# 國立交通大學

# 光電工程研究所

# 碩士論文



Research on MIS Stacked Solar Cells

研究生:李欣育

指導教授:李柏璁 教授

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# 疊合式金氧半太陽能電池之研究

### 學生:李欣育

#### 指導教授:李柏璁 博士

#### 國立交通大學光電工程研究所碩士班

### 摘、要

在本篇論文當中,首先我們先分析 n 型與 p 型的金氧半太陽能電池。由於我 們是使用磁控濺鍍機來成長超薄穿隧氧化層,大量的缺陷會在濺鍍過程中被製造 出來。於是我們加入一道氫氣退火的製程,以形成矽氫鍵結的方式來修補矽的懸 空鍵。我們同時也調控氧化層厚度、工作壓力、以及用於載子收集之金屬層的厚 度來達到高開路電壓輸出。

隨後,為了實現疊合式金氧半太陽能電池,我們使用晶圓直接接合的方式來 達到穿隧二極體並對其進行分析。最後再將n型與p型金氧半太陽能電池整合到 穿隧二極體上,完成疊合式金氧半太陽能電池並量測其光伏特性。量測結果顯示 最好的開路電壓達到 593mV,大於單一接面的金氧半太陽能電池,證明我們所提 出來的結構之可行性以及其用在電解水的潛力

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# Research on MIS Stacked Solar Cells

student : Hsin-Yu Lee

Advisors : Dr. Po-Tsung Lee

Institute of Electro-Optical Engineering, National Chiao Tung University



In this thesis, the n-type and p-type MIS solar cells are investigated first. Since we use sputter to deposit tunnel oxide as insulating layer, a lot of defects are produced during sputtering. Therefore, we introduce an annealing process in hydrogen atmosphere to passivate Si dangling bonds by the formation of Si-H bonds. We also fine tune the oxide thickness, working pressure, and collecting thin metal thickness to achieve high  $V_{oc}$ .

Later, to realize MIS stacked solar cells, we fabricate and investigate the tunneling junction by directly wafer bonding. Finally, we integrate n-type and p-type MIS junctions on bonded sample and measure the photovoltaic properties of MIS stacked solar cells. Consequently, the best Voc we obtain is 593mV, larger than single junction cells, demonstrating that the structure is practical and have its potential to achieve water splitting.

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# **Chapter 1 Introduction**

### 1.1 Background

In recent years, due to the greenhouse effect and energy crisis, much effort has been made on the research and development of renewable energy. Renewable energy is energy generated from natural resources such as solar, wind, tides, geothermal heat and so on. The distinguishing feature of solar energy is that it produces eternal and enormous energy about 1000W/m<sup>2</sup> without local limitation and pollution. Therefore, only solar energy among these renewable energies is much more promising and potential for worldwide usage.



### **1.2** MIS Solar Cells

### **1.2.1 General Description**

The first solar cell using diffused p-n junction was fabricated at Bell Laboratory in the early 1950's while the sunlight energy conversion efficiency is only around 6 percent with ultra high cost. In 1970 the first highly effective GaAs heterostructure solar cells were created by Zhores Alferov and his team in the USSR<sup>[1,2]</sup>. However, the cost of III-V semiconductor substrate limits the application only in outer space. To replace fossil fuel, the reduction of the cost-per-Watt ratio has been a primary work in solar cells fabrication ever since then. The metal-insulator-semiconductor (MIS) solar cells have received much attention in the decades because of the simple and low-temperature fabrication process and the comparable high efficiency to diffused p-n junction solar cells<sup>[3-9]</sup>. The high-temperature junction diffusion step is completely eliminated in these devices. Therefore, MIS solar cells are candidates for drastically reducing the cost-per-Watt ratio of solar electricity.

In early years, the MIS solar cells can be fabricated by deposited a layer of low work function metal on the top of p-type semiconductor with a thin insulating layer in between. Due to the formation of Schottky barrier, at the surface of semiconductor, electrical field is formed, and the separation of excitons is possible. When the light incident on the cells, majority carriers and minority carriers generate at the surface field; the majority carrier blocked by the insulator while the minority carriers are able to flow through by quantum mechanical tunneling if this layer is sufficient thin. However, a major disadvantage of MIS solar cells with semi-transparent metal layer is that the thin metal layers reflect light and there is a trade-off between carrier production and collection. To overcome this problem, grating-type MIS solar cells with only collecting grid fingers are invented.

Although a simple MIS structures have photovoltaic properties, several treatment have been done in order to improve the performance of MIS solar cells. If an inversion layer is induced by the presence of insulator charges, the larger depletion region separate carriers efficiently and larger conversion efficiency could be expected. This kind of device is called an MIS inversion layer (MIS-IL) solar cells. The following sections briefly review the researches nowadays<sup>[3,10]</sup>.

### **1.2.2 First-Generation MIS-IL Solar Cells**

The cross-section of the first generation MIS-IL solar cell, including bifacial sensitivity, is shown in Fig 1.1. The inversion layer is induced by fixed positive charges present in the transparent insulator film<sup>[4-8]</sup>, which covers both the silicon surface and the MIS contacts. In order to increased fixed charges in film, cell has to dip in cesium solution<sup>[10]</sup> and cesium ion cans easily be caught in the trap. Though cell degradation after cesium dip is faster, the following SiN layer can serve as a passivation layer and reduce the surface recombination<sup>[3,10]</sup>. In this structure, the ultrathin oxide layer (<2nm) blocks majority carrier (hole) currents injected into the metal at forward bias and reduces surface recombination. Therefore, a higher open circuit voltage of MIS solar cells than that of Schottky barrier solar cells can be achieved.



