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Sample size determination for production yield estimation with multiple independent process characteristics

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ABSTRACT

Capability measure for processes yield with single characteristic has been investigated extensively, but is still comparatively neglected for processes with multiple characteristics. Wu and Pearn [Wu, C.W., Pearn, W.L., 2005. Measuring manufacturing capability for couplers and wavelength division multiplexers (WDM). International Journal of Advanced Manufacturing Technology 25(5/6), 533–541] proposed a capability index for multiple characteristics called C_{PU}^{T} , which provides an exact measure on process yield for multiple characteristics with each characteristic normally distributed. However, the exact sampling distribution of C_{PU}^{T} (multiple characteristics) is analytically intractable. In this paper, we apply the bootstrap method for calculating the lower confidence bounds of the index C_{PU}^{T} , and determine the sample size for a specified estimation accuracy. In order to obtain a desired estimation quality assurance, the sample size determination is essential as it provides the accuracy of the lower bound obtained from the bootstrap method. For convenience of applications, we tabulate the sample size required for various designated accuracy for the engineers/practitioners to use. A real-world example from manufacturing process with multiple characteristics is investigated to illustrate the applicability of the proposed approach.

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1. Introduction

Process capability indices (PCIS) are effective tools for quality assurance and process improvement. Numerous capability indices quantifying process potential and process performance are essential to any successful quality improvement activities and quality program implementation. Several basic capability indices have been widely used in manufacturing industry as follows:

$$C_p = \frac{USL - LSL}{6\sigma},\tag{1}$$

$$C_{PU} = \frac{USL - \mu}{3\sigma}, \qquad (2)$$

$$C_{PL} = \frac{\mu - LSL}{3\sigma},$$
(3)
$$C = \frac{USL - LSL}{(4)}$$

$$C_{pm} = \frac{602}{6\sqrt{\sigma^2 + (\mu - T)^2}},$$
(4)

$$C_{pk} = \min\left\{\frac{USL - \mu}{3\sigma}, \frac{\mu - LSL}{3\sigma}\right\},\tag{5}$$

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where USL and LSL are the upper and the lower specification limits, μ is the process mean, σ is the process standard deviation, and *T* is the target value.

In order to calculate the estimator, data must be collected. A great degree of uncertainty may be introduced into the capability assessments due to sampling errors. As the sampling errors have been ignored, the approach, simply by the calculated values of the estimated indices and then making a conclusion on whether the given process is capable, is highly unreliable. A reliable approach for estimating the true value of process capability is to determine the sample size for desired estimation accuracy. The sample size is directly related to the estimation accuracy and the cost of the data collection plan. The capability measurements for processes with single characteristic have been investigated extensively (see Kane, 1986; Pearn et al., 1992; Chen, 1998; Chen and Hsu, 2004; Cheng et al., 2006; Flaig, 2006; Vännman, 2006; Vännman and Albing, 2007). However, the lacks of these studies associated with analyzing the quality and efficiency of a process, are, so far, limited by discussing one single quality specification. In this paper, we consider the process capability with multiple characteristics to determine the sample size for desired estimation accuracy.

For process with multiple characteristics, several approaches have been suggested (see e.g. Bothe, 1992; Chen et al., 2003a,b; Castagliola and Castellanos, 2005; Huang et al., 2005; Wu and Pearn, 2005). For example, Bothe (1992) considered a simple





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measurement by taking the minimum measure of each single characteristic. For example, considering a *v*-characteristics product with *v*-yield measures P_1, P_2, \ldots, P_v , the overall process yield is measured as $P = \min\{P_1, P_2, \ldots, P_v\}$. Furthermore, Chen et al. (2003a) provided the process capability index with multi-characteristics as

$$S_{pk}^{T} = \frac{1}{3} \Phi^{-1} \left\{ \left[\prod_{j=1}^{\nu} (2\Phi(3S_{pkj}) - 1) + 1 \right] / 2 \right\},$$
(6)

where $\Phi(\cdot)$ is the cumulative distribution of the standard normal distribution N(0, 1), Φ^{-1} is the inverse function of $\Phi(\cdot)$, S_{pkj} denotes the S_{pk} value of the *j*th characteristic for j = 1, 2, ..., v, and v is the number of characteristics. This index, which provides an exact measurement on the process yield, establishes the relationship between the manufacturing specification and the actual process performance (Pearn and Cheng, 2007). Wu and Pearn (2005) discussed the process with multi-characteristics for one-sided specification and proposed a capability index as

$$C_{PU}^{T} = \frac{1}{3} \Phi^{-1} \left\{ \prod_{j=1}^{\nu} \Phi(3C_{PUj}) \right\},$$
(7)

where C_{PUj} denotes the C_{PU} value of the *j*th characteristic for j = 1, 2, ..., v, and *v* is the number of characteristics. A one-to-one correspondence relationship between the index C_{PU}^{T} and the overall process yield *P* can be established as

$$P = \prod_{j=1}^{\nu} P_j = \prod_{j=1}^{\nu} \Phi(3C_{PUj}) = \Phi(3C_{PU}^T).$$
(8)

Bootstrap approach seems to be a reasonable method for tackling the problem that the sampling distribution of C_{PU}^{T} (multiple characteristics) is analytically intractable. Since lower confidence bound estimates the minimum process capability conveying critical information regarding product quality, Wu and Pearn (2005) estimated the confidence bound by percentile bootstrap (PB) method. However, there are four types of bootstrap methods to estimate confidence bound, including the standard bootstrap confidence interval (SB), the percentile bootstrap confidence interval (PB), the biasedcorrected percentile bootstrap confidence interval (BCPB), and the bootstrap-t (BT) method. And the engineers/practitioners would want to know which one is recommended. In this paper, we compare the performance of confidence bound for the one-sided index C_{PU}^{T} with multiple characteristics by using these four bootstrap methods. The modified index C_{PU}^{T} proposed by Wu and Pearn (2005) are calculated. Furthermore, we find that the BCPB method would be the recommended method to estimate confidence bound in the general cases. We also provide the tables about the sample sizes required for various designated estimation accuracy for the engineers/practitioners to use in their factory applications. A realworld example from manufacturing process with multiple characteristics is investigated to illustrate the applicability of the proposed approach.

Table 1 Various C_{Pll}^{T} values and the corresponding process yield

| C_{PU}^{T} | Process yield |
|--------------|---------------|
| 1.00 | 0.9986501020 |
| 1.25 | 0.9999115827 |
| 1.33 | 0.9999669634 |
| 1.45 | 0.9999931931 |
| 1.50 | 0.9999966023 |
| 1.60 | 0.9999992067 |
| 1.67 | 0.9999997278 |
| 2.00 | 0.9999999990 |
| | |

Table 2

Minimal requirement for each single characteristic of various capability levels for multiple characteristics

| <i>c</i> ′ | c_L | |
|------------|-------|-------|
| | 1.000 | 1.33 |
| 1 | 1.000 | 1.330 |
| 2 | 1.068 | 1.383 |
| 3 | 1.107 | 1.414 |
| 4 | 1.133 | 1.436 |
| 5 | 1.153 | 1.452 |

| Table 3 |
|--|
| The total rank of the four bootstrap methods as $C_{rrr}^T = 1, 1.33$ and $v = 2(1)$ |

