國立交通大學

電子工程學系 電子研究所 碩士論文

利用交錯訊號穿透提升隔離度 低功率混頻器之研究

The study of low power down conversion mixer using cross signal feed-through to enhance isolation

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中華民國九十九年六月

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摘要

本文描述如何使用 single-balance 電路架構來設計低功率降頻混頻器。有鑑於此電路架構先天的缺點—低隔離度,利用交錯的本地震盪(Lo)穿透後達到互相抵銷的效果,進而提升隔離度,而又因其電路架構先天的優勢,達到低功率消耗的效果。此混頻器使用 TSMC 0.18µm CMOS 製成並且經由 ADS momentum 做 EM模擬分析。在此設計一個 RF 為 5.8GHz, Lo 為 5.81GHz, IF 為 10MHz 的降頻器,約有 6dB 增益,-8.5dB 的 Lo-IF 隔離度,>60dB 的 Lo-RF 隔離度,2dBm 左右的 IIP3,17dB 之 Noise Figure,和 2.72mW 的功率消耗。

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Abstraction STREET

The study is using single-balance structure to design a low power down conversion

mixer. Because of the basic single balance structure has a inborn defect—bad

isolation, we use cross Lo feed-through to cancelling the Lo signal which appearing in

IF port so that can enhance Lo-IF isolation. And because of its innate structure benefit,

low power consumption is reachable. The mixer is implemented by using TSMC

0.18µm process. The EM simulation results with ADS momentum. The mixer is deign

with RF in 5.8GHz, Lo in 5.81GHz and IF in 10MHz. And it exhibits 6dB of gain,

-8.5dB of Lo-If isolation, over -60dB of Lo-RF isolation, 2dBm of IIP3, 17dB of

Noise figure, and 2.72mW of power consumption.

ii

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99年6 月

Contents

摘要	i
Abstraction	ii
誌 謝	iii
Contents	iv
Figure Captions	vi
Table Lists	viii
Chapter1 Introduction	1
1.1 RF transceiver	1
1.2 Technology concept	3
1.3 Motivation	4
Chapter2 Fundamental of Down Conversion Mixer	5
2.1 Introduction	5
2.2 Characteristic	6
2.2.1 Power	6
2.2.2 Gain	6
2.2.3 Isolation	6
2.2.4 IIP3	7
2.2.5 Noise Figure 2.3 Passive circuit	8
2.3 Passive circuit	9
2.4 Active circuit	10
2.4.1 Single-balance mixer	10
2.4.2 Gilbert cell (double-balance) mixer	10
2.4.3 Active circuit operate theory	11
Chapter 3 Down-Conversion Mixer Circuit Design	13
3.1 Introduction	13
3.2 First stage	14
3.3 Second stage	15
3.4 Third stage	17
3.5 Cross signal feed-through	19
3.6 Output buffer	26
3.7 Total circuit	28
Chapter 4 Simulation and Measurement Result	31
4.1 Simulation	31
4.2 Measurement	37
4.3 Specification	42

Chapter 5 Design Flow	43
5.1 Design flow	43
Chapter 6 Conclusion and Improvement	
6.1 Conclusion	44
6.2 Improvement	46
Reference	47
Vita	ДС



Figure Captions

Fig 1.1 RF transceiver structure	-1-
Fig 2.1 Down conversion mixer principles	-5-
Fig 2.2 LO-RF isolation	-7-
Fig 2.3 IIP3	-8-
Fig 2.4 Noise factor in cascade stage	-8-
Fig 2.5 Passive double-balance mixer	-9-
Fig 2.6 Single-balance mixer	-10-
Fig 2.7 Gilbert cell mixer	-11-
Fig 3.1 First stage	-14-
Fig 3.2 Second stage	-15-
Fig 3.3 Simulation of VLO	-16-
Fig 3.4 Third stage	-17-
Fig 3.5 Simulation of Rload	-18-
Fig 3.6 Small-signal model of M2	-19-
Fig 3.7 Gilbert-cell Structure	-20-
Fig 3.8 Small-signal model of M2 and M5	-21-
Fig 3.9 Second stage after design	-22-
Fig 3.10 Small-signal model of M2	-22-
Fig 3.11 Simulation of C1 and C2	-23-
Fig 3.12 Simulation with capacitance	-24-
Fig 3.13 Simulation without capacitance	-24-
Fig 3.14 Source follower buffer	-26-
Fig 3.15 Small-signal model of M7	-27-
Fig 3.16 Simulation of S33	-27-

Fig 3.17 Total circuit		-28-
Fig 3.18 Circuit Layout		-29-
Fig 3.19 Implementation		-30-
Fig 4.1 Conversion gain		-31-
Fig 4.2 Isolation Lo-IF		-32-
Fig 4.3 Isolation Lo-RF		-33-
Fig 4.4 IIP3		-34-
Fig 4.5 Noise Figure		-35-
Fig 4.6 Gain		-38-
Fig 4.7 Isolation Lo-RF		-39-
Fig 4.8 Isolation Lo-IF	Julian Committee	-40-
Fig 4.9 IIP3	1896	-41-

Table Lists

Table 3.1 Voltage and Current	-29
Table 4.1 Compare with C and without C	-36
Table 4.2 Different condition	-37
Table 4.3 Calibrate number	-37
Table 4.4 Spec.	-42
Table 6.1 Comparison of Mixer performance	-45



Chapter1

Introduction

1.1 RF transceiver

In the last few years, wireless technology is growing maturely. Not only in communication, more and more product having wireless system for convenient and useful, such as wireless printer, wireless mouse, MP3 player, even some gaming machines have it.

Generally, the radio frequency system module can be separated two parts by its working situation, transmitter and receiver.

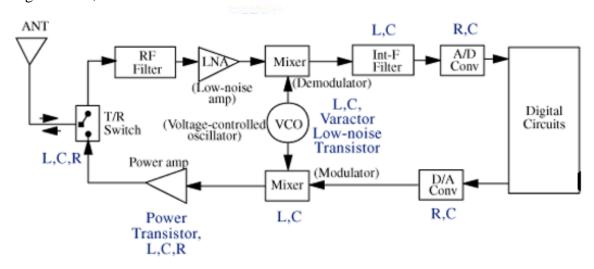


Fig 1.1 RF transceiver structure

Transmitter is the lower side of Fig 1.1. This parts mainly function is to transmit the signal out of the devise. The digital signal we want to transmit is firstly send to a D/A converter (digital to analog), and the digital square wave became analog sin wave. But the frequency is too low to transmit, so the signal is next send to the up-conversion mixer rising up its frequency. Because we want our signal sending as far as it can, so we need to promote its power level to against the loss when delivering. Power amplifier is achieving this mission. After the three functional blocks, T/R

switch choose the path that the signal can pass to Antenna and then delivering out.

The other part – receiver is upper side of fig 1.1. Oppositely, this part is receiving signal from another device. After a long distance delivery, signal is very weak and company with noise, first thing is using the RF filter to filter the noise. Low noise amplifier has gain and then like transmitter, we need to down the frequency to that the digital circuit can handle, so we need the down conversion mixer. Finally, A/D converter translate sin wave to square wave.