Fig 1.1: The cross-section of the first generation MIS-IL solar cell with bifacial

sensitivity



The first-generation MIS-IL solar cells have a high conversion efficiency approach 20%, but the surface recombination velocity at the surface is still large due to low temperature PECVD SiN passavation<sup>[3,10]</sup>. From the simulation with PC-1D<sup>[3]</sup>, the open circuit voltage can increase by 20-40mV with SiN deposition temperature increasing from 250°C to 400°C. In second-generation MIS-IL solar cells, some treatments are done in order to further increase the efficiency as follows:

- (a) Formation of special texture on semiconductor surface;
- (b) Better surface passivation by high temperature deposited film before electrode deposition;

(c) Smaller contact area on the top of texture after removal of passivation layer.

Two types of second-generation MIS-IL solar cells are shown in Fig. 1.2 and Fig.

1.3



Fig. 1.2: Figure of a truncated-pyramid MIS-IL silicon solar cell



Fig. 1.3: Figure of a wire-grooved ART (Abrased-Ridge-Top) solar cell

### **1.2.4** MIS-n<sup>+</sup>p Solar Cells (MINP)

This kind of cells deposit Aluminum electrode on conventional diffused p-n junctions with thin tunneling oxide in between, resulting in hybrid MIS-n<sup>+</sup>p solar cells<sup>[3]</sup>. The MIS structure creates another junction to enhance the efficiency of p-n junction and surface recombination velocity can also be reduced by the thin tunneling oxide. Furthermore, with aluminum in substitution for silver electrode lowers the costs for mass production.



Fig 1.4: Schematic cross-section of the bifacial MIS-n<sup>+</sup>p solar cell (MINP)

### **1.3** MIS Stacked Solar Cells

Although the conversion efficiency of MIS solar cells can be compared with conventional diffused p-n junction cells, based on detail balanced limit, the upper limit of energy conversion efficiency of ideal photovoltaic devices with one energy band-gap is about 31.0%. That is to say, there is much more energy loss so far in this kind of devices. To overcome this drawback, one of favorable high efficiency photovoltaic devices, stacked solar cells, has been demonstrated<sup>[11-13]</sup>. Stacked solar cells not only provide high energy conversion efficiency, but supply high open circuit voltage as well due to the electrically cascade of two current balanced solar cells. High voltage output lowers the ohmic losses at series resistance inside and outside the stacked cells. In addition, it makes possible the combination of photovoltaic-electrolysis system for hydrogen production with single cell in reality.

For an ideal stacked solar cell, all photo-generated carriers in the central sub-cells of the stacked solar cell can be efficiently recombined at the tunnel junctions. That is to say, current matching between sub-cells is an important issue to enhance the efficiency of stacked cells.

### 1.4 Motivation

In recent years, solar cells and fuel cells are seen as potential devices to overcome the problem of energy crisis. The combination of solar cells and fuel cell is an efficient way to construct a pollution-free energy providing system. Solar cells convert sun light to electricity during the day, and the remained electricity is converted into hydrogen by splitting water; fuel cells generate electricity from saved hydrogen at night.

In order to generate hydrogen by water splitting, a theoretic of at least 1.23V

voltage output is necessary, which can be achieved by stacked cells. Besides, to simplify the fabrication process and design consideration, MIS solar cell is a potential structure. Therefore, a series of experiment on MIS stacked solar cells have been done in this thesis.

# **1.5** About this work

In this work, three different junctions have been investigated, respectively. We use direct wafer bonding to achieve the tunneling diode with an n-type wafer and a p-type wafer. We also study the characteristics of MIS solar cells fabricated on n-type and p-type silicon wafer individually. Finally, we combine these two components to achieve a MIS stacked solar cell and study its photovoltaic properties.

# **Chapter 2 Principle of MIS solar cells**

### 2.1 General Description of solar cells

For a solar cell, the current-voltage (I-V) characteristics in dark and under illumination are the most important method to evaluate a solar cell. While the cell is exposed to AM 1.5, only incident photons with energy larger than the energy bandgap  $E_g$  of active layer can be absorbed and generate electron-hole pairs. Electron-hole pairs in depletion region or diffused into depletion region are separated by internal electric field and then collected by electrodes, afterwards.

In the dark, the current-voltage (I-V) characteristics of an ideal p-n junction solar cell which acts just like an ideal diode is given by

$$I = I_s (e^{qV_a/kT} - 1)$$
 (Eq. 2.1)

where I<sub>S</sub> referred to as the reverse saturation current of the diode, V<sub>a</sub> is the applied voltage,  $q = 1.6 \times 10^{-19}$  C is the fundamental unit of charge,  $k = 1.38 \times 10^{-23}$  J/K is the Boltzmann's constant, and T is the absolute temperature. Fig 2.1 shows the energy-band diagram of a conventional p-n junction solar cell under solar illumination and the ideal equivalent circuit of the p-n junction solar cell under solar irradiation.



Fig 2.1: (a) band diagram of a conventional p-n junction solar cell under illumination (b) the ideal equivalent circuit of the p-n junction solar cell under solar irradiation

A light-generated current source  $I_L$  parallel with the junction, and then the current-voltage (I-V) curve simply shifted down. The behavior under illumination is represented by

$$I = I_s (e^{qV_a/kT} - 1) - I_L$$
 (Eq. 2.2)

The representative current-voltage (I-V) characteristics of a solar cell in the dark

and under illumination are shown in Fig. 2.2.