| | | | | | 10 | | | | |
|-------|----------------|-------|-------|-------|----------------|---------------------|-------|-------|--|
| n | $C_{PU}^T = 1$ | | | | $C_{PU}^T = 1$ | $C_{PU}^{T} = 1.33$ | | | |
| | SB | PB | BCPB | PT | SB | PB | BCPB | PT | |
| v = 2 | | | | | | | | | |
| 30 | 3 | 2 | 1.006 | 3.994 | 2.996 | 1.996 | 1.008 | 4.000 | |
| 40 | 2.996 | 2.004 | 1.004 | 3.996 | 2.982 | 2.008 | 1.034 | 3.974 | |
| 50 | 2.992 | 2.002 | 1.024 | 3.982 | 2.99 | 2.012 | 1.030 | 3.968 | |
| 60 | 2.982 | 2.014 | 1.042 | 3.962 | 2.984 | 2.010 | 1.056 | 3.950 | |
| 70 | 2.994 | 2.004 | 1.018 | 3.984 | 2.984 | 2.020 | 1.030 | 3.966 | |
| 80 | 2.988 | 2.012 | 1.026 | 3.974 | 2.972 | 2.028 | 1.072 | 3.928 | |
| 90 | 2.994 | 2.016 | 1.022 | 3.968 | 2.970 | 2.026 | 1.084 | 3.920 | |
| 100 | 2.980 | 2.020 | 1.026 | 3.974 | 2.992 | 2.002 | 1.072 | 3.934 | |
| 125 | 3.000 | 2.010 | 1.018 | 3.972 | 2.968 | 2.040 | 1.104 | 3.888 | |
| 150 | 2.988 | 2.012 | 1.040 | 3.960 | 2.974 | 2.056 | 1.094 | 3.876 | |
| 200 | 3.004 | 2.018 | 1.036 | 3.942 | 2.972 | 2.018 | 1.148 | 3.858 | |
| v = 3 | | | | | | | | | |
| 30 | 2.966 | 2.028 | 1.1 | 3.906 | 2.942 | 2.048 | 1.112 | 3.896 | |
| 40 | 2.95 | 2.04 | 1.106 | 3.904 | 2.954 | 2.046 | 1.132 | 3.868 | |
| 50 | 2.97 | 2.034 | 1.1 | 3.896 | 2.946 | 2.044 | 1.15 | 3.86 | |
| 60 | 2.942 | 2.07 | 1.124 | 3.864 | 2.922 | 2.094 | 1.216 | 3.768 | |
| 70 | 2.954 | 2.052 | 1.12 | 3.874 | 2.916 | 2.112 | 1.29 | 3.678 | |
| 80 | 2.944 | 2.062 | 1.172 | 3.818 | 2.904 | 2.108 | 1.332 | 3.656 | |
| 90 | 2.94 | 2.078 | 1.166 | 3.816 | 2.836 | 2.168 | 1.428 | 3.568 | |
| 100 | 2.934 | 2.072 | 1.162 | 3.828 | 2.894 | 2.136 | 1.352 | 3.61 | |
| 125 | 2.964 | 2.06 | 1.124 | 3.852 | 2.832 | 2.172 | 1.59 | 3.406 | |
| 150 | 2.97 | 2.044 | 1.136 | 3.848 | 2.804 | 2.176 | 1.62 | 3.398 | |
| 200 | 2.918 | 2.114 | 1.2 | 3.768 | 2.784 | 2.23 | 1.636 | 3.344 | |
| v = 4 | | | | | | | | | |
| 30 | 2.97 | 2.052 | 1.116 | 3.856 | 2.94 | 2.076 | 1.17 | 3.814 | |
| 40 | 2.912 | 2.084 | 1.208 | 3.796 | 2.882 | 2.11 | 1.3 | 3.708 | |
| 50 | 2.922 | 2.094 | 1.224 | 3.76 | 2.826 | 2.186 | 1.508 | 3.478 | |
| 60 | 2.91 | 2.096 | 1.222 | 3.772 | 2.798 | 2.188 | 1.53 | 3.478 | |
| 70 | 2.882 | 2.126 | 1.254 | 3.736 | 2.822 | 2.186 | 1.664 | 3.328 | |
| 80 | 2.916 | 2.108 | 1.26 | 3.716 | 2.79 | 2.274 | 1.666 | 3.268 | |
| 90 | 2.892 | 2.12 | 1.318 | 3.668 | 2.742 | 2.272 | 1.784 | 3.196 | |
| 100 | 2.886 | 2.124 | 1.28 | 3.706 | 2.73 | 2.308 | 1.85 | 3.11 | |
| 125 | 2.922 | 2.126 | 1.308 | 3.644 | 2.634 | 2.4 | 2.054 | 2.912 | |
| 150 | 2.92 | 2.1 | 1.328 | 3.648 | 2.684 | 2.412 | 2.034 | 2.868 | |
| 200 | 2.88 | 2.152 | 1.394 | 3.57 | 2.632 | 2.434 | 2.322 | 2.606 | |
| v = 5 | | | | | | | | | |
| 30 | 2.938 | 2.084 | 1.222 | 3.756 | 2.86 | 2.15 | 1.398 | 3.59 | |
| 40 | 2.878 | 2.118 | 1.314 | 3.688 | 2.786 | 2.216 | 1.652 | 3.344 | |
| 50 | 2.892 | 2.148 | 1.326 | 3.63 | 2.792 | 2.24 | 1.648 | 3.316 | |
| 60 | 2.85 | 2.16 | 1.408 | 3.582 | 2.758 | 2.254 | 1.828 | 3.156 | |
| 70 | 2.846 | 2.158 | 1.45 | 3.542 | 2.686 | 2.336 | 2.026 | 2.942 | |
| 80 | 2.902 | 2.18 | 1.382 | 3.528 | 2.654 | 2.4 | 2.11 | 2.83 | |
| 90 | 2.876 | 2.172 | 1.5 | 3.452 | 2.572 | 2.432 | 2.288 | 2.702 | |
| 100 | 2.83 | 2.192 | 1.56 | 3.406 | 2.582 | 2.478 | 2.384 | 2.55 | |
| 125 | 2.904 | 2.156 | 1.514 | 3.42 | 2.56 | 2.482 | 2.6 | 2.354 | |
| 150 | 2.856 | 2.228 | 1.572 | 3.342 | 2.466 | 2.524 | 2.648 | 2.346 | |
| 200 | 2.834 | 2.244 | 1.578 | 3.34 | 2.426 | 2.614 | 2.878 | 2.074 | |

2. Capability measures for multiple characteristics

Capability measure for processes with single characteristic has been investigated extensively. For normally distributed processes with a one-sided specification limit, USL or LSL, the process yield



Fig. 1a. The total rank of the four bootstrap methods as $C_{PU}^{T} = 1$, v = 2.



Fig. 1b. The total rank of the four bootstrap methods as $C_{PU}^{T} = 1$, v = 3.



Fig. 1c. The total rank of the four bootstrap methods as $C_{PU}^T = 1$, v = 4.

is listed in the following, where Z follows the standard normal distribution N(0,1)

$$P(X < USL) = P\left(\frac{X - \mu}{\sigma} < \frac{USL - \mu}{\sigma}\right) = P(Z < 3C_{PU}) = \Phi(3C_{PU}), \quad (9)$$

$$P(X > LSL) = P\left(\frac{X - \mu}{\sigma} > \frac{LSL - \mu}{\sigma}\right) = P(-Z < 3C_{PL}) = \Phi(3C_{PL}).$$
(10)

For easier presentation, we denote C_I as either C_{PU} or C_{PL} . Thus, process capability index C_I provides an exact measure of the potential process yield for processes with a one-sided manufacturing specification. The corresponding process yield for a well controlled normally distributed process is easily calculated as Φ (3 C_I).

Considering processes with v-characteristics (assuming characteristics are mutually independent) and v yield measures



Fig. 1d. The total rank of the four bootstrap methods as $C_{PU}^T = 1$, v = 5.



Fig. 2a. The total rank of the four bootstrap methods as $C_{PU}^T = 1.33$, v = 2.



Fig. 2b. The total rank of the four bootstrap methods as $C_{PU}^{T} = 1.33$, v = 3.