1.2 Technology concept

Pseudomorphic High Electronic Mobility Transistor (pHEMT) FET,

Hetero-junction bipolar transistor (HBT), bipolar junction transistor (BJT), CMOS,

BiCMOS, LDMOS are common implementation of RF integrated circuit.

Each implementation technology has their advantage and drawback, so it is the reason why individual implementation component built systems are favored for so many years. CMOS for base band section, bipolar for IF partition, ceramic for SAW filters, III-V such as GaAs for RF transmitter especially for power amplifier.

Consider the various technologies for RF circuit, III-V technology always has better characteristics such as lower noise and higher unit current gain cut off frequency (ft). But it's too expensive and few so that silicon-based FET is popular recently. Fortunately, the process reduce the minimum channel length in recent years, unit current gain cut off frequency (ft) has increased, For instance, TSMC 0.13um technology, ft is above 100GHz [10], for TSMC 0.18um technology, ft is about 51 GHz. Basically, that is suitable for present protocol. CMOS technology has become the most popular process not only because of the cost and integration level, but also its special benefit – low power consumption.

1.3 Motivation

According to WLAN (wireless local area network) technology is getting mature, more and more products have the function on it. Especially portable product, rely on wireless technology's convenient, lot's of them using the technology as common. In recently, every notebook definitely have WLAN function, some high-level mobile phone also get it, although they have 3G network. Some big-screen MP3, like ipod, is also using this function as selling point. And lots of handheld game console also have it to link on the internet finding another player to challenge.

Because portable product is using battery as its main power supply, low power consumption circuit design become more and more important, that can enhance the using time of product. In RF system, no matter in transmitter or in receiver, mixer both plays an important role on it. So in this thesis, we force on designing a low power mixer.

Chapter2

Fundamental of Down Conversion Mixer

2.1 Introduction

Mixer performs frequency translation by multiplying two signals (and possibly their harmonic).

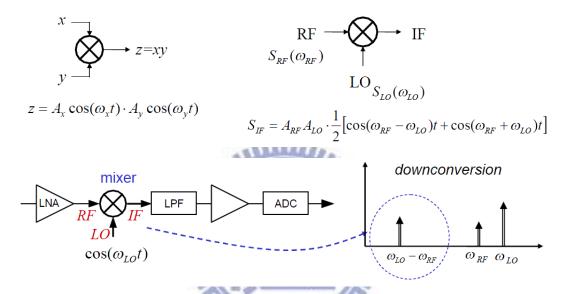


Fig 2.1 Down conversion mixer principles

Down conversion mixer employed in the receive path have two distinctly different inputs, called RF port and Lo port. The RF port senses the signal to be down converted and the Lo port senses the periodic waveform generated by local oscillator. The output of them is IF port, which signal can be used in baseband. The frequency of IF is decided by frequency of RF and Lo. As Fig 2.1, we can find the two cosine wave multiply can generate the two frequencies subtract term.

2.2 Characteristic

There have five most important characteristics of Mixer.

2.2.1 Power

DC power is the most obvious characteristic. Unlikely digital circuit, analog circuit always have DC power when the circuit acting.

As the reason, low power design is a very popular direction on analog circuit. The equation of power is that Power = V*I, so the only way to achieve low power is lower voltage supply or lower current be used.

2.2.2 Gain

The gain of mixers must be carefully defined to avoid confusion. The "Voltage conversion gain" is defined as the ratio of the rms voltage of IF signal to the rms voltage of RF signal. Note that these two signals are centered around two different frequencies.

The "Power conversion gain" is defined as the IF power delivered to the load divided by the available RF power from the source. If the input impedance and the load impedance of the mixer are both equal to the source impedance, for example 50 Ω , then the voltage conversion gain and power conversion gain are equal when expressed in decibels.

Although the circuit main function is to change frequency level, gain cannot be to low. Noise figure has a huge relationship with circuit gain in cascade structure.

2.2.3 Isolation

We have two important isolations, Lo-RF isolation and Lo-IF isolation.

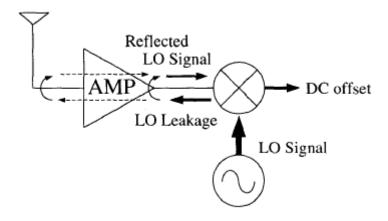


Fig 2.2 LO-RF isolation

As we can see in Fig 2.2, when the signal of Lo leakage to RF port, the reflected Lo signal will have self conversion and cause DC offset at IF port. The current of that will make the power of circuit rise or even cause the circuit in saturation.

Another important isolation, Lo-IF isolation is also a important issue. Although the Lo signal and IF signal have different frequency, but lots of receiver structure have more than once down convert and power gain. If the IF port output connect with a amplifier as next stage, the large Lo signal may cause the voltage swing larger than expect, will cause the amplifier in saturation and smaller the gain as it origin design.

So, both of them are important for mixer.

2.2.4 IIP3

IIP3 is the way to show the linearity of circuit. According to mixer's input signal is always not so large, P1dB is not appropriate characteristic for compare with others. We use IIP3 to show the linearity, the larger IIP3 circuit has, the more linearity it is.

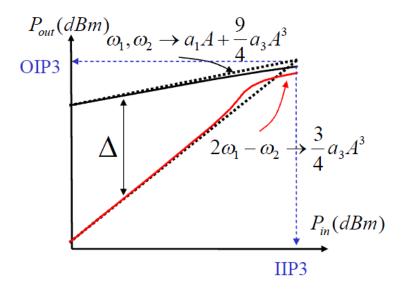


Fig 2.3 IIP3

2.2.5 Noise Figure

Noise figure has huge relationship with the gain of front circuits. Mixer is not the first stage of receiver, so we can have a relax specification on it.

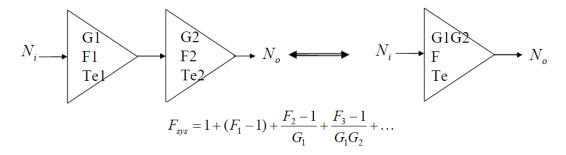


Fig 2.4 Noise factor in cascade stage

2.3 Passive circuit

In most of mixer designed, there had two kinds of structure. One of them is passive circuit. This structure has lower (almost zero) DC power consumption.

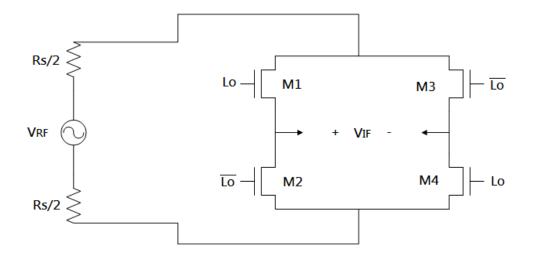


Fig 2.5 Passive double-balance mixer

For low power design, it's seems the best structure because there's no DC power dissipation. But after we study intensively, we find out the circuit needs large power of Lo to make the function works. M1~M4 needs to be acted like switches, so we needs a strong oscillator to generate this signal. Although mixer has no power dissipation, but the needing oscillator circuit may need huge power for generates signals. So the total structure may not have lower power.