Fig. 2.2: I-V characteristics of a solar cell in the dark and under illumination



Since a solar cell is a power source, the output power equals to the product of the

voltage and current on a working point of the illuminated I-V curve. On the curve, there is a working point corresponding to maximum power output denoted as  $P_{max}$  (shown in Fig 2.2). Also, we identify the open circuit voltage  $V_{oc}$  which is related to the separation of quasi-Fermi levels in Fig 2.1(a) as the voltage across the illuminated cell with infinity load resistance. The short circuit current density,  $I_{SC}$ , is the current through the illuminated cell if the load resistance is zero. The maximum power is obtained at the voltage  $V_{max}$  and corresponding  $I_{max}$ . Therefore, fill factor FF can be expressed as

$$FF = \frac{V_{max} \times I_{max}}{V_{oc} \times I_{sc}} \qquad (Eq. \ 2.3)$$

And the power conversion efficiency  $\eta$  which is defined as the ratio of the output electrical power to the incident optical power, is given by

$$\eta = \frac{P_m}{P_{in}} = \frac{V_{max} \times I_{max}}{P_{in}} = \frac{FF \times V_{oc} \times I_{sc}}{P_{in}} \qquad (Eq. \ 2.4)$$

From Eq. 2.4, to enhance the conversion efficiency, three important parameters,

V<sub>oc</sub>, I<sub>sc</sub> and FF have to be put into consideration:

- (a) For  $I_{sc}$  enhancement, well designed collection fingers help the extract of photo current and anti-reflection coating can improve the production of photo current.
- (b) For  $V_{oc}$  enhancement, because  $V_{oc}$  is related to the built-in potential of the junction, material choosing is the first consideration. Furthermore, the recombination defects in junctions should be passivated not to reduce the  $V_{oc}$ . (c) Furthermore, the closer to unity FF is the better the conversion efficiency of a solar cell, while the fill factor FF corresponds to contact formation and carrier collection efficiency.

Air mass is the optical path length through Earth's atmosphere for light from the sun. As it passes through the atmosphere, light is attenuated by scattering and absorption; the more atmosphere through which it passes, the greater the attenuation. For a thickness  $L_0$  of the atmosphere, the path length L through the atmosphere for solar radiation incident at angle  $\theta$  relative to the normal to the Earth's surface is  $L = L_0 / \cos \theta$ . The region above Earth's atmosphere, where there is no atmospheric attenuation of solar

radiation, is considered to have "air mass zero" (AM0). Similarly, the solar radiation after traveling through the atmosphere to sea level is referred to as AM1. However, the radiation angle of the sun changes with latitude and even from time to time. Consequently, AM1.5g, corresponding to a solar zenith angle of 48° and equals to 1000W/m<sup>2</sup>, is almost universally used to characterize solar cells at the Earth's surface.

### 2.2 Transport Mechanism of MIS Junctions

In 1938, Walter H. Schottky suggested that a potential barrier could arise from a metal-semiconductor also diode known as Schottky diode. The current transportation for a Schottky diode is mainly due to majority carrier as opposed to minority carrier in p-n junction. The current density can be represented as

$$J = J_s (e^{qV/nkT} - 1)$$

where  $J_S$  is the reverse saturation current density,  $q = 1.6 \times 10^{-19}$  C is the fundamental unit of charge, n is the ideality factor,  $k = 1.38 \times 10^{-23}$  J/K is the Boltzmann's constant, and T is the absolute temperature. The above equation is identical in the form to the equation of the p-n junction. However, the thermionic emission current is mainly due to majority carrier while p-n junction is due to minority carrier. Therefore, a smaller turn-on voltage can be expected in Schottky diode. For solar cell application, low turn-on voltage and the interface states of a Schottky diode will

degrade cell performance, so a thin insulating layer is introduced into the interface.

In the following paragraphs, seven regions of the J-V characteristics of an MIS solar cell with p-type semiconductor in dark and under illumination will be explained with  $J_m$  (current density flows from metal to semiconductor by thermionic emission),  $J_s$  (current density flows from semiconductor to metal by thermionic emission) and  $J_e$  (photo electron tunneling current density with help of traps).

#### (a) Dark — forward bias (negative bias at metal)

When the MIS diode is under forward bias, band near the junction bend upward. This band bending causes an accumulation of majority carriers (holes) near the oxide-semiconductor interface. For Schottky barrier diode, the thermionic emission current can easily pass through MS junction and result in high dark current. However, these carriers should pass the oxide with the assistance of traps existed in the oxide or tunneling for MIS junction with sufficient thin oxide. Therefore, exponential rising of the current with applied forward bias can be expected. As shown in Fig 2.3(a), the total current density

$$J = J_s - J_m \cong J_s \propto e^{qV/nkT}$$



Fig 2.3: (a) Band diagram and current flow of a MIS solar cell under forward bias in

### dark (b) Charge distribution at accumulation region

#### (b) Dark — zero bias

When the MIS solar cell is zero biased, the net current is zero due to thermal

equilibrium.

$$J = J_s - J_m = 0$$

As shown in Fig 2.4(a), a depletion region formed near the surface of semiconductor. In MIS junction, depletion region is always smaller than p-n junction, so how to enlarge the depletion region by fixed charges in insulator is a most important issue.



Fig 2.4 (a): Band diagram and current flow of a MIS solar cell under zero bias in dark (b)

Charge distribution at depletion region

### (c) Dark — reversed bias



appearance of inversion layer and reduced thermionic emission from semiconductor. Under this bias condition, the total current in cell is determined by  $J_{\text{m}}$  component which reaches saturation at large reverse bias, as shown in Fig 2.5(a)

$$J = J_s - J_m \cong -J_m \cong const.$$



Fig 2.5: (a) Band diagram and current flow of a MIS solar cell under reversed bias in



When the MIS solar cell under illumination is forward biased, the  $J_s$  and  $J_m$  flow as same as that in dark. Besides, photo-generated electrons will flow into semiconductor along with the direction of electric field. The electrons in metal can also pass through the oxide under the assistance of the traps in the oxide. This current component is denoted as Je as shown in Fig 2.6. Under such condition, the total current is increased by Je and then total current density

$$J = J_s - J_m + J_e \cong J_s + J_e$$



Fig 2.6: Band diagram and current flow of a MIS solar cell which is large forward

biased under illumination



# (e) Illuminated — zero current (open circuit)

If the positive bias voltage decreases, the Je component decreases due to the decrease of electric field in the oxide. As bias voltage decreases to a certain extent, the slope of band bending changes from positive to negative, corresponding to the change of the direction of electric field, and then the electrons flowing from semiconductor to metal emerge with the assistance of oxide traps. This current component, denoted as Je, will cancel the net thermionic emission current and the total current density

$$J = J_s - J_m - J_e = 0$$

At this case, the bias voltage is called open circuit voltage  $V_{oc}$ . Fig 2.7 shows the MIS solar cell under this condition.



