the $f = 46.12$ and $f = 46.68$. Figure 12, which is an enlarge-
rotational speed be the control parameter with the other
naramet

4 GLOBAL ANALYSIS BY THE INTERPOLATED CELL MAPPING METHOD

In the study of non-linear dynamic systems the influence of initial conditions on system behaviour plays an

Fig. 12 Enlargement of the bifurcation diagram in Fig. 11, showing a period 5*T* window for *f*=46.12*–*46.68

important role. For some system parameters, different initial conditions may lead to different attractors that may be regular or chaotic. Therefore, knowledge about attractors and the domains of attraction is very important when investigating a non-linear system. Attractors and domains of attraction must be delineated in the region of interest in order to characterize the global behaviour of a system.

Considering the case of $f = 18$, equation (4) becomes

$$
\ddot{x} + 1.4\dot{x} + 4\sin x = 9\sin 2x - 9\cos 8t \sin 2x \qquad (24)
$$

To apply the interpolated cell mapping algorithm, the first stage of any computation is to generate the mapping function from a 10 201 (101 \times 101) grid of points distributed in the phase plane using a fourth-order Runge– Kutta integration algorithm. A trajectory is considered to be periodic when the distance between two trajectory uted in the phase plane using a fourth-order Runge–
Kutta integration algorithm. A trajectory is considered
to be periodic when the distance between two trajectory
states is less than 10^{-3} . When no periodic motion occu until 20 interpolation steps, a trajectory is considered
chaotic. **Fig. 13** Domains of attraction for period 2*T* motion of equa-
Figure 13 shows the result obtained by the ICM
 $\frac{1.4}{1.4}$

method applied to equation (24) for the region of interest: −2.3 ≤ *x* ≤ 2.3, −2 ≤ *y* ≤ 2. In Fig. 13 the domain different multiperiodic solutions and cause different of attraction of attractor 1 is denicted by dots, the domains of attraction. In addition, the basins of attr domain of attraction of attractor 2 by the symbol \times and the sink cell by the symbol $+$. in equation (4) are shown in Figs 17 and 18.

It is natural to study similar effects to the basin of attraction for the other parameters that control the system. In this problem, the effects of the damping term **5 CONCLUSIONS** are considered. The values of the coefficient of damping are chosen as 2.0, 1.1 and 0.8 respectively in equation It has been shown that the simplified model of a fly-ball

Proc Instn Mech Engrs Vol 213 Part C C03497 © IMechE 1999

of attraction of attractor 1 is depicted by dots, the domains of attraction. In addition, the basins of attrac-
domain of attraction of attractor 2 by the symbol \times tion of the chaotic attractor when $f = 20.37$ and $f =$

(24). Figures 14 to 16 show that different damping governor exhibits both regular and chaotic motions. values can yield different attractors that correspond to Parametric studies have been performed by the IHB

Fig. 14 Domains of attraction for period 1*T* motion of equa- **Fig. 16** Domains of attraction for chaotic motion of equation tion (24) with a damping value of 2.0 (24) with a damping value of 0.8

tion (24) with a damping value of 1.1

method, the numerical integration method and other on such analyses, many aspects of the dynamic behavanalytical techniques to analyse the behaviour of bifur- iour of this simplified governor model are presented. cation and chaos. With the parametric studies the per- The global behaviour of the systems is obtained by iodic solutions can be clearly guided by the IHB method means of the interpolated cell mapping method (ICM). and their stability is analysed by examining the move- The basins of attraction of the period attractor and ments of eigenvalues of the monodromy matrix. The chaotic attractor are obtained for certain system paramsolutions obtained by the IHB method are found to eters of interest. match exactly those obtained by numerical integration. It must be emphasized that this mathematical model A symmetry-breaking precursor to period-doubling for a fly-ball governor is only a simplified one. The simbifurcation and a cascade of period doubling routes to plifications are not all reasonable, for instance the negchaos are observed in this system. Many of the character- lect of the $O(\bar{\epsilon}^2)$ term in equation (4) for $\bar{\epsilon} = 0.5$. The istics available for detecting chaotic motion such as numerical data used are chosen to enrich the dynamic Lyapunov exponents, Lyapunov dimensions, Poincaré behaviour rather than to agree closely with the practical

Fig. 15 Domains of attraction for period 4*T* motion of equa-
 Fig. 17 Domains of attraction for chaotic motion of equation (24) with $f = 20.37$

maps and power spectra are obtained numerically. Based

Fig. 18 Domains of attraction for chaotic motion of equation **APPENDIX** (24) with $f = 23$

data for actual governors. This paper serves as an intro-
duction to the study of a more precise mathematical duction (8) may be expressed as model of a fly-ball governor.