Another bad issue of this structure is that the circuit has poor gain. So this circuit is seldom used in receiver design.

2.4 Active circuit

The most popular type of mixer is active circuit. And there has two kinds of active circuits – Single-balance and Double-balance.

2.4.1 Single-balance mixer

Single-balance mixer is with one RF input and differential Lo inputs.

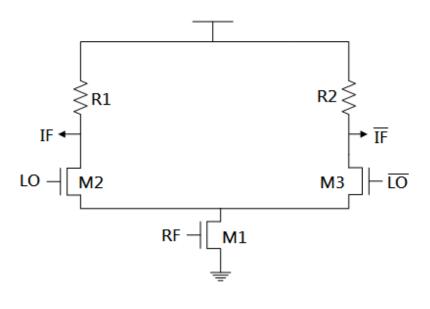


Fig 2.6 Single-balance mixer

Single-balance mixer has a better gain than passive circuit, but like most of analog circuit, it has DC power consumption. Poor Lo-IF isolation is also the reason that makes it not as popular as double-balance mixer.

2.4.2 Gilbert cell (double-balance) mixer

Gilbert cell is the most common structure. Most of designs of mixer are base on this structure. It has both differential RF signal and Lo signal input.

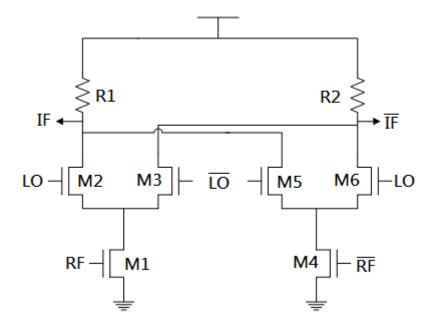


Fig 2.7 Gilbert cell mixer

The structure's biggest disadvantage is that DC current is twice larger than single-balance structure. But the better isolation, higher linearity, makes it becoming the first choice when anybody wants to design a mixer.

2.4.3 Active circuit operate theory

We can depart the circuit into three stages: driver stage, switching stage, and load stage.

M1 (and M4) is the first stage. In this stage, like normally amplifier, provide voltage gain to RF signal.

$$gm \times V_{RF} \times r_{out}$$
.....(1)

M2 and M3 (M5 and M6) is the second stage. The theory of this stage is base on the saturation MOS current equation.

$$K(V_{GS} - V_{th})^{2}$$

$$= K[(V_{g} + V_{lo} \cos \omega_{1}t) - (V_{s} + V_{rf} \cos \omega_{2}t) - V_{th}]^{2}$$
And only AC term
$$(V_{lo} \cos \omega_{1}t - V_{rf} \cos \omega_{2}t)^{2}$$

$$= ... - 2V_{lo} \cos \omega_{1}t \times V_{rf} \cos \omega_{2}t...$$

$$= ... + A \times \cos(\omega_{1} - \omega_{2})t......(2)$$

R1 and R2 is the third stage. In down conversion system, we usually use resistance as impedance.



Chapter 3

Down-Conversion Mixer Circuit Design

3.1 Introduction

In normal, the mixer designer used Gilbert cell mixer to be the basic structure, because it have higher isolation (including Lo-RF and Lo-IF), lower noise factor.

Although the benefits are so obvious, the Gilbert cell circuit is not such perfect. Its circuit is just like a differential pair, so if we want the circuit to have the same gain with single-balance circuit, it takes twice large of current than single-balance circuit.

But single-balance structures isolation is so poor that we cannot ignore them, especially LO-IF isolation.

In this chapter, we are using a single-balance structure to achieve low power issue, and have some change of circuit to enhance Lo-IF isolation.

The circuit is design in TSMC 0.18µm. RF frequency is 5.8GHz, Lo frequency is 5.81GHz, and IF frequency is expected 10MHz.

3.2 First stage

First stage is the most important stage of the mixer design. It can decide the total circuit power, almost can decide gain, and also has large effect on linearity and noise factor.

Because of NMOS's characteristic - the higher frequency has the lower gain, choose appropriate current is getting hard. We cannot have too much current for low power circuit, but we also need a current for circuit characteristic.

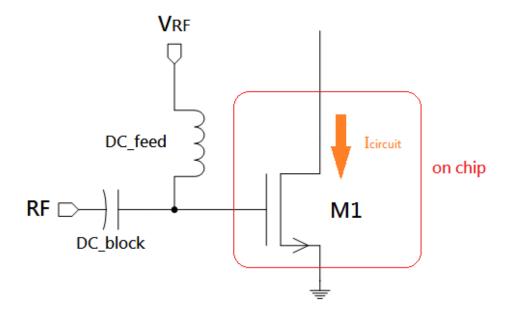


Fig 3.1 First stage

In Fig 3.1, after we decide the current and gain of circuit, we finally can choose appropriate NMOS size for M1. And because M1 should active in saturation mode, we can easily design the V_{RF} . Finally, M1's width is 6 μ m, finger is 6, and with 0.18 μ m length. V_{RF} is 0.7V and cause the current become about 1mA.

Because we choose 1.8V for VDD, we can almost sure our circuit consume about 2mW.

3.3 Second stage

This stage is using Lo signal to down-conversion the RF signal to IF frequency. In this stage, Icircuit in Fig 3.1 be divide by two parts. Because we need the both side have the same gain and just opposite phase, the currents must be just the same. So we can easily design the M2's and M3's size in Fig 3.2.

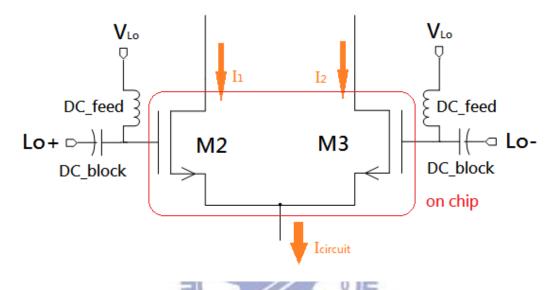


Fig 3.2 Second stage

In Fig 3.2, I₁ and I₂ is about 0.5mA, is just half of Icircuit, so we can easily choose M2's and M3's size as half of M1's. Width is still $6\mu m$ but fingers become 3, and length is $0.18\mu m$.

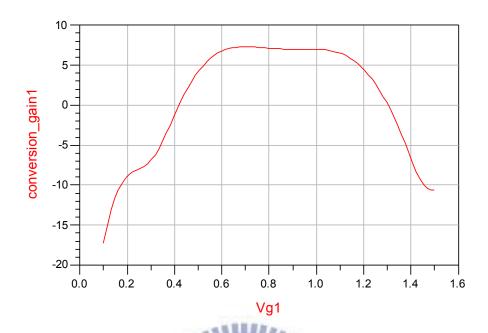


Fig 3.3 Simulation of VLO

Then we need to design V_{Lo} . As show in Fig 3.3, we simulate sweep V_{Lo} from 0V to 1.5V, and we can find out if V_{Lo} is between 0.7V to 1V have the maximum gain, and we check every point in this section, V_{Lo} at 1V get the most linearity, so we choose $V_{Lo}=1V$ for design.