Fig 2.7: Band diagram and current flow of a MIS solar cell which is open circuited

under illumination



# (f) Illuminated — zero bias (short circuit)

When the MIS solar cell is short circuit connected, the thermionic emission currents cancel each other. Therefore, the current

$$J = J_s - J_m - J_e = -J_e = -J_{sc}$$

The only existing current component that can be drawn out from the device is photo current and this current density is also denoted as short current density  $J_{sc}$ . Fig 2.8 shows the energy band diagram under this condition.



Fig 2.8: Band diagram and current flow of a MIS solar cell which is zero biased under



# (g) Illuminated — reverse bias

When the MIS solar cell is under reverse bias, JS decrease due to the reduced thermionic emission probability. The total current

$$J = J_s - J_m - J_e = J_m - J_e$$

The current density  $J_m$  will reach saturation while if the intensity of the illumination increases, Je increases. The energy band diagram under this condition is shown in Fig 2.9.



Fig 2.9: Band diagram and current flow of a MIS solar cell which is reverse biased



# 2.3 Fabrication of MIS Solar Cells in this Thesis

In this section, we introduce the fabrication process of MIS solar cells in our experiment. Different from the high efficiency bifacial cell discuss in 1.2.2, in order to simplify the fabrication process, electrodes and thin metal films for carrier collection are thermal evaporated through finger-type metal masks on ultra-thin insulating layers. The detailed process is listed as follows:

- (a) Wafers cleaning with traditional RCA clean
- (b) Deposit ultra-thin oxide on wafers with sputtering
- (c) Thermal evaporate electrodes on the back side of wafers

- (d) Annealing at 500  $^{\circ}$ C for 1hr in hydrogen atmosphere
- (e) Thermal evaporate a thin layer of metal film via metal mask on the top of oxide
- (f) Thermal evaporate front electrodes
- (g) Deposit a passivation layer on cells

The structures of n-type and p-type MIS solar cells are shown in Fig 2.10 respectively.



Fig 2.10: Structures of (a) n-type solar cell (b) p-type solar cell

# **Chapter 3 Properties of p-type MIS solar cells**

In this chapter, we focus on the research on MIS solar cells with p-Si substrate. Different from conventional MIS solar cells, we deposit thin tunneling oxide with magnetic sputter instead of thermal oxide. The advantages of sputter oxide are the film thickness and large tuning range of film quality. However, ion bombard effect will produce large amount of defect at the interface and in the oxide film, so some post annealing have to be done to passivate defects after oxide deposition

# 3.1 Photovoltaic Properties with Annealing Process

As show in Fig 3.1 and Table 3.1, cell with poor photovoltaic characteristic is obtained without post-oxidation annealing. From the J-V curve under AM1.5g irradiation, a low  $V_{oc}$  and  $J_{sc}$  indicated that there is probably a great quantity of recombination centers in the oxide film. According to the researches<sup>[14,15]</sup>, high temperature post-oxidation annealing reduces the defect density in thin tunneling oxide and lowers leakage current in MIS diodes. In order to reduce the recombination centers in the tunneling oxide, a post-oxidation annealing is introduced in our fabrication process. In Fig3.1 and Table3.1, solar cells under illumination with annealing at 500°C for 1hr in hydrogen atmosphere are shown. Because hydrogen can easily diffused into oxide film and can passivate Si dangling bonds by formation of Si-H bonds, samples

annealing at 500°C in hydrogen atmosphere exhibit good photovoltaic properties with higher  $V_{oc}$ ,  $J_{sc}$  and FF (Table 3.1). From the capacitance-voltage (C-V) measurement shown in Fig 3.2, with no post annealing, C-V curve have abnormal rapid drop at accumulation region, corresponding to large leakage current due to defects in ultra-thin oxide film with sputter. However, after high temperature H-annealing, the C-V curve only have small drop at accumulation region, indicating the suppression of recombination in oxide film, and an evidence of defect passivation is attain as same as which in J-V curve.



Fig 3.1: Photovoltaic properties of cells with and without H-annealing

Post Annealing	V <sub>oc</sub> (mV)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	FF(%)	Efficiency
as-dep.	207	0.96	28.8	0.06%
H <sub>2</sub> 500°C 1hr	471	13.0	67.8	4.16%

Table 3.1: Photovoltaic properties of cells with and without H-annealing



Fig 3.2: C-V measurement of cells with and without H-annealing

# **3.2** Photovoltaic Properties with Different Oxide Thickness

In order to increase the  $V_{oc}$ , a thin tunneling insulating layer is a must for MIS solar cells. Once the insulator is too thick, the tunneling probability reduce significantly, and then photo carriers cannot be collected by electrodes. According to the simulation on MIS solar cells with small defect density, most photo carriers are blocked by oxide

thicker than 2nm and cells show no photovoltaic properties<sup>[16]</sup>. Therefore, the oxide thickness for the performance of MIS solar cell is critical. With the increasing oxide thickness, the voltage drop on insulator increases, and hence decrease the electric field at the surface of semiconductor. Moreover, a thicker oxide will also lower the tunneling probability of minority carriers, so the drop of current in the J-V curve starts from forward bias.