 P_1, P_2, \ldots, P_V , Wu and Pearn (2005) suggested that the overall process yield should be calculated as $P = P_1 \times P_2 \times \ldots \times P_V$ which is significantly less than the calculated one. From the definition of one-sided yield index in (9), the process yield index with single characteristic can be rewritten as

$$C_{PU} = \frac{1}{3} \Phi^{-1} \bigg\{ \Phi(\frac{USL - \mu}{\sigma}) \bigg\},\tag{11}$$

where $\Phi(\cdot)$ is the cumulative distribution of the standard normal distribution N(0,1), and Φ^{-1} is the inverse function of $\Phi(\cdot)$. For the process with multiple quality characteristics, a simple measure by taking the minimum of the measure of each single characteristic



Fig. 2c. The total rank of the four bootstrap methods as $C_{PU}^{T} = 1.33$, v = 4.



Fig. 2d. The total rank of the four bootstrap methods as $C_{PII}^T = 1.33$, v = 5.

Table 4 Sample size *n* required for $R_{\gamma} \ge R_{PU}$, with quality characteristics v = 3, $R_{PU} = 0.75(0.01)0.95$, $\gamma = 0.9$, 0.95, 0.975, 0.99, and $C_{PU}^{T} = 1$

| R _{PU} | $\gamma = 0.9$ | 90 | $\gamma = 0.9$ | 95 | $\gamma = 0.9$ | 975 | $\gamma = 0.9$ |)9 |
|-----------------|----------------|--------|----------------|--------|----------------|--------|----------------|--------|
| | n | Rγ | n | Rγ | n | Rγ | n | Rγ |
| 0.75 | - | - | - | - | - | - | 16 | 0.7518 |
| 0.76 | - | - | - | - | 6 | - | 21 | 0.7609 |
| 0.77 | - | - | - | - | 7 | 0.7776 | 24 | 0.7731 |
| 0.78 | - | - | - | - | 14 | 0.7832 | 28 | 0.7807 |
| 0.79 | - | - | - | - | 18 | 0.7904 | 31 | 0.7901 |
| 0.80 | - | - | 6 | - | 22 | 0.8005 | 36 | 0.8012 |
| 0.81 | - | - | 12 | 0.8119 | 26 | 0.8107 | 40 | 0.8103 |
| 0.82 | - | - | 17 | 0.8222 | 32 | 0.8226 | 49 | 0.8201 |
| 0.83 | - | - | 23 | 0.8316 | 38 | 0.8304 | 56 | 0.8305 |
| 0.84 | - | - | 28 | 0.8414 | 44 | 0.8403 | 65 | 0.8414 |
| 0.85 | 6 | - | 35 | 0.8536 | 52 | 0.8502 | 75 | 0.8502 |
| 0.86 | 18 | 0.8608 | 41 | 0.8600 | 63 | 0.8613 | 88 | 0.8609 |
| 0.87 | 26 | 0.8708 | 51 | 0.8710 | 73 | 0.8700 | 105 | 0.8710 |
| 0.88 | 33 | 0.8805 | 60 | 0.8802 | 88 | 0.8800 | 124 | 0.8812 |
| 0.89 | 44 | 0.8909 | 76 | 0.8912 | 105 | 0.8908 | 146 | 0.8610 |
| 0.90 | 54 | 0.9005 | 93 | 0.9004 | 128 | 0.9000 | 176 | 0.9005 |
| 0.91 | 71 | 0.9107 | 115 | 0.9102 | 158 | 0.9103 | 213 | 0.9101 |
| 0.92 | 92 | 0.9205 | 146 | 0.9201 | 197 | 0.9204 | 268 | 0.9202 |
| 0.93 | 121 | 0.9306 | 188 | 0.9303 | 253 | 0.9300 | 339 | 0.9302 |
| 0.94 | 164 | 0.9400 | 251 | 0.9402 | 337 | 0.9400 | 451 | 0.9400 |
| 0.95 | 231 | 0.9500 | 350 | 0.9502 | 473 | 0.9505 | 634 | 0.9500 |

has been considered. Wu and Pearn (2005) proposed the following overall capability index is referred to as:

$$C_{PU}^{T} = \frac{1}{3} \Phi^{-1} \left\{ \prod_{j=1}^{\nu} \Phi(3C_{PUj}) \right\},$$
(12)

Table 5

Sample size *n* required for $R_{\gamma} \ge R_{PU}$, with quality characteristics v = 3, $R_{PU} = 0.75(0.01)0.95$, $\gamma = 0.9$, 0.95, 0.975, 0.99, and $C_{pu}^{-} = 1.33$

| R _{PU} | $\gamma = 0.9$ | 90 | γ = 0 .9 | 95 | $\gamma = 0.9$ | 975 | $\gamma = 0.9$ | 99 |
|-----------------|----------------|--------|-----------------|--------|----------------|--------|----------------|--------|
| | n | Rγ | n | Rγ | n | Rγ | n | Rγ |
| 0.75 | - | - | - | - | 6 | - | 19 | 0.7533 |
| 0.76 | - | - | - | - | 8 | 0.7608 | 22 | 0.7600 |
| 0.77 | - | - | - | - | 14 | 0.7721 | 24 | 0.7719 |
| 0.78 | - | - | - | - | 17 | 0.7820 | 28 | 0.7813 |
| 0.79 | - | - | - | - | 21 | 0.7923 | 33 | 0.7914 |
| 0.80 | - | - | 6 | 0.8074 | 24 | 0.8008 | 38 | 0.8019 |
| 0.81 | - | - | 16 | 0.8119 | 28 | 0.8109 | 41 | 0.8101 |
| 0.82 | - | - | 19 | 0.8200 | 33 | 0.8209 | 50 | 0.8219 |
| 0.83 | - | - | 24 | 0.8310 | 40 | 0.8334 | 57 | 0.8320 |
| 0.84 | 6 | - | 31 | 0.8421 | 44 | 0.8406 | 65 | 0.8400 |
| 0.85 | 12 | 0.8518 | 35 | 0.8519 | 54 | 0.8506 | 77 | 0.8524 |
| 0.86 | 21 | 0.8615 | 42 | 0.8613 | 62 | 0.8602 | 88 | 0.8603 |
| 0.87 | 26 | 0.8700 | 51 | 0.8705 | 73 | 0.8704 | 102 | 0.8705 |
| 0.88 | 34 | 0.8807 | 62 | 0.8817 | 89 | 0.8814 | 122 | 0.8814 |
| 0.89 | 43 | 0.8910 | 74 | 0.8902 | 104 | 0.8904 | 145 | 0.8906 |
| 0.90 | 55 | 0.9010 | 91 | 0.9009 | 129 | 0.9017 | 174 | 0.9010 |
| 0.91 | 72 | 0.9118 | 113 | 0.9101 | 157 | 0.9109 | 213 | 0.9101 |
| 0.92 | 89 | 0.9202 | 144 | 0.9211 | 196 | 0.9201 | 269 | 0.9204 |
| 0.93 | 118 | 0.9303 | 184 | 0.9301 | 254 | 0.9301 | 348 | 0.9301 |
| 0.94 | 159 | 0.9400 | 249 | 0.9400 | 340 | 0.9400 | 501 | 0.9421 |
| 0.95 | 226 | 0.9501 | 353 | 0.9501 | 481 | 0.9500 | 658 | 0.9500 |

where C_{PUj} denotes the C_{PU} value of the *j*th characteristic for j = 1, 2, ..., v, and v is the number of characteristics. The index, C_{PU}^{T} , can be a generalization of the single characteristic yield index. Let $C_{PU}^{T} = c$, we have

$$\left\{\prod_{j=1}^{\nu} \Phi(3C_{PUj})\right\} = \Phi(3c).$$
(13)

In fact, Wu and Pearn (2005) showed that the one-to-one correspondence relationship between the index C_{PU}^{T} and the overall process yields *P* can be established as follows:

$$P = \prod_{j=1}^{\nu} P_j = \prod_{j=1}^{\nu} \Phi(3C_{PUj}) = \Phi(3C_{PUj}^T).$$
(14)

Hence, the new index C_{PU}^{T} provides an exact measure on the overall process yield when the characteristics are mutually independent. For example, if $C_{PU}^{T} = 1.00$, the entire process yield would be exactly 99.865%, and each single characteristic yield is no less than $(0.9986501)^{1/5} = 0.9997299$ (equivalent to 270 NCPPM). Table 1 displays various commonly used capability requirement and the corresponding overall process yield.