3.4 Third stage

This stage is translating current gain become the voltage gain. Not like up-conversion system, IF frequency is very low, in this case is 10 MHz, so we cannot use inductances as impedance, it would need a very large inductance(Z=j ω L). Although inductances have no DC power consumption, is the best choice of low power design, but the size will become too large to put it in the chip. So we have to use resistance to replace them.

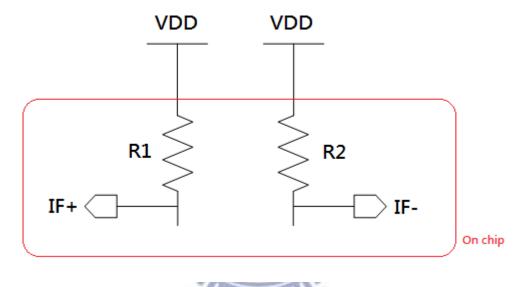


Fig 3.4 Third stage

If we choose a too big resistance, there will have lots of voltage dropped on it, case the MOS below them in liner section, gets the bad gain and bad linearity. But what if we choose too small, there will still have not enough gain.

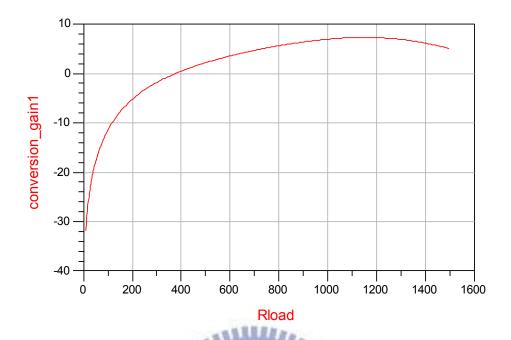


Fig 3.5 Simulation of Rload

In Fig 3.5, we use ADS to simulate what appropriate number it should be. We sweep from $10\Omega~$ to $1.5K\Omega$. We can find out when the resistance below $800\Omega~$ or larger than 1400Ω , gain will degrade. In this area, after simulate every point, we choose the best linearity point - $1220\Omega~$ for this circuit.

3.5 Cross signal feed-through

As we mention in Chpater 2.4, single-balance circuit has a big disadvantage that it has a poor isolation on Lo-IF port. Although they are in different frequency, but what if the next circuit of mixer output is an amplifier, the big Lo signal will cause the MOS saturation. So we do not want large Lo signal feed-through to IF port.

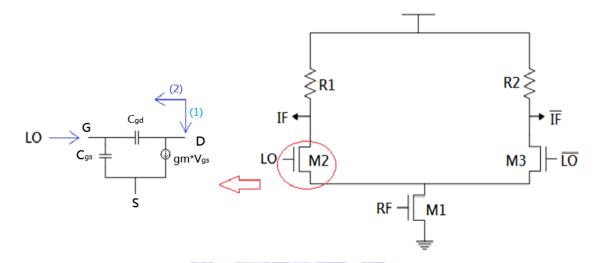


Fig 3.6 Small-signal model of M2

As Fig 3.6, we can find out why the single-balance circuit has poor Lo-IF isolation.

$$Lo_{out1} = V_{lo} \times \frac{R1}{R1 + \frac{1}{j\omega C_{gd}}}.....(1)$$

The first term of Lo $_{out}$ is cause by C_{gd} . Its phase is almost 270 degree from the origin signal.

$$Lo_{out2} = V_{lo} \times gm \times R1.....(2)$$

The second term of Lo_{out} is cause by the M2's gm. As the M2's and M3's sources connect together, we can assume their source as virtual ground in AC operating. So

the V_{gs} is the same as V_{lo} . So we can find Loout term in the function (2).

As we can see in Fig 3.6, the two phases are different, so they would not be cancelled by each others.

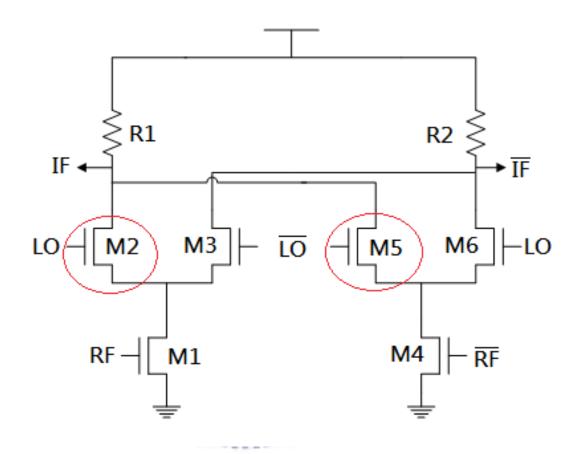


Fig 3.7 Gilbert-cell Structure

That's check why double-balance mixer has such a good isolation of LO-IF.

That's plot the small signal of M2 and M5.

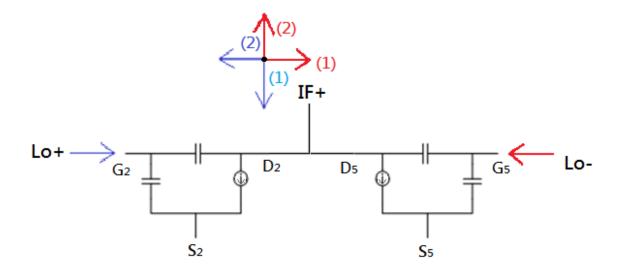


Fig 3.8 Small-signal model of M2 and M5

Because of M2 and M5 have complete different input phase of Lo signal, Gilbert-cell mixer can easily enhance isolation. The Lo+ signal causes 180 degree and 270 degree of phase of Lo, and the Lo- signal causes 360 degree (0 degree) and 90 degree of phase of Lo. Although because M2 and M5 is totally the same, not only size but also bias situation, so the signal's amplitude they cause are the same, too. So as the reason, the feed-through signals are almost perfectly cancelled.

After we analyze the structure, we find out one part of Lo feed-through signals is cancelled by the opposite signal feed-through by the other MOS's C_{gd} . So we design the following structure.

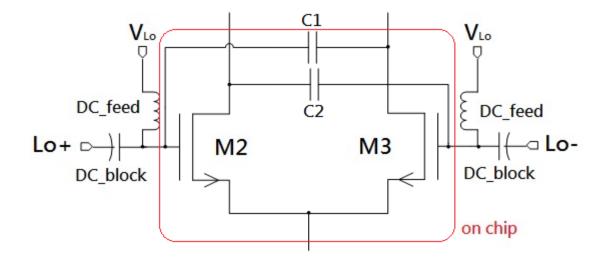


Fig 3.9 Second stage after design

Shows in Fig 3.8, we use C1 and C2 to replace M5's and M6's Cgd. So we can cancel a part of Lo signal that feed-through to the IF port.