From Fig 3.3 and Table 3.2, we can also see the tendency of fill factor decreasing while thickness becomes thicker. The J-V curve of sample with sputtered 389s drop at small forward bias, confirmed with above discussion. Although  $J_{sc}$  with sample of sputtered oxide 389s is nearly no change due to slightly decreasing in electric field and tunneling probability at zero bias, low fill factor decreases cell efficiency dramatically and a further decrease with thicker oxide is expected.



Table 3.2: Photovoltaic properties of cells with varying thickness

# **3.3** Photovoltaic Properties with Different Working Pressure

Since we use magnetic sputter to deposit the tunneling oxide on cells, several parameters can be tuned to change the film quality like gas flow rate, working pressure, and RF power and so on. In this section, we vary the working pressure and try to figure out how the film quality changed with different working pressure.

As shown in Fig 3.4 and Table 3.3, the best  $V_{oc}$  reaches 475mV at the working pressure 20mT. As working pressure increases, the  $V_{oc}$  decreases to 350mV at working pressure 40mT. From C-V measurement shown in Fig. 3.5, a curve shift toward zero with the increasing working pressure reveals the reduced barrier height at MIS junction. Furthermore, the small rising at point A indicates defects which are induced by increasing ion bombards probability in oxide film. Therefore, smaller  $V_{oc}$  are obtained because of lower barrier height and lager defect density with the increasing working pressure.



Fig 3.4: Photovoltaic properties of cells with varying working pressure

Pressure (mTorr)	V <sub>oc</sub> (mV)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	FF(%)	Efficiency
20	475	16.8	64.3	5.15%
30	386	16.3	68.3	4.31%
40	350	14.8	66.8	3.45%

Table 3.3: Photovoltaic properties of cells with varying working pressure



Fig 3.5: C-V measurement of cells with varying working pressure

# **3.4** Photovoltaic Properties with Different Metal Thickness

In our MIS solar cells, due to fabrication simplicity, metal electrodes are thermal evaporated through metal masks and then large collecting finger space reduce carrier collection efficiency, as shown in Fig 3.6 and Table 3.4 with no thin metal film. To overcome this problem, a thin metal film for carrier collection is introduced into our cells. Although a thick metal film has good carrier collection efficiency, the reflection is also increase with the increasing metal thickness. Hence, the tradeoff between transparent and carrier collection efficiency is important.

In our work, with decreasing metal film from 15nm to 10nm, an apparent enhancement of  $J_{sc}$  from 13 to 16 mA/cm<sup>2</sup> is shown in Fig 3.5 and Table 3.4.



Fig 3.6: Photovoltaic properties of cells with varying thickness of Al film

Metal Thickness (nm)	V <sub>oc</sub> (mV)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	<b>FF(%)</b>	Efficiency
No metal	411	0.44	64.8	0.12%
10	475	16.9	64.3	5.15%
15	463	12.5	71.9	4.18%

Table 3.4: Photovoltaic properties of cells with varying thickness of Al film

# 3.5 Summary

In this chapter, works on MIS solar cells with p-Si have been discussed at different cases. From the data shown above, post-oxidation annealing in hydrogen atmosphere is a must for cells with sputter oxide due to the high defect density in film. Although film quality can be modified by post annealing, the thickness and sputtering working pressure are also key factors in MIS solar cells, and the best case is sputtered 160s with RF power 50W and working pressure 20mTorr. Finally, we change the thin collecting metal thickness and analyze its properties; cells with aluminum thickness 10nm in our structure have highest efficiency. Although there is only a slightly enhancement in  $V_{oc}$  with decreasing metal thickness from 15nm to 10nm, higher efficiency because of higher J<sub>sc</sub> do help the performance of MIS stacked solar cells.

# **Chapter 4 Properties of n-type MIS solar cells**

In this chapter, n-type MIS solar cells are discussed. As same as that in p-type MIS solar cells, thin tunneling oxide are deposited by magnetic sputter. In order to achieve high  $V_{oc}$  by forming a MIS junction with large barrier height, a high work function metal should be used on n-Si, so we choose gold which has high work function about 5.1eV. However, the barrier height difference between Au and n-Si is only 0.6V with doping density is  $10^{16}$  cm<sup>-3</sup> as shown in Fig 4.1, lower than that between Al and p-Si. Therefore, a small  $V_{oc}$  could be expected.



Fig 4.1 Metal-Semiconductor work function difference versus doping (From Sze<sup>[17]</sup>)

### 4.1 Photovoltaic Properties with Annealing Process

In p-type MIS solar cells, post-oxidation annealing is necessary to get good photovoltaic characteristics (Fig 3.1 and Table 3.1), so the same annealing process annealing at 500°C for 1hr in hydrogen atmosphere is also done. Better photovoltaic characteristics as shown in Fig4.2 after H-annealing are obtained without doubt. Different from p-type MIS solar cells, the cell with no treatment has a not bad fill factor 50.7%, still lower than that with H-annealing though. With C-V analysis (Fig.4.3), the curve drop of as-dep. sample at accumulation region is not as much as that of p-type sample, so n-type MIS solar cells without annealing have better photovoltaic properties. After H-annealing process, though the curve still has a small drop at accumulation region, the right shifted curve indicates the rise of barrier height due to passivation by the formation of Si-H bonds, and then the Voc after H-annealing increases from 313mV to 422mV. However, this value is still lower than that of p-type cells because of the smaller barrier height mentioned in the beginning of chapter4.