Wu and Pearn (2005) also showed that for process with *v* characteristics, if the requirement for the overall process capability is $C_{PU}^T \ge c_0$, a sufficient condition (which is minimal) for the requirement to each single characteristic can be obtained by the following. Let *c'* be the minimum C_{PUj} required for each single characteristic, then

$$\frac{1}{3} \Phi^{-1} \left\{ \prod_{j=1}^{\nu} \Phi(3C_{PUj}) \right\} \ge \frac{1}{3} \Phi^{-1} \left\{ \prod_{j=1}^{\nu} \Phi(3c') \right\} \ge c_0.$$

$$(15)$$

We can obtain the lower bound of each single characteristic to be

$$c_L = \frac{1}{3} \Phi^{-1} \left(\sqrt[v]{\Phi(3c_0)} \right).$$
(16)

Table 2 displays the minimum c_L of C_{PUj} for the required overall process capability C_{PU}^{T} are 1.00 and 1.33 for v = 1(1)5 characteristics. For example, if the overall capability requirement $C_{PU}^{T} \ge 1.00$ would be satisfied, it means each single characteristic yield is no less than $(0.9986501)^{1/5} = 0.9997299$ (equivalent to 270 NCPPM), and the capability for all the five characteristics is the following, for j = 1, 2, ..., 5.

overlay ♠



Fig. 3. Deposited layers on TFT-LCD.



Fig. 4. Exposure process on panel window.

Table 6

Specifications for thin film transistor liquid crystal display

| Parameter | Specifications |
|--------------------|----------------|
| Overlay | ≼0.1 μm |
| Critical dimension | ≼0.3 μm |
| Uniformality | ≼0.03 |

$$C_{PUj} = \frac{1}{3} \Phi^{-1} \left(\sqrt[5]{\Phi(3)} \right) = 1.153 \quad \text{for } j = 1, 2, \dots, 5.$$
 (17)

3. Bootstrap methods for calculating the lower bounds of C_{PU}^{T}

3.1. Lower confidence bounds on C_{PU}^{T}

For each single characteristic, the C_{PU_j} values can be estimated by their natural estimators $\widehat{C}_{PU_j} = (USL_j - \bar{x}_j)/s_j$, j = 1, 2, ..., v, where \bar{x}_j and s_j are the sample mean and the sample standard deviation of the *j*th characteristic, respectively. Thus, the estimator of \widehat{C}_{PU}^T are defined as

$$\widehat{C}_{PU}^{T} = \frac{1}{3} \Phi^{-1} \Biggl\{ \prod_{j=1}^{\nu} \Phi(3\widehat{C}_{PUj}) \Biggr\}.$$
(18)

In order to calculate the estimator of C_{PU}^{I} , however, sample data must be collected. Therefore, due to sampling errors, a great degree of uncertainty may be introduced into capability assessments. It is highly unreliable simply by the calculated values of the estimated indices and then making a conclusion on whether the given process is capable. Since the sampling errors have been ignored, a reliable

 Table 7

 Calculations for process capability of the overlay, critical dimension and uniformality

| Characteristics USI | x | S | C _{PUj} | L _C |
|--|----------|---------|------------------|----------------|
| Overlay0.1Critical dimension0.1Uniformality0.0 | 0.0795 | 0.0065 | 1.0499 | 0.9394 |
| | 0.2693 | 0.0083 | 1.2298 | 1.1016 |
| | 3 0.0267 | 0.00097 | 1.1404 | 1.0215 |

approach for estimating the true value of process index is to construct the lower confidence bound.

Determination of the lower confidence bound on the actual process capability is essential for quality assurance. The lower confidence bound can not only be essential to production yield assurance, but also be used in capability testing for decision making. Since the sample size provides the accuracy of the lower bound, for the given desired estimation accuracy R_{PU} ($R_{PU} = C_{PU}^{T(LB)}$) where $C_{PU}^{T(LB)}$ is the lower confidence bound on C_{PU}^{T}) and the confidence level γ (ensures that the risk of making incorrect decisions will be no larger than the preset Type I error $1 - \gamma$), the approximate sample size must be obtained. Before estimating the sample size, it is necessary to determine a desired lower confidence bound for C_{PU}^{T} , depending on the ratio of $R_{PU} = C_{PU}^{T(LB)}/\hat{C}_{PU}^{T}$. Hence, we need to compute the lower confidence bound to determine sample sizes required for specified estimation accuracy of the C_{PU}^{T} .

While the sampling distribution of the estimator \hat{C}_{PU}^{T} for multiple samples is unknown, we use the nonparametric bootstrap method and the following to estimate the lower confidence bound $C_{PU}^{T(LB)}$. Efron (1981) introduced a nonparametric, computational intensive but effective estimation method, called the "Bootstrap", which is a data-based simulation technique for statistical inference. The merit of the nonparametric bootstrap approach is that it does not rely on any assumptions regarding the underlying distribution. The bootstrap sampling is equivalent to sampling (with replacement) from the empirical probability distribution function. The essence of bootstrapping is that, without any knowledge about a population, the distribution found in a random sample of size *n* from the population is the best guide to the distribution in the population. By resampling observations from the observed data, the population that consists of the n observed sample values is used to model the unknown real population.

In the bootstrap, *B* new samples, each of the same size as the observed data *n*, are drawn with replacement from the population. Efron and Tibshirani (1986) developed four types of bootstrap confidence interval, including the standard bootstrap confidence interval (SB), the percentile bootstrap confidence interval (PB), the biased-corrected percentile bootstrap confidence interval (BCPB), and the bootstrap-*t* (BT) method. Franklin and Wasserman (1992) investigated the lower confidence bounds for the capability indices, C_p , C_{pk} and C_{pm} using these bootstrap methods. Some simulations results indicate that for normal processes the bootstrap confidence limits perform equally well (see Chou et al., 1990 and Bissell, 1990). In the following, we give an overview of four Bootstrap confidence bounds of the index.

3.2. Bootstrap methods

3.2.1. Standard bootstrap (SB)

From the *B* bootstrap estimator \hat{C}_{PU}^{T*} , the sample average and the sample standard deviation are calculated as follows:

$$\widehat{C}_{PU}^{T_*} = \frac{1}{B} \sum_{i=1}^{B} \widehat{C}_{PU}^{T_*}(i),$$
(19)

$$S_{\mathcal{C}_{PU}}^{*} = \sqrt{\frac{1}{B-1} \sum_{I=1}^{B} [\widehat{C}_{PU}^{T*}(i) - \widehat{C}_{PU}^{T*}]^2},$$
(20)