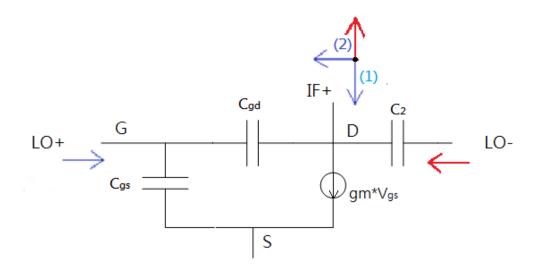


Fig 3.10 Small-signal model of M2

In Fig 3.9, the C_2 is just like M5's C_{gd} in Fig 3.7. We can cancel the Lo+ signal feed-through by C_{gd} . Having the structure like this, then we need to design the appropriate number of C_2 and C_3 . First we used ADS to simulate what level the C_{gd} is. We floated the Source of a the-same-size MOS, and put two terms on gate and drain. After we plot the S-parameter plan, than find a capacitance level can cause similar

S-parameter plan. Now we find the level is fF, what we need to do is only to optimize the number. In this level, the impedance which IF signal saw is so large, that we can consider there is an open circuit, and with out loss.

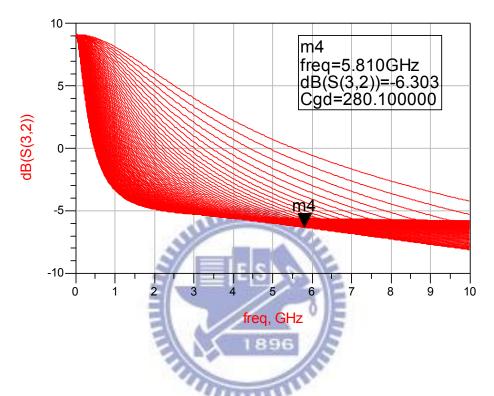


Fig 3.11 Simulation of C₁ and C₂

We can find out when C₁ and C₂ over 150fF can achieve the best isolation. And what if over 300fF, the isolation is stable. When we choose the number is not just "big is best", if the C₁ and C₂ is too big, IF signal will pass through from them to the Lo port, cause the gain depressed. Finally we choose a 200fF capacitance as C₁ and C₂. This number we can have a good isolation and not to influence any other characteristic.

To prove the capacitance is work on enhance isolation, we simulate the same circuit but one have capacitance but the others not.

The result is in following plot.

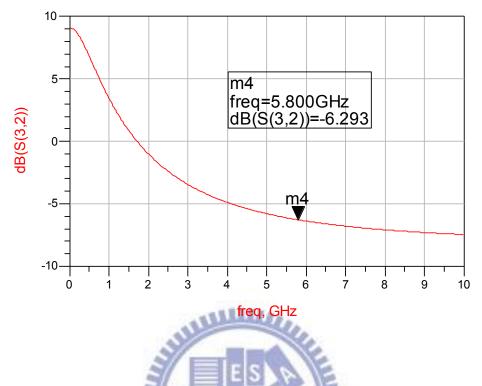


Fig 3.12 Simulation with capacitance

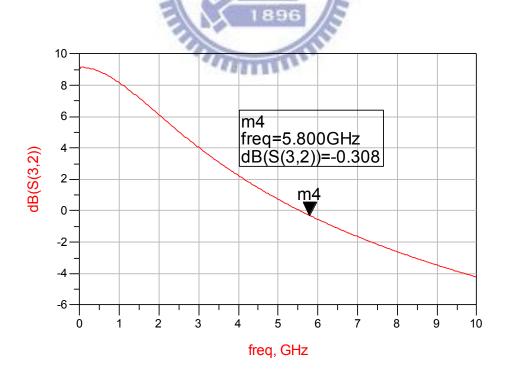


Fig 3.13 Simulation without capacitance

In Fig 3.11 and Fig 3.12, we can find out with the cross capacitance, Lo-IF isolation can be enhance by almost 6dB.

Back to the Fig 3.9, we can still see a 180 degree phase Lo signal appearing in IF port. We have no way to cancelling it, otherwise we use another MOS. But what if we do this way, the current will become the same level as Gilbert cell mixer, and loss our main purpose – low power.



3.6 Output buffer

Because of needing to measure all the frequency point on output port, we must have a broad band matching at output port.

The RF signal is 5.8GHz, Lo signal is 5.81GHz, and IF signal is 10MHz. In this case, we have two ways to do the matching job. First way is using traditional RF matching technology – LC matching. But because the IF frequency is so low and the three frequency is so apart, we need a very large size inductance and capacitance and also many of them. According to the chip size limit, we can only design a circuit that littler than 1.4*1.4 mm*mm. So we absolutely cannot use LC matching.

So the only way we can use is Source follower buffer.

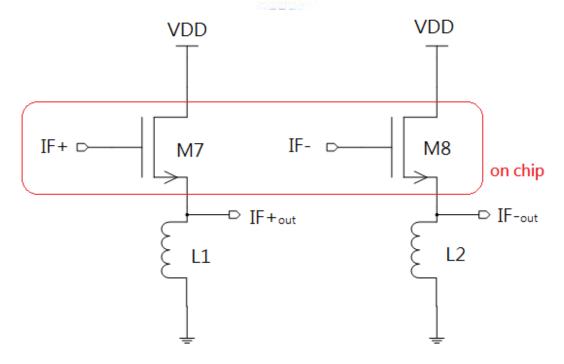


Fig 3.14 Source follower buffer

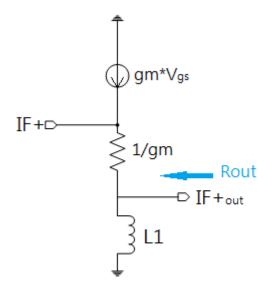


Fig 3.15 Small-signal model of M7

In Fig 3.14, we can find that Rout almost equal 1/gm, because L1 is big enough that parallel connection equal to 1/gm. We can choose appropriate size that 1/gm equal to 50Ω .

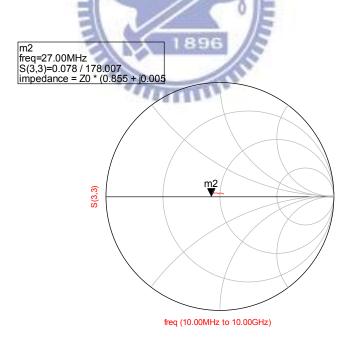


Fig 3.16 Simulation of S33

As Fig 3.15, we can find every frequency point is around 50Ω .

3.7 Total circuit

Finally we can have the complete circuit.