Table 4.1: Photovoltaic properties of cells with and without H-annealing



# 4.2 Photovoltaic Properties with Different Oxide Thickness

As discussed in section 3.2, insulating thickness is critical for cell efficiency. We change the sputter time to control the same film thickness as what we do on p-type cells. As shown in Fig4.4 and Table4.2, the tendency from 389s to 778s exhibit lowering tunneling probability and a large voltage drop on thick oxide. The increase in  $V_{oc}$  from 160s to 389s can be explained by the increasing Schottky barrier height with the increasing oxide thickness<sup>[18-20]</sup> and better interface defect passivation.

The best tunneling oxide thickness of n-type MIS solar cells is sputtered 389s (Fig4.4 and Table4.2), thicker than that of p-type in our work. Try to explain this huge

difference with the transport mechanism, in p-type MIS solar cells under illumination, the majority carrier holes are easily blocked by thin oxide due to lower diffusion constant in Si and minority carrier electrons are tunneling through oxide film to produce light current. On the contrary, in n-type MIS solar cells, majority carriers are electrons which are more difficult to be blocked with higher diffusion constant. Therefore, a thicker oxide is needed in MIS solar cells on n-Si.



Fig 4.4: Photovoltaic properties of cells with varying thickness

Sputter Time (s)	V <sub>oc</sub> (mV)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	<b>FF(%)</b>	Efficiency
160	295	14.0	54.7	2.25%
389	366	13.4	56.4	2.76%
583	346	11.6	35.9	1.44%
778	320	11.1	22.3	0.80%

Table 4.2: Photovoltaic properties of cells with varying thickness

# 4.3 Photovoltaic Properties with Different Working Pressure

In Fig. 4.5 and Table 4.3, the tendency of  $V_{oc}$  of n-type cells with increasing working pressure is the same as that of p-type. However, in Fig. 4.6, the C-V curves shift is not apparent between 30mT and 40mT, indicating almost the same barrier heights and  $V_{oc}$ . However, cells with working pressure 20mT show no rising at point A and steep slope in transition from inversion to accumulation, demonstrating lower defect density in oxide film and interface. Therefore, the  $V_{oc}$  of n-type cells with working pressure 20mT reach 422mV, which is the best value in our work, greatly larger than cells with 30mT and 40mT.



Table 4.3: Photovoltaic properties of cells with varying working pressure



4.4 Photovoltaic Properties with Different Metal Thickness

As discussed in section 3.4, the thickness of metal film is a tradeoff between collection efficiency and reflection. In n-type cells, we use gold as front electrode to form MIS junctions. Since the reflection of gold is different from aluminum, the optimum thickness is also different. As shown in Fig 4.7 and Table 4.4,  $J_{sc}$  reaches about 14.3mA/cm<sup>2</sup> with 15nm gold film, and keeps no change while increasing to 20nm. Therefore, an optimum thickness between 15nm and 20nm of gold film on n-type MIS solar cells can be expected. However, there is 40mV difference between 15nm and 20nm, which is not present in p-type solar cells (Fig 3.6 and Table 3.4). This phenomena

result from the nickel deposited on the gold film, which lowers the work function of gold while gold is thinner than 20nm. Since the barrier height is lowered by the lower work function, the  $V_{oc}$  is reduced.



Fig 4.7: Photovoltaic properties of cells with varying thickness of Au film

Metal Thickness (nm)	V <sub>oc</sub> (mV)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	FF(%)	Efficiency
5	196	0.91	36.6	0.07%
10	329	7.17	40.7	0.96%
15	381	14.3	54.0	2.95%
20	422	14.4	58.4	3.55%

Table 4.4: Photovoltaic properties of cells with varying thickness of Au film

# 4.5 Summary

In this chapter, n-type MIS solar cells are realized and analyzed with different parameters. The best tunneling oxide thickness is sputtered 389s with working pressure 20mTorr, thicker than that of p-type cells, and this phenomena can be explain with transport mechanism discussed in section 2.2.

As same as the tendency with the change of annealing process, oxide thickness, metal thickness and working pressure, we get the optimum fabrication parameters and achieve the  $V_{oc}$  422mV.



# **Experiments of MIS Stacked Solar Cells** Chapter 5 5.1

### **5.1.1 General Description**

**Tunneling Diode** 

Tunneling diode also referred as Esaki diode<sup>[21-23]</sup>, is one of the most important issues affecting stacked solar cell performance. The problem of tunnel junction formation is related to the demand of obtaining uniformly highly doped layer without defects which result in carrier recombination and leakage current in depletion regions. In a common tunneling diode, degenerate semiconductors<sup>[17,24]</sup> are used to increase tunneling probability through depletion region.

$$E_{\rm F} - E_{\rm v} = kT \ln \left(\frac{N_{\rm v}}{p_0}\right) \quad (Eq. 5.1)$$
$$E_{\rm C} - E_{\rm F} = kT \ln \left(\frac{N_{\rm C}}{n_0}\right) \quad (Eq. 5.2)$$

Where N<sub>c</sub> and N<sub>v</sub> are referred to as effective density of states, n<sub>0</sub> and p<sub>0</sub> are doping density. From Eq. 5.1 and Eq. 5.2, degenerate semiconductor can obtain with  $n_0$  and  $p_0$ lager than N<sub>c</sub> and N<sub>v</sub>.