 Table 8

 Calculations for overall yield index

| Characteristic | \widehat{C}_{PU}^{T} | NCPPM | $C_{PU}^{T(LB)}$ | NCPPM |
|----------------|------------------------|-------|------------------|-------|
| LCD | 1.0085 | 1241 | 0.9277 | 2692 |

| Tal | ole 9 | | |
|-----|-------|--|--|
| | | | |

| The 150 sample observations for | r three quality | characteristics |
|---------------------------------|-----------------|-----------------|
|---------------------------------|-----------------|-----------------|

| Overlay (µm |): USL = 0.1 μm | | | | | | | | |
|---------------|---------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0.0779 | 0.0697 | 0.0764 | 0.0763 | 0.0834 | 0.0860 | 0.0778 | 0.0849 | 0.0846 | 0.0649 |
| 0.0853 | 0.0801 | 0.0711 | 0.0847 | 0.0817 | 0.0747 | 0.0886 | 0.0777 | 0.0889 | 0.0716 |
| 0.0802 | 0.0776 | 0.0800 | 0.0811 | 0.0873 | 0.0804 | 0.0810 | 0.0729 | 0.0782 | 0.0794 |
| 0.0711 | 0.0712 | 0.0724 | 0.0839 | 0.0831 | 0.0846 | 0.0803 | 0.0851 | 0.0701 | 0.0741 |
| 0.0706 | 0.0826 | 0.0665 | 0.0843 | 0.0862 | 0.0824 | 0.0810 | 0.0804 | 0.0838 | 0.0693 |
| 0.0757 | 0.0842 | 0.0765 | 0.0742 | 0.0838 | 0.0832 | 0.0837 | 0.0745 | 0.0820 | 0.0911 |
| 0.0786 | 0.0751 | 0.0738 | 0.0801 | 0.0853 | 0.0667 | 0.0778 | 0.0888 | 0.0890 | 0.0638 |
| 0.0796 | 0.0859 | 0.0718 | 0.0799 | 0.0637 | 0.0789 | 0.0878 | 0.0926 | 0.0674 | 0.0745 |
| 0.0859 | 0.0913 | 0.0863 | 0.0695 | 0.0878 | 0.0753 | 0.0790 | 0.0798 | 0.0801 | 0.0736 |
| 0.0746 | 0.0885 | 0.0788 | 0.0746 | 0.0862 | 0.0787 | 0.0753 | 0.0793 | 0.0776 | 0.0945 |
| 0.0833 | 0.0709 | 0.0804 | 0.0780 | 0.0888 | 0.0842 | 0.0794 | 0.0793 | 0.0771 | 0.0835 |
| 0.0691 | 0.0806 | 0.0805 | 0.0735 | 0.0843 | 0.0837 | 0.0727 | 0.0834 | 0.0752 | 0.0877 |
| 0.0771 | 0.0850 | 0.0755 | 0.0826 | 0.0776 | 0.0833 | 0.0669 | 0.0740 | 0.0839 | 0.0743 |
| 0.0781 | 0.0754 | 0.0840 | 0.0840 | 0.0962 | 0.0780 | 0.0801 | 0.0742 | 0.0781 | 0.0908 |
| 0.0911 | 0.0849 | 0.0764 | 0.0932 | 0.0783 | 0.0732 | 0.0722 | 0.0775 | 0.0787 | 0.0715 |
| Critical dime | nsion (µm): USL = (| 0.1 μm | | | | | | | |
| 0.2559 | 0.2627 | 0.2717 | 0.2656 | 0.2756 | 0.2747 | 0.2645 | 0.2671 | 0.2588 | 0.2703 |
| 0.2689 | 0.2633 | 0.2694 | 0.2573 | 0.2691 | 0.2776 | 0.2550 | 0.2632 | 0.2624 | 0.2605 |
| 0.2783 | 0.2623 | 0.2691 | 0.2571 | 0.2616 | 0.2759 | 0.2670 | 0.2688 | 0.2598 | 0.2620 |
| 0.2788 | 0.2507 | 0.2661 | 0.2726 | 0.2807 | 0.2735 | 0.2673 | 0.2478 | 0.2831 | 0.2653 |
| 0.2691 | 0.2792 | 0.2718 | 0.2791 | 0.2770 | 0.2581 | 0.2731 | 0.2660 | 0.2612 | 0.2718 |
| 0.2657 | 0.2711 | 0.2579 | 0.2649 | 0.2760 | 0.2707 | 0.2769 | 0.2605 | 0.2648 | 0.2723 |
| 0.2657 | 0.2650 | 0.2764 | 0.2827 | 0.2734 | 0.2676 | 0.2757 | 0.2662 | 0.2758 | 0.2753 |
| 0.2514 | 0.2654 | 0.2754 | 0.2842 | 0.2524 | 0.2734 | 0.2687 | 0.2743 | 0.2631 | 0.2719 |
| 0.2726 | 0.2828 | 0.2750 | 0.2721 | 0.2633 | 0.2608 | 0.2877 | 0.2628 | 0.2894 | 0.2638 |
| 0.2700 | 0.2654 | 0.2819 | 0.2728 | 0.2713 | 0.2670 | 0.2580 | 0.2730 | 0.2652 | 0.2794 |
| 0.2656 | 0.2850 | 0.2735 | 0.2774 | 0.2730 | 0.2757 | 0.2640 | 0.2707 | 0.2564 | 0.2634 |
| 0.2638 | 0.2727 | 0.2681 | 0.2647 | 0.2720 | 0.2687 | 0.2627 | 0.2828 | 0.2838 | 0.2700 |
| 0.2638 | 0.2640 | 0.2797 | 0.2708 | 0.2704 | 0.2475 | 0.2713 | 0.2710 | 0.2870 | 0.2610 |
| 0.2651 | 0.2729 | 0.2698 | 0.2702 | 0.2694 | 0.2586 | 0.2619 | 0.2790 | 0.2723 | 0.2833 |
| 0.2709 | 0.2592 | 0.2740 | 0.2598 | 0.2557 | 0.2790 | 0.2714 | 0.2874 | 0.2656 | 0.2789 |
| Uniformality | : USL = 0.03 | | | | | | | | |
| 0.0272 | 0.0264 | 0.0255 | 0.0267 | 0.0248 | 0.0272 | 0.0270 | 0.0267 | 0.0257 | 0.0265 |
| 0.0264 | 0.0265 | 0.0252 | 0.0278 | 0.0263 | 0.0272 | 0.0252 | 0.0264 | 0.0264 | 0.0247 |
| 0.0271 | 0.0276 | 0.0268 | 0.0293 | 0.0283 | 0.0265 | 0.0269 | 0.0275 | 0.0277 | 0.0257 |
| 0.0255 | 0.0269 | 0.0259 | 0.0271 | 0.0273 | 0.0256 | 0.0278 | 0.0283 | 0.0267 | 0.0277 |
| 0.0254 | 0.0265 | 0.0280 | 0.0283 | 0.0262 | 0.0269 | 0.0267 | 0.0266 | 0.0263 | 0.0261 |
| 0.0269 | 0.0270 | 0.0262 | 0.0279 | 0.0252 | 0.0255 | 0.0277 | 0.0254 | 0.0262 | 0.0279 |
| 0.0265 | 0.0271 | 0.0286 | 0.0252 | 0.0261 | 0.0266 | 0.0278 | 0.0270 | 0.0255 | 0.0274 |
| 0.0244 | 0.0272 | 0.0279 | 0.0259 | 0.0266 | 0.0265 | 0.0256 | 0.0274 | 0.0266 | 0.0282 |
| 0.0268 | 0.0260 | 0.0256 | 0.0253 | 0.0268 | 0.0287 | 0.0270 | 0.0294 | 0.0265 | 0.0258 |
| 0.0275 | 0.0265 | 0.0282 | 0.0270 | 0.0266 | 0.0267 | 0.0254 | 0.0270 | 0.0277 | 0.0257 |
| 0.0278 | 0.0255 | 0.0274 | 0.0260 | 0.0273 | 0.0269 | 0.0256 | 0.0293 | 0.0256 | 0.0274 |
| 0.0249 | 0.0265 | 0.0269 | 0.0269 | 0.0268 | 0.0267 | 0.0262 | 0.0266 | 0.0271 | 0.0269 |
| 0.0252 | 0.0257 | 0.0286 | 0.0267 | 0.0265 | 0.0270 | 0.0270 | 0.0261 | 0.0264 | 0.0263 |
| 0.0280 | 0.0271 | 0.0267 | 0.0274 | 0.0266 | 0.0277 | 0.0252 | 0.0268 | 0.0267 | 0.0257 |
| 0.0264 | 0.0273 | 0.0244 | 0.0263 | 0.0264 | 0.0258 | 0.0268 | 0.0260 | 0.0276 | 0.0256 |
| | | | | | | | | | |

where $\widehat{C}_{PU}^{T_*}(i)$ is the *i*th bootstrap estimate. The quantity $S_{C_{PU}}^{*}$ is actually an estimator of the standard deviation of \widehat{C}_{PU}^{T} , and if \widehat{C}_{PU}^{T} is approximately normal distribution, the $(1 - 2\alpha)$ 100% SB confidence interval can be obtained as

 $[\widehat{C}_{PU}^{T} - Z_{\alpha}S_{C_{PU}}^{*}], \qquad (21)$

where Z_{α} is the upper α quantile of the standard normal distribution.