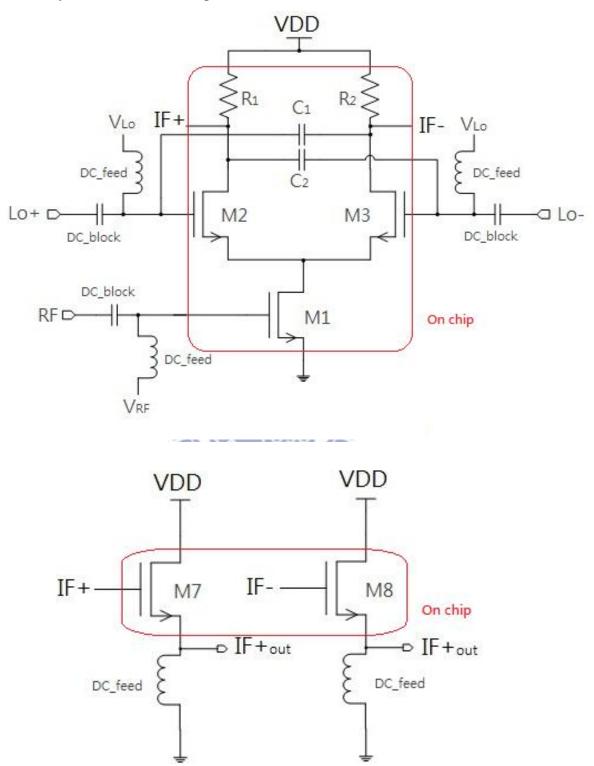


Fig 3.17 Total circuit

In Fig 3.16, all the DC_feeds or DC_blocks we can use RF bias tee to achieve their functions.

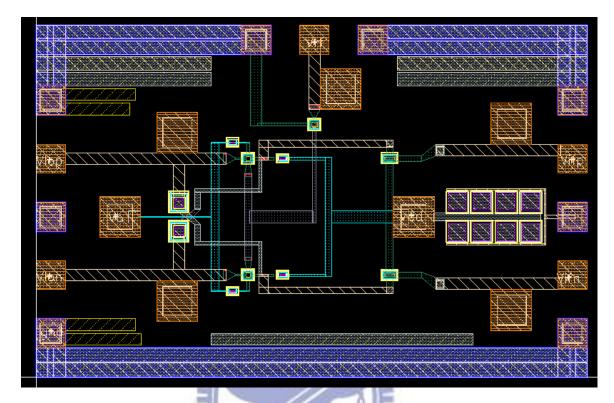


Fig 3.18 Circuit Layout

1896

For measure convenient, we plot some pads that we can bound wires them.

Using this pad we can measure some DC data, without use any RF probe or any RF instrument.

Table 3.1 Voltage and Current

VDD	$V_{ m RF}$	V_{Lo}	Icircuit	Power	Itotal	
1.8V	0.7V	1 V	0.98mA	1.7mW	27.3mA	

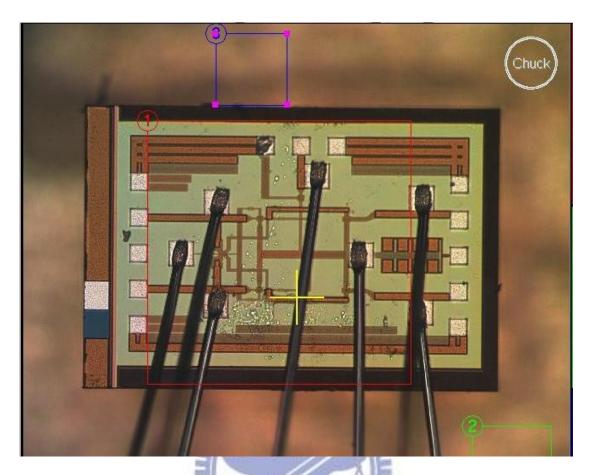


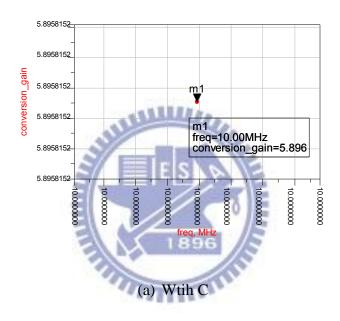
Fig 3.19 Implementation

Chapter 4

Simulation and Measurement Result

4.1 Simulation

We simulated both with and without the cross capacitance data. But with capacitance, we simulated post-layout circuit. Without capacitance simulated pre-layout data.



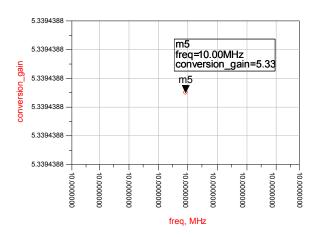
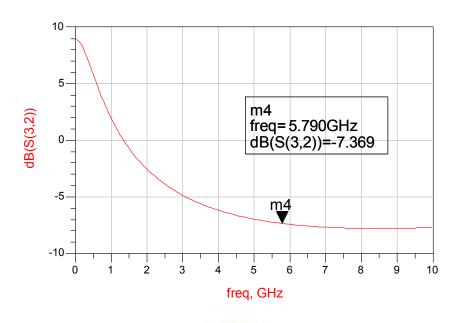


Fig 4.1 Conversion gain



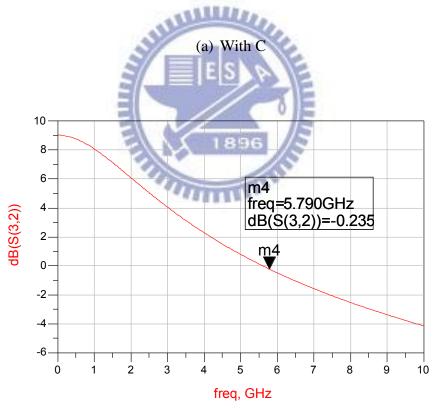


Fig 4.2 Isolation Lo-IF



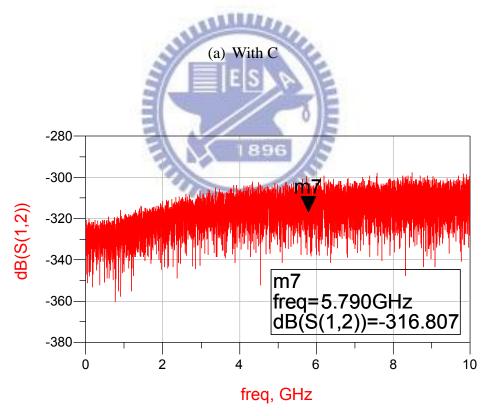
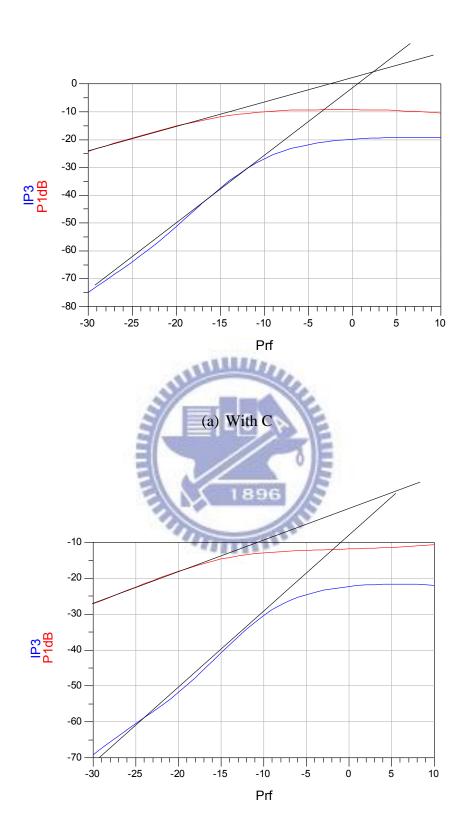
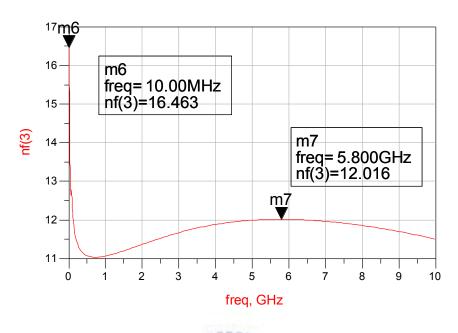