The current-voltage properties of a tunneling diode is shown in Fig 5.1, different from conventional p-n junction, the I-V curve is ohmic at small voltage while negative differential resistance (NDR) appears with increasing forward bias. The current-voltage characteristic of a tunneling diode can be explained using the band diagram and J-V characteristic shown schematically in Fig 5.1. When a reverse bias is applied, Fig 5.1(a),

current flows by electron tunneling from occupied states on the p-side valence band into unoccupied states in the n-side conduction band. In equilibrium, with no applied bias, shown in Fig 5.1(b), the net tunneling current is zero. With a small forward bias, current flow by electron tunneling gives rise to a peak current  $I_{\text{p}}$  at voltage  $V_{\text{p}},$  as labeled in Fig 5.1(c). When the conduction band minimum on the n side is raised above the valence band maximum on the p side, the valley current  $I_v$  results at a voltage  $V_v$  in Fig 5.1(d). With further increase in the voltage, the current increases due to tunneling through defect states in the depletion layer and thermionic emission over the diode internal barrier, Fig 5.1(e).







diode with varying bias (From Y. Yan<sup>[25]</sup>)

In a tunneling diode, the doping profile is key point for the performance<sup>[25-27]</sup>. Once an abrupt doping profile is obtained, the resistance at the junction is decreased. In other words, less voltage loss in a stacked solar cell with a higher  $V_{oc}$  could be achieved. On the contrary, the broadening of the abrupt doping profiles increases the tunneling diode depletion region and significantly reduces the tunneling probability through depletion region. Consequently, stacked solar cell performance will dramatically be degraded.

With ion implantation, a common way to achieve tunneling diode, the doping profile of junction is hard to control. Therefore, we use direct wafer bonding to realize a good tunneling junction between two MIS solar cells.



### 5.1.2 Bonding Theorem

Direct wafer bonding generally refers to a process which two cleaned wafers adhere to each other without intermediate medium. If two polished wafers are brought into close sufficiently, attractive forces could pull the two bodies together into intimate contact so that bonds can form across the interface. Nevertheless, the bonding force is too weak that wafer would debond during suffering a small shear force. To strengthen the bonds across the interface, the room temperature bonded wafers have to undergo a high temperature annealing, and then two wafers can adhere to each other permanent.

Direct wafer bonding depends on types of interaction: van der Waals forces,

hydrogen bonds or strong chemical bonds of metallic, ionic or covalent may mediate the adhesion. At room temperature, the attraction between two contacted cleaned wafers is seen as a van der Waals forces or hydrogen bonds<sup>[28]</sup>. After the subsequent heat treatment, the chemical bonds will be formed gradually at the interface, increasing the bonding energy.

The bonding energy is determined by substrate, annealing temperature, surface cleaning, and surface treatments and so on. Among these process parameters, surface cleaning is the most important. In the research, a particle with diameter 0.5um makes diameter 2.5 mm unbounded areas, so wafer cleaning in clean-room before bonding is a better way to enhance the yield and bonding quality. In reality, the bonding strength and electrical properties can even close to a bulk material with carful cleaning process and high temperature annealing.

### 5.1.3 Fabrication of Tunneling Diodes

The fabrication processes of a tunneling diode by direct wafer bonding are listed as follows

- (1) Wafer are cleaned with RCA clean
- (2) Ion implantation at the polished side
- (3) Dopants activated with rapid thermal annealing (RTA)  $1050^{\circ}$ C 30s
- (4) Furnace 600°C 30 min in N2 to recovery implantation damage

- (5) Wafer are dipped in diluted HF to remove native oxide
- (6) Ultrasonic cleaning with acetone and IPA, respectively
- (7) Direct bond n-type and p-type Si wafers with polished sides each other in IPA

and then Put the bonded samples into a clamp (Fig 5.2)

(8) Heated up to  $500^{\circ}$ C for 1 hour

(9) Al 100nm and Ni 100nm are deposited on n-type and p-type Si to form ohmic contacts and measure its J-V properties



Fig 5.2: Schematic top view and side view of bonding clamp

### 5.1.4 Result and Discussion

The current-voltage characteristics of tunneling diode fabricated by bonding are shown in Fig 5.3. Without furnace at  $600^{\circ}$ C for 30 minutes to recovery implantation

damage, the lower current is attained without doubt. Moreover, the forward bias current is lower than reversed bias current. After furnace annealing, current raises at least two orders at reversed bias and about four orders at forward bias (Fig 5.3), and J-V curves shows no NDR in tunneling diode but a typical characteristic of a diode with large reversed saturation current.



Fig 5.3: Current-Voltage properties of bonded samples in dark with and without furnace

annealing

To explain these strange J-V properties, we measure the junctions between ion implantation regions and wafers. From Fig 5.4, we can conclude that without furnace annealing, the junctions between ion implantation regions and wafers, corresponding to

n-n<sup>+</sup> and p-p<sup>+</sup> internal junctions, dominate the J-V properties and exhibit the opposite trend. With Furnace annealing, junctions vanished due to dopants diffusion and an ohmic curve with large current density are obtained because of defects diminishing.



Fig 5.4: Current-Voltage properties of single wafer under dark with and without furnace

### annealing

Although the bonded sample shows no NDR in J-V curve (Fig 5.3), indicating insufficient doping activation or defects in the central junction, the current density reaches 10mA/cm<sup>2</sup> with 20mV voltage drop, which would only slightly degrade the performance of MIS stacked solar cells. Therefore, we use this junction as the central

junction for MIS stacked solar cells.