3.2.2. The percentile bootstrap (PB)

From the ordered collection of $\widehat{C}_{PU}^{T_*}(i)$, select the α percent and the $(1 - \alpha)$ percent points as the end points, and the PB confidence interval is

$$[\widetilde{C}_{PU}^{T*}(\alpha B)]. \tag{22}$$

3.2.3. Biased-corrected percentile bootstrap (BCPB)

The bootstrap distribution may be biased while the percentile confidence interval is possible due to sampling errors. In other words, that bootstrap distributions obtained using only a sample of the complete bootstrap distribution may be shifted higher or lower than expected. Thus, a three steps procedure has been developed to correct for this potential bias Efron (1982). First, using the ordered distribution of \widehat{C}_{Pl}^{T*} , calculate the probability of

$$P_0 = P[\hat{C}_{PU}^{T*} \leqslant \hat{c}_{PU}^T]. \tag{23}$$

Second, calculate

$$Z_0 = \Phi^{-1}(P_0), \tag{24}$$

$$P_L = \Phi(2Z_0 - Z_\alpha),\tag{25}$$

$$P_U = \Phi(2Z_0 + Z_\alpha), \tag{26}$$

where $\Phi(\cdot)$ is the standard normal cumulative distribution function. Finally, the BCPB confidence is obtained as

$$[C_{PU}^{T*}(P_LB)]. \tag{27}$$

3.2.4. Bootstrap-t (BT)

<u>~-</u>

While the distribution of the statistic is skewed, the percentile bootstrap confidence interval is probably lower. Thus, the

Table 10

The average rank of the four bootstrap methods as $C_{PU} = 1,1.33$ and v = 2

| n | | $C_{PU}^{I}=1$ | | | | | $C_{PU}^{I}=1.33$ | | | | |
|-----|------|----------------|-------|----------------|-------|-------|-------------------|-------|-------|-------|-------|
| | | N_1 | N_2 | N ₃ | N_4 | R | N_1 | N_2 | N_3 | N_4 | R |
| 30 | SB | 0 | 1 | 498 | 1 | 3 | 1 | 0 | 499 | 0 | 2.996 |
| | PB | 2 | 497 | 0 | 1 | 2 | 2 | 498 | 0 | 0 | 1.996 |
| | BCPB | 498 | 1 | 1 | 0 | 1.006 | 497 | 2 | 1 | 0 | 1.008 |
| | PT | 0 | 1 | 1 | 498 | 3.994 | 0 | 0 | 0 | 500 | 4 |
| 40 | SB | 1 | 0 | 499 | 0 | 2.996 | 2 | 6 | 491 | 1 | 2.982 |
| | PB | 0 | 499 | 0 | 1 | 2.004 | 3 | 491 | 5 | 1 | 2.008 |
| | BCPB | 499 | 0 | 1 | 0 | 1.004 | 493 | 1 | 2 | 4 | 1.034 |
| | PT | 0 | 1 | 0 | 499 | 3.996 | 3 | 1 | 2 | 494 | 3.974 |
| 50 | SB | 1 | 3 | 495 | 1 | 2.992 | 2 | 3 | 493 | 2 | 2.99 |
| | PB | 2 | 495 | 3 | 0 | 2.002 | 2 | 493 | 2 | 3 | 2.012 |
| | BCPB | 495 | 1 | 1 | 3 | 1.024 | 492 | 4 | 1 | 3 | 1.03 |
| | PT | 2 | 1 | 1 | 496 | 3.982 | 4 | 0 | 4 | 492 | 3.968 |
| 60 | SB | 1 | 7 | 492 | 0 | 2.982 | 3 | 6 | 487 | 4 | 2.984 |
| | PB | 1 | 492 | 6 | 1 | 2.014 | 4 | 488 | 7 | 1 | 2.01 |
| | BCPB | 492 | 1 | 1 | 6 | 1.042 | 487 | 5 | 1 | 7 | 1.056 |
| | PT | 6 | 0 | 1 | 493 | 3.962 | 6 | 1 | 5 | 488 | 3.95 |
| 70 | SB | 1 | 2 | 496 | 1 | 2.994 | 1 | 8 | 489 | 2 | 2.984 |
| | PB | 0 | 498 | 2 | 0 | 2.004 | 2 | 488 | 8 | 2 | 2.02 |
| | BCPB | 497 | 0 | 0 | 3 | 1.018 | 493 | 2 | 2 | 3 | 1.03 |
| | PT | 2 | 0 | 2 | 496 | 3.984 | 4 | 2 | 1 | 493 | 3.966 |
| 80 | SB | 0 | 7 | 492 | 1 | 2.988 | 4 | 9 | 484 | 3 | 2.972 |
| | PB | 1 | 492 | 7 | 0 | 2.012 | 3 | 482 | 13 | 2 | 2.028 |
| | BCPB | 495 | 1 | 0 | 4 | 1.026 | 485 | 4 | 1 | 10 | 1.072 |
| | PT | 4 | 0 | 1 | 495 | 3.974 | 8 | 5 | 2 | 485 | 3.928 |
| 90 | SB | 1 | 4 | 492 | 3 | 2.994 | 5 | 11 | 478 | 6 | 2.97 |
| | PB | 0 | 494 | 4 | 2 | 2.016 | 4 | 482 | 11 | 3 | 2.026 |
| | BCPB | 495 | 1 | 2 | 2 | 1.022 | 483 | 3 | 3 | 11 | 1.084 |
| | PT | 4 | 1 | 2 | 493 | 3.968 | 8 | 4 | 8 | 480 | 3.92 |
| 100 | SB | 1 | 10 | 487 | 2 | 2.98 | 3 | 6 | 483 | 8 | 2.992 |
| | PB | 2 | 488 | 8 | 2 | 2.02 | 8 | 484 | 7 | 1 | 2.002 |
| | BCPB | 494 | 2 | 1 | 3 | 1.026 | 484 | 5 | 2 | 9 | 1.072 |
| | PT | 3 | 0 | 4 | 493 | 3.974 | 5 | 5 | 8 | 482 | 3.934 |
| 125 | SB | 1 | 2 | 493 | 4 | 3 | 5 | 14 | 473 | 8 | 2.968 |
| | PB | 1 | 494 | 4 | 1 | 2.01 | 3 | 478 | 15 | 4 | 2.04 |
| | BCPB | 495 | 3 | 0 | 2 | 1.018 | 480 | 2 | 4 | 14 | 1.104 |
| | PT | 3 | 1 | 3 | 493 | 3.972 | 12 | 6 | 8 | 474 | 3.888 |
| 150 | SB | 1 | 8 | 487 | 4 | 2.988 | 4 | 22 | 457 | 17 | 2.974 |
| | PB | 2 | 490 | 8 | 0 | 2.012 | 6 | 465 | 24 | 5 | 2.056 |
| | BCPB | 492 | 1 | 2 | 5 | 1.04 | 480 | 5 | 3 | 12 | 1.094 |
| | PT | 5 | 1 | 3 | 491 | 3.96 | 10 | 8 | 16 | 466 | 3.876 |
| 200 | SB | 0 | 8 | 482 | 10 | 3.004 | 7 | 15 | 463 | 15 | 2.972 |
| | PB | 3 | 487 | 8 | 2 | 2.018 | 12 | 469 | 17 | 2 | 2.018 |
| | BCPB | 492 | 3 | 0 | 5 | 1.036 | 466 | 11 | 6 | 17 | 1.148 |
| | PT | 5 | 2 | 10 | 483 | 3.942 | 16 | 5 | 13 | 466 | 3.858 |

bootstrap-*t* is developed and that the generated distribution will mimic the distribution of *T*. First, approximate the distribution of a statistic of $T = (\widehat{C}_{PU}^T - C_{PU}^T)/S_{C_{PU}^T}$ by using bootstrap. By taking bootstrap samples from the original data values the bootstrap approximation in this case can be obtained, calculate the corresponding estimates $\widehat{C}_{PU}^{**}(i)$ and their standard error, and then find the *T*-values $T = (\widehat{C}_{PU}^{**} - \widehat{C}_{PU}^T)/S_{C_{PU}^T}^{**}$. The $(1 - 2\alpha)$ 100% BT confidence interval can be obtained as

$$[C_{PU}^{I} - t_{\alpha}^{*} S_{C_{PU}}^{*}], \qquad (28)$$

where t_{α}^* and $t_{1-\alpha}^*$ are the upper α and $1 - \alpha$ quantile of the bootstrap *T*-distribution respectively.