Fig 4.3 Isolation Lo-RF



(b) Without C

Fig 4.4 IIP3



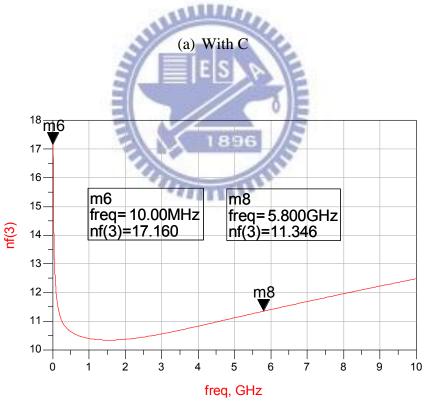


Fig 4.5 Noise Figure

Table 4.1 Compare with \boldsymbol{C} and without \boldsymbol{C}

	Power	Gain	Lo-If	Lo-RF	NF	IIP3
	(mW)	(dB)	Isolation	Isolation	(dB)	(dBm)
			(dB)	(dB)		
Without						
Cross C	1.7	5.3	-0.23	-316.807	17.16	>5
Pre-sim						
With						
Cross C	1.7	5.896	-7.369	-48.794	16.463	>3
Po-sim						



4.2 Measurement

In this section, we show two conditions of voltage. First is the origin voltage's situation. The other is we tune a little VDD voltage to make the results close to our simulation data.

Table 4.2 Different condition

	VDD	VrF	VLo	Icircuit	Power	Itotal
Condition	1.8V	0.7V	1V	1.12mA	2.06mW	25.3mA
1						
Condition	2.0V	0.7V	1V	1.36mA	2.72mW	26.6mA
2			h-onested a			

And there following table gives calibrate numbers for measure.

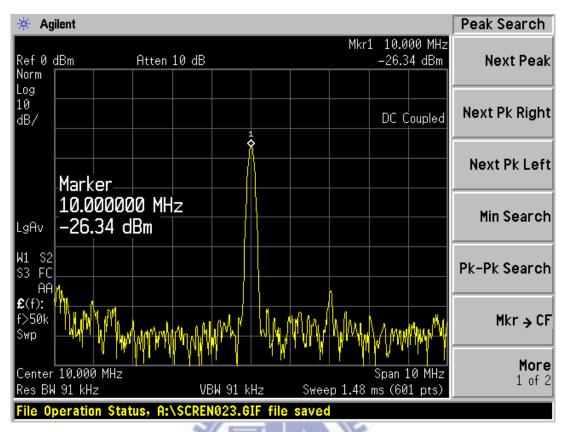
Table 4.3 Calibrate number

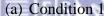
		FRENCH OF		The state of the latest of the		
	Lo	RF port	IF port	Lo port	RF port	IF port
RF input	input	loss	loss	loss	loss	loss
		@5.8GHz	@10MHz	@5.81GHz	@5.81GHz	@5.81GHz
-27.1dBm	0dBm	-2.91dB	-1.1dB	-7dB	-2.91dB	-2.91dB

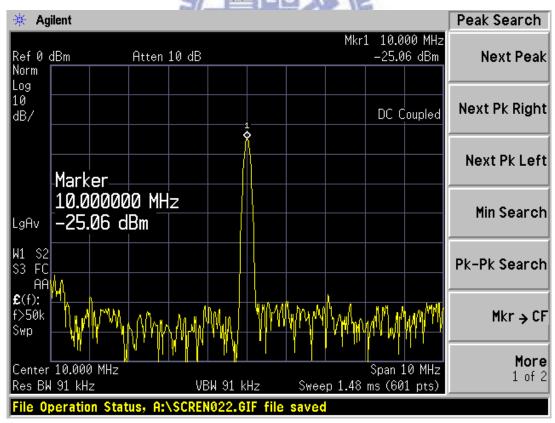
Gain = (measure_data - RF_port_loss) - (RF_input + IF_loss)

Isolation_Lo-IF = (measure_data - IF_port_loss) - (Lo_input + Lo_loss)

Isolation_Lo-RF = (measure_data - RF_port_loss) - (Lo_input + Lo_loss)

