

## CHAPTER 3

### DIMENSIONLESS GROUPS AND UNCERTAINTY ANALYSIS

#### 3.1 Dimensionless Groups

The non-dimensional parameters associated with the flow considered here are the jet Reynolds number  $Re_j$ , based on the mean gas speed  $V_j$  at the injection pipe exit and the exit diameter of the injection pipe  $D_j$ , and the Rayleigh number  $Ra$ , based on the temperature difference between the heated disk and inlet gas  $\Delta T$  and the jet-to-disk separation distance  $H$ . They are defined as

$$Re_j = \frac{V_j D_j}{\nu} = \frac{4}{\pi} \frac{Q_j}{\nu D_j}, \quad (3.1)$$

and

$$Ra = \frac{g\beta(T_f - T_j)H^3}{\alpha\nu} = \frac{g\beta\Delta TH^3}{\alpha\nu} \quad (3.2)$$

where  $\alpha$  is the thermal diffusivity,  $g$  is the gravitational acceleration,  $\beta$  is the thermal expansion coefficient, and  $\nu$  is the kinematic viscosity.

#### 3.2 Uncertainty Analysis

An uncertainty analysis is carried out here to estimate the uncertainty levels in the experiment. Kline and McClintock [34] proposed a formula for evaluating the uncertainty in the result  $F$  as a function of independent variables,  $X_1, X_2, \dots, X_n$ ,

$$F = F(X_1, X_2, X_3, \dots, X_n) \quad (3.3)$$

The absolute uncertainty of  $F$  is expressed as

$$\delta F = \left\{ \left[ \left( \frac{\partial F}{\partial X_1} \right) \delta X_1 \right]^2 + \left[ \left( \frac{\partial F}{\partial X_2} \right) \delta X_2 \right]^2 + \left[ \left( \frac{\partial F}{\partial X_3} \right) \delta X_3 \right]^2 + \dots + \left[ \left( \frac{\partial F}{\partial X_n} \right) \delta X_n \right]^2 \right\}^{1/2} \quad (3.4)$$

and the relative uncertainty of  $F$  is

$$\frac{\delta F}{F} = \left\{ \left[ \left( \frac{\partial \ln F}{\partial \ln X_1} \right) \left( \frac{\delta X_1}{X_1} \right) \right]^2 + \left[ \left( \frac{\partial \ln F}{\partial \ln X_2} \right) \left( \frac{\delta X_2}{X_2} \right) \right]^2 + \dots + \left[ \left( \frac{\partial \ln F}{\partial \ln X_n} \right) \left( \frac{\delta X_n}{X_n} \right) \right]^2 \right\}^{1/2} \quad (3.5)$$

If  $F = X_1^a X_2^b X_3^c \dots \dots$ , then the relative uncertainty is

$$\frac{\delta F}{F} = \left[ \left( a \frac{\delta X_1}{X_1} \right)^2 + \left( b \frac{\delta X_2}{X_2} \right)^2 + \left( c \frac{\delta X_3}{X_3} \right)^2 + \dots \right]^{1/2} \quad (3.6)$$

where  $(\partial F / \partial X_i)$  and  $\delta X_i$  are, respectively, the sensitivity coefficient and uncertainty level associated with the variable  $\delta X_i$ . The values of the uncertainty intervals  $\delta X_i$  are obtained by a root-mean-square combination of the precision uncertainty of the instruments and the unsteadiness uncertainty, as recommended by Moffat [35]. The choice of the variable  $X_i$  to be included in the calculation of the total uncertainty level of the result  $F$  depends on the purpose of the analysis. The uncertainties for the chosen parameters are calculated as follows:

(1) Uncertainty of the measured temperature difference,  $\Delta T = T_f - T_j$

$$\delta(T_f - T_j) = [(\delta T_f)^2 + (\delta T_j)^2]^{1/2} \quad (3.7)$$

(2) The dependence of the air properties  $k$ ,  $\mu$ , and  $\nu$  on the temperature ( $T$  in K) [36] is

$$k = 1.195 \times 10^{-6} T^{1.6} / (T + 118)$$

$$\mu = 1.448 \times 10^{-6} T^{1.5} / (T + 118) \quad (3.8)$$

$$\nu = \mu / \rho$$

The uncertainties of the properties are

$$\begin{aligned} \frac{\delta k}{k} &= \frac{T}{k} \frac{\partial k}{\partial T} \frac{\delta T}{T} \\ \frac{\delta \rho}{\rho} &= \frac{T}{\rho} \frac{\partial \rho}{\partial T} \frac{\delta T}{T} \\ \frac{\delta \mu}{\mu} &= \frac{T}{\mu} \frac{\partial \mu}{\partial T} \frac{\delta T}{T} \end{aligned} \quad (3.9)$$

(3) Uncertainty of Rayleigh number,  $R_a$ ,

$$Ra = \frac{g\beta(T_f - T_j)H^3}{\alpha v} = \frac{g\beta\Delta TH^3}{\alpha v} \quad (3.10)$$

$$\frac{\delta Ra}{Ra} = \left[ \left( \frac{\delta g\beta}{g\beta} \right)^2 + \left( 3 \frac{\delta H}{H} \right)^2 + \left( \frac{\delta \Delta T}{\Delta T} \right)^2 + \left( \frac{\delta \alpha}{\alpha} \right)^2 + \left( \frac{\delta v}{v} \right)^2 \right]^{1/2} \quad (3.11)$$

(4) Uncertainty of jet Reynolds number,  $Re_j$ ,

$$Re_j = \frac{V_j D_j}{v} = \frac{4}{\pi} \frac{Q_j}{v D_j} \quad (3.12)$$

$$\frac{\delta Re_j}{Re_j} = \left[ \left( \frac{\delta v}{v} \right)^2 + \left( \frac{\delta Q_j}{Q_j} \right)^2 + \left( \frac{\delta D_j}{D_j} \right)^2 \right]^{1/2} \quad (3.13)$$

The results from this uncertainty analysis are summarized in Table 3.1.



**Table 3.1** Summary of uncertainty analysis

Parameter and Estimate Uncertainty	
Parameters	Uncertainty
$D_j, D_w, H$ (m)	$\pm 0.00005$ m
T (°C)	$\pm 0.2$ °C
$\Delta T$ (°C)	0.4 °C
$Q_j$ (slpm)	$\pm 2\%$
$\mu$ (Nm/s <sup>2</sup> )	$\pm 0.05\%$
$\rho$ (kg/m <sup>3</sup> )	$\pm 0.05\%$
$\nu$ (m <sup>2</sup> /s)	$\pm 0.07\%$
Ra	$\pm 8.6\%$
$Re_j$	$\pm 2.3\%$