4. Performance comparisons of bootstrap methods

We use bootstrap methods to calculate the lower confidence bound of C_{PU}^{T} , used to demonstrate the estimation accuracy $R_{PU} = C_{PU}^{T(LB)} / \tilde{C}_{PU}^{T}$. Then we can determine the required sample sizes for specified estimation accuracy on C_{PU}^{T} . We also rank the four bootstrap methods according to R_{PU} for ascertaining their performance.

Considering the data generated by MATLAB program with multiple independent characteristics from normal distribution, the assumption of normality for each single characteristic is required for the process yield calculation. But the bootstrap approach, which does not require any assumption, is a general nonparametric method. Let the capability C_{PU_j} of each single characteristic satisfy the minimal value (see Table 2) required for overall process capability C_{PU}^T . For example, if a process has a capability requirement $C_{PU}^T \ge 1.00$ with v = 5, i.e., the capability for all the five characteristics is the following $C_{PU_j} \ge 1.153$ for j = 1, 2, ..., 5. We repeated 500 simulations and then obtained each rank of the four bootstrap methods. The calculation of the total weighted average rank *R* of each bootstrap method is as follows:

$$R = \frac{1}{500} \sum_{i=1}^{4} N_i \times i, \tag{29}$$

Table 11 The average rank of four bootstrap methods as $C_{PU} = 1,1.33$ and v = 3

| n | | $C_{PU}^T = 1$ | | | | $C_{PU}^{T} = 1.33$ | | | | | |
|-----|------|----------------|----------------|----------------|-------|---------------------|-------|-------|----------------|-------|-------|
| | | N_1 | N ₂ | N ₃ | N_4 | R | N_1 | N_2 | N ₃ | N_4 | R |
| 30 | SB | 5 | 11 | 480 | 4 | 2.966 | 5 | 19 | 476 | 0 | 2.942 |
| | PB | 3 | 482 | 13 | 2 | 2.028 | 3 | 473 | 21 | 3 | 2.048 |
| | BCPB | 480 | 4 | 2 | 14 | 1.1 | 479 | 3 | 1 | 17 | 1.112 |
| | PT | 12 | 3 | 5 | 480 | 3.906 | 14 | 4 | 2 | 480 | 3.896 |
| 40 | SB | 7 | 12 | 480 | 1 | 2.95 | 4 | 20 | 471 | 5 | 2.954 |
| | PB | 3 | 477 | 17 | 3 | 2.04 | 5 | 470 | 22 | 3 | 2.046 |
| | BCPB | 479 | 4 | 2 | 15 | 1.106 | 473 | 6 | 3 | 18 | 1.132 |
| | PT | 11 | 7 | 1 | 481 | 3.904 | 18 | 4 | 4 | 474 | 3.868 |
| 50 | SB | 2 | 15 | 479 | 4 | 2.97 | 2 | 25 | 471 | 2 | 2.946 |
| | PB | 3 | 478 | 18 | 1 | 2.034 | 5 | 469 | 25 | 1 | 2.044 |
| | BCPB | 481 | 3 | 1 | 15 | 1.1 | 472 | 4 | 1 | 23 | 1.15 |
| | PT | 14 | 4 | 2 | 480 | 3.896 | 21 | 2 | 3 | 474 | 3.86 |
| 60 | SB | 9 | 16 | 470 | 5 | 2.942 | 8 | 34 | 447 | 11 | 2.922 |
| | PB | 3 | 468 | 20 | 9 | 2.07 | 6 | 451 | 33 | 10 | 2.094 |
| | BCPB | 473 | 6 | 7 | 14 | 1.124 | 456 | 9 | 6 | 29 | 1.216 |
| | PT | 15 | 10 | 3 | 472 | 3.864 | 30 | 6 | 14 | 450 | 3.768 |
| 70 | SB | 5 | 19 | 470 | 6 | 2.954 | 5 | 47 | 433 | 15 | 2.916 |
| | PB | 2 | 473 | 22 | 3 | 2.052 | 7 | 439 | 45 | 9 | 2.112 |
| | BCPB | 475 | 6 | 3 | 16 | 1.12 | 444 | 9 | 5 | 42 | 1.29 |
| | PT | 18 | 2 | 5 | 475 | 3.874 | 45 | 5 | 16 | 434 | 3.678 |
| 80 | SB | 8 | 24 | 456 | 12 | 2.944 | 12 | 42 | 428 | 18 | 2.904 |
| | PB | 7 | 462 | 24 | 7 | 2.062 | 9 | 438 | 43 | 10 | 2.108 |
| | BCPB | 463 | 8 | 9 | 20 | 1.172 | 436 | 8 | 10 | 46 | 1.332 |
| | PT | 23 | 5 | 12 | 460 | 3.818 | 43 | 12 | 19 | 426 | 3.656 |
| 90 | SB | 8 | 24 | 458 | 10 | 2.94 | 15 | 69 | 399 | 17 | 2.836 |
| | PB | 3 | 465 | 22 | 10 | 2.078 | 12 | 407 | 66 | 15 | 2.168 |
| | BCPB | 466 | 6 | 7 | 21 | 1.166 | 415 | 9 | 23 | 53 | 1.428 |
| | PT | 23 | 5 | 13 | 459 | 3.816 | 58 | 15 | 12 | 415 | 3.568 |
| 100 | SB | 9 | 23 | 460 | 8 | 2.934 | 15 | 49 | 410 | 26 | 2.894 |
| | PB | 4 | 463 | 26 | 7 | 2.072 | 12 | 423 | 50 | 15 | 2.136 |
| | BCPB | 465 | 7 | 10 | 18 | 1.162 | 428 | 13 | 14 | 45 | 1.352 |
| | PT | 22 | 7 | 6 | 465 | 3.828 | 46 | 16 | 25 | 413 | 3.61 |
| 125 | SB | 6 | 18 | 464 | 12 | 2.964 | 19 | 79 | 369 | 33 | 2.832 |
| | PB | 5 | 467 | 21 | 7 | 2.06 | 18 | 386 | 88 | 8 | 2.172 |
| | BCPB | 471 | 11 | 3 | 15 | 1.124 | 386 | 19 | 9 | 86 | 1.59 |
| | PT | 18 | 4 | 12 | 466 | 3.852 | 77 | 16 | 34 | 373 | 3.406 |
| 150 | SB | 3 | 22 | 462 | 13 | 2.97 | 25 | 85 | 353 | 37 | 2.804 |
| | PB | 9 | 467 | 17 | 7 | 2.044 | 25 | 377 | 83 | 15 | 2.176 |
| | BCPB | 470 | 7 | 8 | 15 | 1.136 | 378 | 18 | 20 | 84 | 1.62 |
| | PT | 19 | 3 | 13 | 465 | 3.848 | 72 | 20 | 45 | 363 | 3.398 |
| 200 | SB | 15 | 42 | 412 | 31 | 2.918 | 26 | 97 | 336 | 41 | 2.784 |
| | PB | 8 | 436 | 47 | 9 | 2.114 | 30 | 350 | 95 | 25 | 2.23 |
| | BCPB | 456 | 10 | 12 | 22 | 1.2 | 364 | 34 | 22 | 80 | 1.636 |
| | PT | 21 | 12 | 29 | 438 | 3.768 | 82 | 18 | 46 | 354 | 3.344 |

where N_i is the total number of rank i (i = 1, 2, ..., 5) during the simulations. For example, if a process has a capability requirement $C_{PU}^T \ge 1.00$ with v = 2 and sample size n = 30, we can obtained the weighted average rank R of the SB method to be

$$R = (0 \times 1 + 1 \times 2 + 498 \times 3 + 1 \times 4)/500 = 3.$$
(30)