ACKNOWLEDGEMENT

This research was supported by the National Science Council, Republic of China, under Grant

REFERENCES *x*

- **1 Yagasaki, K., Sakata, M.** and **Kimura, K.** Dynamics of a weakly nonlinear system subjected to combined parametric and external excitation. *Trans. ASME, J. Appl. Mechanics*, 1990, 57, 209. and external excitation. *Trans. ASME, J. Appl. Mechanics*, 1990, **57**, 209. (26)
- **2 Sanchez, N. E.** and **Nayfeh, A. H.** Prediction of bifurcations in a parametrically excited Duffing oscillator. *Int. J. Non*-
 N is the order of the harmonic to be taken into account
- parametric excitation. *Trans. ASME, J. Appl. Mechanics*, coordinates, the following is obtained: 1989, **56**, 947.
- **4 Sekar, P.** and **Marayanan, S.** Periodic and chaotic motions of a square prism in cross-flow. *J. Sound Vibr.*, 1994, $170(1)$, 1. of a square prism in cross-flow. *J. Sound Vibr*., 1994, **170**(1), 1.
- **5 Gottlieb, O.** Bifurcations and routes to chaos in wave-
structure interaction systems. *J. Guidance, Control, and* $Dynamics, 1992, 15(4), 832.$ (27) *Dynamics*, 1992, **15**(4), 832.
- application to determine periodic solution of non-linear
- 7 Lau, S. L. and Yuen, S. W. The Holf bifurcation and limit cycle by the incremental harmonic balance method. *Computer Meth. Appl. Mech. Engng*, 1991, 91, 1109.

Proc Instn Mech Engrs Vol 213 Part C C03497 © IMechE 1999

- **8 Friedmann, P., Hammond, C. E.** and **Woo, T. H.** Efficient numerical treatment of periodic systems with application to stability problems. *Int. J. Numer. Meth. Engng*, 1977, **11**, 1117.
- **9 Tongue, B. H.** On the global analysis of nonlinear system through interpolated cell mapping. *Physica D*, 1987, **28**, 401.
- **10 Tongue, B. H.** and **Gu, K.** Interpolated cell mapping of dynamical systems. *Trans. ASME, J. Appl. Mechanics*, 1988, **55**, 461.
- **11 Wolf, A., Swift, J. B., Swinney, H. I.** and **Vastano, J. A.** Determining Lyapunov exponent from a time series. *Physica D*, 1985, **16**, 285.
- **12 Baker, G. L.** and **Gollub, J. P.** *Chaotic Dynamics: an Introduction*, 1990 (Cambridge University Press).
- **13 Cheung, Y. K., Chen, S. H.** and **Lau, S. L.** Application of the incremental harmonic balance method to cubic nonlinearity systems. *J. Sound Vibr*., 1990, **140**(2), 273.

$$
x_0 = \sum_{j=0,1,2,...}^{N} \left(a_{j/q} \cos \frac{j}{q} \tau + b_{j/q} \sin \frac{j}{q} \tau \right)
$$

$$
\Delta x_0 = \sum_{j=0,1,2,...}^{N} \left(\Delta a_{j/q} \cos \frac{j}{q} \tau + \Delta b_{j/q} \sin \frac{j}{q} \tau \right)
$$
(25)

NSC87-2212-E-009-019.
 NSC87-2212-E-009-019.

for unsymmetrical solution with period $2q\pi$ in terms of
 τ , and as
 $x_0 = \sum_{x=0}^{2N-1} \left(a_{j/q} \cos \frac{j}{2} \tau + b_{j/q} \sin \frac{j}{2} \tau \right)$ τ , and as

$$
x_0 = \sum_{j=1,3,5,...}^{2N-1} \left(a_{j/q} \cos \frac{j}{q} \tau + b_{j/q} \sin \frac{j}{q} \tau \right)
$$

$$
\Delta x_0 = \sum_{j=1,3,5,...}^{2N-1} \left(\Delta a_{j/q} \cos \frac{j}{q} \tau + \Delta b_{j/q} \sin \frac{j}{q} \tau \right)
$$
(26)