# 5.2 Fabrication of MIS Stacked Solar Cells

To realize a MIS stacked solar cell, we should integrate three different junctions discussed early together. Starting from a bonded sample first, n-type and p-type MIS junctions are fabricated on both sides. However, 4-inch Si wafers has a thickness about 525um, which is thicker than the skin depth of visible light, so the cell on the back side under illumination can absorb light hardly. From point of current matching, net current output would be limited by bottom cell which generates less current. Consequently, a thinning process of bonded sample has to be done before two MIS junction fabrication to increase current in stacked cells. Although bonded sample can suffer mechanical thinning process, huge amount of defects at the surface are produced simultaneously. Hence, additional chemical etching process is introduced to remove surface defect and thin the wafer at the same time. The fabrication processes of MIS stacked solar cell are listed below:

- (1) Bonded samples thinning with sand paper
- (2) Dip samples into Si etchant (HF:CH<sub>3</sub>COOH:HNO<sub>3</sub>=6:7:20) to remove surface defects and thin the samples at the same time
- (3) Deposit tunneling oxide with sputter at both sides

- (4) H-annealing 500°C 1hr to passivate defects in oxide film
- (5) The top cell deposit the transparent structure as same as that in section 2.3
- (6) The bottom cell deposit rear electrode
- (7) The structures of MIS stacked solar cells are shown in Fig 5.5



Fig 5.5: Structures of MIS stacked solar cell with top cell is (a) n-type (b) p-type

### 5.3 Results and Discussions of MIS Stacked Solar Cells

In this section, we show the J-V characteristics in dark and under solar irradiation. As discussed above, thinning process is essential to enhance cell efficiency. Afterward, we dip cells into Si etchant to remove damaged layer and thin the thickness at the same time. However, as shown in Fig 5.6, only the stacked cell with p-type cell thinning on the top reveals a low leakage current. The leakage currents of others are high due to insufficient passivation and high defect density. Therefore, fabrication uncertainty is a difficulty to maintain the quality of stacked cells.



Fig 5.6: Current-voltage properties of MIS stacked solar cells in dark with (a) no thinning process (b) n-type cell thinning on the top (c) p-type cell thinning on the top

The current-voltage characteristics of MIS stacked solar cells under AM1.5g are shown in Fig 5.7 and Table 5.1. The cell without thinning process exhibits low  $J_{sc}$  $5.25mA/cm^2$  because the current is limited by bottom cell discussed in section 5.2. After thinning the top n-type cell to 50nm approximately, a much higher  $J_{sc}$  16.5mA/cm<sup>2</sup> is obtained. However, the large leakage current suppresses the photovoltaic performance and the cell with n-type thinning on the top reaches the  $V_{oc}$  414mV.

Since the cell with p-type thinning on the top reveals a low leakage current, the  $V_{oc}$  would not be suppressed and reaches  $V_{oc}$  593mV. This value is larger than single

junction MIS solar cells discussed in Ch3 and Ch4, demonstrating the utility of stacked cells. In this structure, the bottom cell is n-type MIS solar cells; the photo current of n-type cells are determined by minority carriers, holes, which have a lower mobility and cannot be collected by electrodes as easily as electrons. Hence, better photovoltaic properties of cells with n-type thinning on the top can be expected.



Fig 5.7: Current-voltage properties of MIS stacked solar cells under illumination

Cell	V <sub>oc</sub> (mV)	J <sub>sc</sub> (mA/cm <sup>2</sup> )	<b>FF(%)</b>	Efficiency
No thinning	437	5.25	23.6	0.54%
n-thinning	414	16.5	25.2	1.71%
p-thinning	593	4.74	41.1	1.15%

Table 5.1: Current-voltage properties of MIS stacked solar cells under illumination

# 5.4 Summary

In this chapter, tunneling diode fabrication using direct wafer bonding is realized first. Although the bonded samples show no NDR which should present in tunneling diode, high reversed saturation current diodes are achieved with only 40mV loss while current density reach  $10mA/cm^2$ . Finally, we integrate n-type and p-type MIS solar cells on bonded sample to realize MIS stacked structure. The V<sub>oc</sub> of MIS stacked cells reach 593mV, lager than that of p-type and n-type cells, demonstrating that the structure is practical and have its potential to achieve water splitting.



# **Chapter 6 Conclusion and Future Work**

# 6.1 Conclusion

In this thesis, MIS stacked solar cells are introduced and achieved in order to reach high voltage output.

First, we give general description of the transport mechanism of MIS solar cells in Chapter2. We also study the MIS solar cells on n-type and p-type of substrates in chapter3 and chapter4. The influence of fabrication parameters such as annealing process, tunneling oxide thickness, working pressure and metal thickness on MIS solar cells are investigate. With the best conditions, we get the  $V_{oc}$  equals to 475mV on p-type cells and 422mV on n-type cells.

In the beginning of chapter5, we introduce the fabrication of tunneling diode by direct wafer bonding. Although the bonded samples exhibit no NDR at small forward bias, diodes with high reversed saturation current are accomplished and can be used in the MIS stacked solar cells. Afterwards, MIS stacked solar cells are realized by integrating two types of MIS solar cells on bonded samples and best V<sub>oc</sub> equals to 593mV in our experiment is obtained.

### 6.2 Future Work

Since best  $V_{oc}$  in our cells is 593mV, lower than theoretic  $V_{oc}$  equals to 0.9V, there

are still many issues to be investigated. First, the voltage drop at the central junction could be lowered by further improving the tunneling current with proper doping activation and defect passivation. Moreover, the thickness of upper cells and bottom cells in stacked cells should be precisely controlled and the current matching could be achieved.

Afterward, in order to enhance the efficiency,  $J_{sc}$  is the important issue to be improved. Surface texturing by chemical etching is a common way to reduce surface reflection while some researches indicate that  $V_{oc}$  would slightly decrease. Besides, transparent conductive oxide such as ITO and ZnO can be introduced in our structure with the aid of sputter to further increase  $J_{sc}^{[29]}$ .

Finally, though the combination between solar cells and fuel cells is still a big challenge, our research does help the development of solar cells and the living of human beings.

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# Vita

**Hsin-Yu Lee** was born at 25, Aug. 1986 in Tainan, Taiwan. He received the B.S. degree in Department of Electrical Engineering, National Taiwan University, Taipei, Taiwan in 2007. The M.S. degree will receive in Department of Photonics, National Chiao Tung University, Hsinchu, Taiwan in 2009. His research include the analysis and fabrication of MIS stacked solar cells.





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