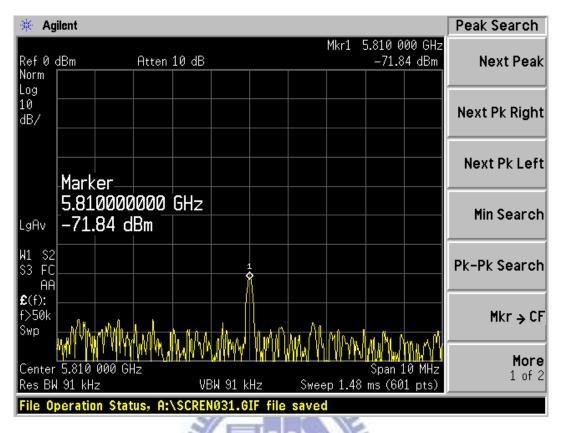


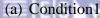


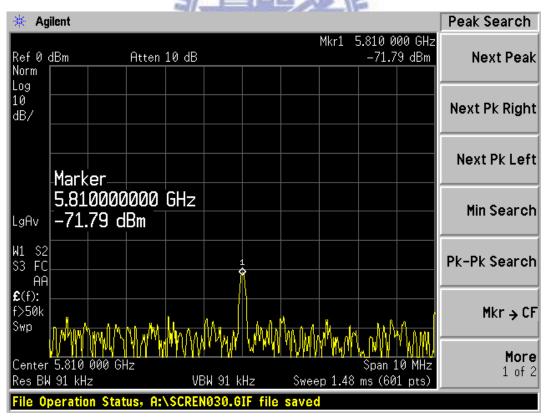


(b) Condition 2

Fig 4.6 Gain

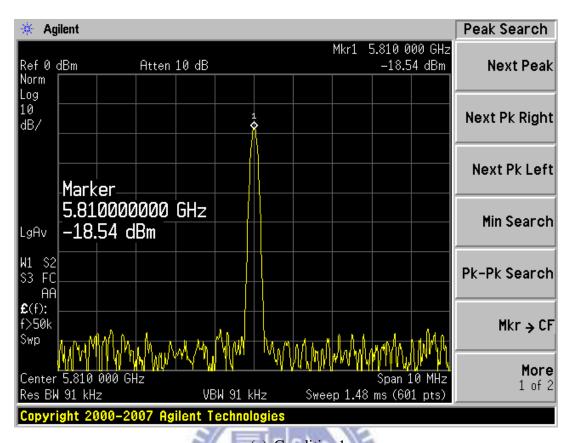


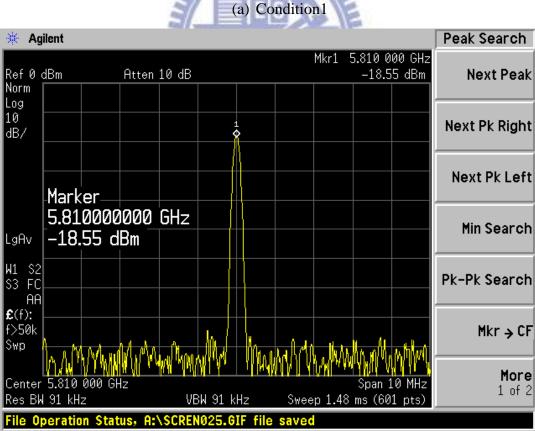




(b) Condition 2

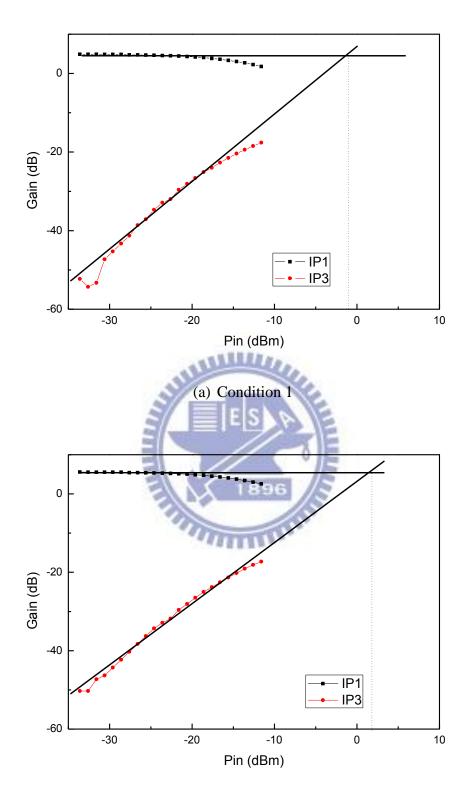
Fig 4.7 Isolation Lo-RF





(b) Condition 2

Fig 4.8 Isolation Lo-IF



(b) Condition 2

Fig 4.9 IIP3

4.3 Specification

Table 4.4 Spec.

	Power	Gain	Lo-If	Lo-RF	NF	IIP3
	(mW)	(dB)	Isolation	Isolation	(dB)	(dBm)
			(dB)	(dB)		
Without						
Cross C	1.7	5.3	-0.23	-316.807	17.16	>5
Pre-sim						
With						
Cross C	1.7	5.896	-7.369	-48.794	16.463	>3
Po-sim						
Condition 1	2.06	4.81	-8.46	-62	18.32	-1
Condition 2	2.72	6.04	-8.45 E	-61.88	17.76	2

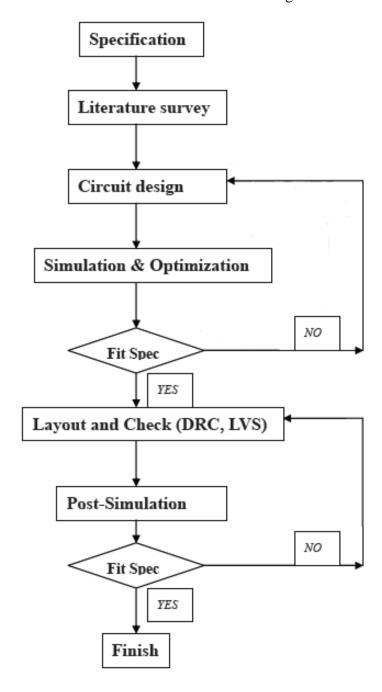
As we can see in Table 4.4, although condition1's power is more similar with simulation data, but condition 2's other data are more likely simulation. So finally we choose condition 2's data as our final data.

Chapter 5

Design Flow

5.1 Design flow

The simulation software ADS designer is used to design the circuit. ADS momentum is used to do EM simulation. After the layout of circuit is finished, DRC & LVS & LPE is done to check the correction for the design.



Chapter 6

Conclusion and Improvement

6.1 Conclusion

Although low power and good characteristics cannot take both, but we still can improve them to be better. We design a single-balance structure mixer, with 2.72mW of power consumption, 6.04dB of gain, -8.45dB of Lo-IF isolation, -61.88dB of Lo-RF isolation, 2dBm of IIP3, and 17.76dB of noise figure. In our measurement and simulation, noise figure is measure or simulate by single side band. So we need to minus 3dB as double side band measure. Now we compare our design to other reference.

As we can see on table 6.1, the power of our design is the best in the table, and also twice less than others. That's because the other reference always using double-balance structure to implement their idea circuit. Our performance in this table is almost the best design, but not in Lo-IF isolation. Born defect of single-balance structure is really cannot be totally cured. But we still improve a lot from origin 0dB to -8.45dB.

Table 6.1 Comparison of Mixer performance

Reference	Tech.	Power	RF	Gain	Lo-If	Lo-RF	NF	IIP3
	(CMOS)	(mW)	Freq	(dB)	Isolation	Isolation	(dB)	(dBm)
	(µm)		(GHz)		(dB)	(dB)		
[2]	0.18	18	2.4	-5.5	-30	-35	17	9.2
[3]*1	0.18	6.57	5.25	8.8	-18	-32	24	-11.7
[4]*1	0.18	6	2.12	20.55	-15.65	-130	9	-0.54
[5]	0.18	6.99	2.5	15	-30	NA	11.8	0
[6]	0.18	8.1	5.8	7.5	-40	>-40	10.9	-5
[7]	0.18	16.2	23	10.26	-	-26	>15	-
[8]	0.13	5.3	2-2.7	13.5	-	-	8	-6
Without C	0.18	1.7	5.8	5.3	-0.23	-316	14.2*2	>5
Po-sim	0.18	1.7	5.8	5.9	-7.37	-48.9	13.5*2	>3
Measurement	0.18	2.72	5.8	6.04	-8.45	-61.88	14.8*2	2

 $^{*^1}$ Design for low power.

^{*2}SSB measurement, minus 3dB as DSB data.

6.2 Improvement

The most important thing we need to improvement is Lo-IF isolation. After the project, we can find out two ways to improve it.

The first way is that we can change the layout. In fig 3.17, we can see lots of DC pad for bound wires. So many metal overlapping and close to each others may cause huge capacitance. Lo signal is 5.81GHz frequency, so the capacitance effect would more seriously. So if we cancel the pads and bias the voltages by bias tee, it can make the effect weaker.

As we mention before, Lo signal in IF port has two phases, and our design can only cancel one of it. But using Lo input is not the only way to cancel the signal, we can also find that in IF+ and IF- port, they have complete opposite phases of Lo feed-through. So we can use this situation and try another way to cancel them by each others.

Although our power is lower than others, but there still has chance to improve it.

If we add body bias to change V_{th} of MOS, the current can be achieved by smaller

VDD. By this way, we can make the DC power lower.

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