Linear Mechanics, 1990, 25(2/3), 163.
3 Szemplinska-Stupnicka, W., Plaut, R. H. and Hsieh, J.-C. and q is the order of the subharmonic. By applying the Been particular statements, \cdots , \cdots , \cdots , \cdots and \cdots and \cdots , \cdots as the generalized \cdots as the generalized \cdots

$$
\int_0^{2q\pi} {\omega_0^2 \Delta \ddot{x} + 2\alpha \omega_0 \Delta \dot{x} + [1 + g_1(x_0, \tau)] \Delta x} \delta(\Delta x) d\tau
$$

$$
= \int_0^{2q\pi} (R + \Delta \omega F + \Delta \gamma P + \Delta \beta Q) \delta(\Delta x) d\tau \qquad (27)
$$

6 Ling, F. H. and **Wu, X. X.** Fast Galerkin method and its Substituting equation (25) [or equation (26)] in equation λ_k and Δb_k terms, an incremenoscillators. *Int. J. Non-Linear Mechanics*, 1987, **22**(2), 89. tal system of 2*N*+1 (or 2*N*) linear equations in terms k and Δb_k is obtained in the form

$$
C\Delta a = \mathbf{R} + \Delta\omega\mathbf{F} + \Delta\gamma\mathbf{P} + \Delta\beta\mathbf{Q}
$$
 (28)

$$
\mathbf{a} = [a_{j/q}, b_{j/q}]^T
$$

\n
$$
\Delta \mathbf{a} = [\Delta a_{j/q}, \Delta b_{j/q}]^T
$$

\n
$$
j = \begin{cases} 0, 1, 2, ..., N \\ 1, 3, ..., 2N - 1 \end{cases}
$$
 for symmetric solution
\n
$$
j = \begin{cases} 0, 1, 2, ..., N \\ 1, 3, ..., 2N - 1 \end{cases}
$$
 for unsymmetric solution
\n
$$
j = \begin{cases} 0, 1, 2, ..., N \\ 1, 2, ..., N \end{cases}
$$

$$
C = \begin{bmatrix} [C_1]_{ij} & [C_{12}]_{ij} \\ [C_{21}]_{ij} & [C_2]_{ij} \end{bmatrix}, \qquad R = \begin{bmatrix} R_{1i} \\ R_{2i} \end{bmatrix}
$$

\n
$$
F = \begin{bmatrix} F_{1i} \\ F_{2i} \end{bmatrix}, \qquad P = \begin{bmatrix} P_{1i} \\ P_{2i} \end{bmatrix}, \qquad Q = \begin{bmatrix} Q_{1i} \\ Q_{2i} \end{bmatrix}
$$

\n
$$
F_{1i} = 2q\pi\mu
$$

\n(30)

The expressions for **C**, **R**, **F**, **P** and **Q** are as follows:

$$
[\mathbf{C}_{1}]_{ij} = \mu_{j} \delta_{ij} q \pi \left[-\left(\frac{j\omega_{0}}{q}\right)^{2} \right] + [\mathbf{C}_{1}]_{ij}^{NL}
$$
\n
$$
(i, j = 0, 1, ..., N) \qquad \qquad \begin{cases} \mathbf{P}_{1i} \\ \mathbf{P}_{2i} \end{cases} = \int_{0}^{2q\pi} -\sin x_{0} \begin{cases} \cos \frac{i\pi}{q} \\ \sin \frac{i\pi}{q} \end{cases} d\tau
$$
\n
$$
[\mathbf{C}_{12}]_{ij} = 2\delta_{ij} q \pi \left(\frac{j\omega_{0}}{q}\right) + [\mathbf{C}_{12}]_{ij}^{NL}
$$
\n
$$
(i = 0, 1, ..., N, j = 1, ..., N)
$$
\n
$$
[\mathbf{C}_{21}]_{ij} = -2\delta_{ij} q \pi \left(\frac{j\omega_{0}}{q}\right) + [\mathbf{C}_{21}]_{ij}^{NL}
$$
\n
$$
(i = 1, ..., N, j = 0, 1, ..., N)
$$
\n
$$
[\mathbf{C}_{21}]_{ij} = \delta_{ij} q \pi \left[-\left(\frac{j\omega_{0}}{q}\right)^{2} \right] + [\mathbf{C}_{2}]_{ij}^{NL}
$$
\nwhere\n
$$
(i, j = 1, ..., N) \qquad \qquad \mathbf{R}_{1i}^{NL} = -\int_{0}^{2q\pi} g_{2}(x_{0}, \tau) \cos \frac{i\tau}{q} d\tau
$$
\nwhere\n
$$
\mathbf{R}_{2i}^{NL} = -\int_{0}^{2q\pi} g_{2}(x_{0}, \tau) \cos \frac{i\tau}{q} d\tau
$$

where

$$
\mu_{j} = \begin{cases}\n2 & \text{for } j = 0 \\
1 & \text{for } j \neq 0\n\end{cases} \quad \delta_{ij} = \begin{cases}\n1 & \text{for } j = j \\
0 & \text{for } i \neq j\n\end{cases} \quad R_{2i}^{NL} = -\int_{0}^{2q\pi} g_{2}(x_{0}, \tau) \sin \frac{i\tau}{q} d\tau
$$
\n
$$
[\mathbf{C}_{1}]_{ij}^{NL} = \int_{0}^{2q\pi} g_{1}(x_{0}, \tau) \cos \frac{i\tau}{q} \cos \frac{j\tau}{q} d\tau
$$
\n
$$
[\mathbf{C}_{21}]_{ij}^{NL} = \int_{0}^{2q\pi} g_{1}(x_{0}, \tau) \cos \frac{i\tau}{q} \sin \frac{j\tau}{q} d\tau
$$
\n
$$
[\mathbf{C}_{21}]_{ij}^{NL} = \int_{0}^{2q\pi} g_{1}(x_{0}, \tau) \sin \frac{i\tau}{q} \cos \frac{j\tau}{q} d\tau
$$
\n
$$
[\mathbf{C}_{2}]_{ij}^{NL} = \int_{0}^{2q\pi} g_{1}(x_{0}, \tau) \sin \frac{i\tau}{q} \sin \frac{j\tau}{q} d\tau
$$

where Elements of matrices **R**, **F**, **P** and **Q**:

$$
\mathbf{a} = [a_{ijq}, b_{ijq}]^{T}
$$
\n
$$
\mathbf{a} = [\Delta a_{jiq}, \Delta b_{jiq}]^{T}
$$
\n
$$
I = \begin{cases}\n0, 1, 2, ..., N \\
1, 3, ..., 2N - 1\n\end{cases}
$$
 for symmetric solution
\n
$$
I = \begin{bmatrix}\nC_{11}l_{ij} & C_{12}l_{ij}\n\end{bmatrix}, \quad \mathbf{R} = \begin{bmatrix}\nR_{11} \\
R_{21}\n\end{bmatrix}
$$
\n
$$
\mathbf{r} = \begin{bmatrix}\nF_{11} \\
F_{21}\n\end{bmatrix}, \quad \mathbf{P} = \begin{bmatrix}\nP_{11} \\
P_{21}\n\end{bmatrix}, \quad \mathbf{Q} = \begin{bmatrix}\nQ_{11} \\
Q_{21}\n\end{bmatrix}
$$
\n
$$
\mathbf{r} = \begin{bmatrix}\nF_{11} \\
F_{21}\n\end{bmatrix}, \quad \mathbf{Q} = \begin{bmatrix}\nQ_{11} \\
Q_{21}\n\end{bmatrix}
$$
\n
$$
\mathbf{r} = \begin{bmatrix}\nF_{11} \\
F_{21}\n\end{bmatrix}, \quad \mathbf{Q} = \begin{bmatrix}\nQ_{11} \\
Q_{21}\n\end{bmatrix}
$$
\n
$$
\mathbf{r}_{11} = 2q\pi\mu_{i} \begin{bmatrix}\n\omega_{0} \left(\frac{i}{q}\right)^{2} a_{i} - \alpha \frac{i}{q} b_{i}\n\end{bmatrix}, \quad i = 0, 1, ..., N
$$
\nThe expressions for **C**, **R**, **F**, **P** and **Q** are as follows:
\nElements of matrix **C**:
\n
$$
F_{21} = 2q\pi \begin{bmatrix}\n\omega_{0} \left(\frac{i}{q}\right)^{2} b_{i} - \alpha \frac{i}{q} a_{i}\n\end{bmatrix}, \quad i = 1, 2, ..., N
$$
\n
$$
[C_{11}l_{ij} = \mu_{j}\delta_{ij} q\pi \begin{bmatrix}\n-\left(\frac{j\omega_{0}}{q}\right)^{2}\right] + [C_{1}l]_{ij}^{NL}
$$
\n
$$
(i, j = 0, 1, ..., N)
$$
\

$$
\mathbf{R}_{1i}^{NL} = -\int_0^{2q\pi} g_2(x_0, \tau) \cos \frac{i\tau}{q} d\tau
$$

$$
\mathbf{R}_{2i}^{NL} = -\int_0^{2q\pi} g_2(x_0, \tau) \sin \frac{i\tau}{q} d\tau
$$

C03497 © IMechE 1999 Proc Instn Mech Engrs Vol 213 Part C

Downloaded from [pic.sagepub.com a](http://pic.sagepub.com/)t NATIONAL CHIAO TUNG UNIV LIB on April 28, 2014