In Table 3, the weighted average rank *R* of four bootstrap method is illustrated with various sample size n = 30(10)100, 125, 150, 200, and v = 2(1)5 as $C_{PU}^T = 1$ and 1.33. For example, if the sample size *n* is 60, v = 2 and the C_{PU}^T is 1.33, the weighted average rank *R* of the four bootstrap methods are 2.984, 2.010, 1.056, 3.950, respectively (see Table 3).

From Table 3, the BCPB (biased-corrected percentile bootstrap) method performs better than other ones when $C_{PU}^{T} = 1$. For the fixed values of C_{PU}^{T} and *n*, the weighted average rank of each method gets closer to each other as *v* increases. This fact indicates that the performances of four methods are not much different when *v* is large.

It is shown in Figs. 1a–1d, 2a–2d that the BCPB method is distinctly better when sample size n < 125. However, as the sample size is greater than 125, the performances of four methods are not much different. Furthermore, as $C_{PU}^T = 1.33$ and the quality characteristic v = 5, the weighted average rank *R* of BCPB method is larger than others. This indicates that BCPB method performs worse than the other ones when n > 125, v = 5 and $C_{PU}^T = 1.33$ (see Fig. 2d). Actually, the estimation of the four methods is similar in this situation. As a result of this fact, we recommend the BCPB method is the best one to calculate \widehat{C}_{PU}^T when the sample size n < 125. In the following section, we use BCPB method to evaluate the estimator \widehat{C}_{PU}^T .

5. Sample size required for designated estimation accuracy

The sample size determination is important, as it directly relates to the cost of data collection plan. We develop a MATLAB program to compute the required sample size *n*. The BCPB method is the recommended one to calculate the estimator \hat{C}_{PU}^{T} . In Section 5, we use the simulation data which is randomly generated from normal distribution to determine the required sample size *n*.

Table 12

The average rank of four bootstrap methods as C_{PU} = 1,1.33 and v = 4

| n | | $C_{PU}^T = 1$ | | | | $C_{PU}^{T} = 1.33$ | | | | | |
|-----|------|----------------|-------|-----|-------|---------------------|-------|-------|----------------|-------|-------|
| | | N_1 | N_2 | N3 | N_4 | R | N_1 | N_2 | N ₃ | N_4 | R |
| 30 | SB | 2 | 21 | 467 | 10 | 2.97 | 4 | 30 | 458 | 8 | 2.94 |
| | PB | 3 | 470 | 25 | 2 | 2.052 | 2 | 465 | 26 | 7 | 2.076 |
| | BCPB | 478 | 3 | 2 | 17 | 1.116 | 469 | 1 | 6 | 24 | 1.17 |
| | PT | 18 | 5 | 8 | 469 | 3.856 | 25 | 4 | 10 | 461 | 3.814 |
| 40 | SB | 6 | 35 | 456 | 3 | 2.912 | 8 | 49 | 437 | 6 | 2.882 |
| | PB | 3 | 457 | 35 | 5 | 2.084 | 7 | 438 | 48 | 7 | 2.11 |
| | BCPB | 461 | 4 | 5 | 30 | 1.208 | 442 | 7 | 10 | 41 | 1.3 |
| | PT | 30 | 4 | 4 | 462 | 3.796 | 43 | 6 | 5 | 446 | 3.708 |
| 50 | SB | 7 | 31 | 456 | 6 | 2.922 | 18 | 73 | 387 | 22 | 2.826 |
| | PB | 1 | 458 | 34 | 7 | 2.094 | 13 | 395 | 78 | 14 | 2.186 |
| | BCPB | 458 | 4 | 6 | 32 | 1.224 | 400 | 16 | 14 | 70 | 1.508 |
| | PT | 34 | 7 | 4 | 455 | 3.76 | 69 | 16 | 22 | 393 | 3.478 |
| 60 | SB | 11 | 30 | 452 | 7 | 2.91 | 17 | 80 | 390 | 13 | 2.798 |
| | PB | 6 | 450 | 34 | 10 | 2.096 | 15 | 391 | 79 | 15 | 2.188 |
| | BCPB | 457 | 6 | 6 | 31 | 1.222 | 399 | 13 | 12 | 76 | 1.53 |
| | PT | 26 | 14 | 8 | 452 | 3.772 | 70 | 16 | 19 | 395 | 3.478 |
| 70 | SB | 16 | 38 | 435 | 11 | 2.882 | 16 | 91 | 359 | 34 | 2.822 |
| | PB | 4 | 444 | 37 | 15 | 2.126 | 21 | 371 | 102 | 6 | 2.186 |
| | BCPB | 447 | 9 | 14 | 30 | 1.254 | 372 | 20 | 12 | 96 | 1.664 |
| | PT | 33 | 10 | 13 | 444 | 3.736 | 91 | 18 | 27 | 364 | 3.328 |
| 80 | SB | 8 | 39 | 440 | 13 | 2.916 | 12 | 112 | 345 | 31 | 2.79 |
| | PB | 8 | 438 | 46 | 8 | 2.108 | 18 | 351 | 107 | 24 | 2.274 |
| | BCPB | 450 | 7 | 6 | 37 | 1.26 | 370 | 19 | 19 | 92 | 1.666 |
| | PT | 34 | 16 | 8 | 442 | 3.716 | 101 | 17 | 29 | 353 | 3.268 |
| 90 | SB | 12 | 45 | 428 | 15 | 2.892 | 23 | 114 | 332 | 31 | 2.742 |
| | PB | 12 | 428 | 48 | 12 | 2.12 | 26 | 330 | 126 | 18 | 2.272 |
| | BCPB | 435 | 12 | 12 | 41 | 1.318 | 343 | 32 | 15 | 110 | 1.784 |
| | PT | 41 | 15 | 13 | 431 | 3.668 | 110 | 23 | 26 | 341 | 3.196 |
| 100 | SB | 14 | 46 | 423 | 17 | 2.886 | 25 | 122 | 316 | 37 | 2.73 |
| | PB | 11 | 427 | 51 | 11 | 2.124 | 27 | 317 | 131 | 25 | 2.308 |
| | BCPB | 440 | 16 | 8 | 36 | 1.28 | 332 | 28 | 23 | 117 | 1.85 |
| | PT | 37 | 9 | 18 | 436 | 3.706 | 116 | 34 | 29 | 321 | 3.11 |
| 125 | SB | 9 | 47 | 418 | 26 | 2.922 | 34 | 152 | 277 | 37 | 2.634 |
| | PB | 18 | 416 | 51 | 15 | 2.126 | 28 | 281 | 154 | 37 | 2.4 |
| | BCPB | 434 | 19 | 6 | 41 | 1.308 | 292 | 31 | 35 | 142 | 2.054 |
| | PT | 39 | 18 | 25 | 418 | 3.644 | 146 | 36 | 34 | 284 | 2.912 |
| 150 | SB | 7 | 55 | 409 | 29 | 2.92 | 30 | 155 | 258 | 57 | 2.684 |
| | PB | 29 | 409 | 45 | 17 | 2.1 | 28 | 275 | 160 | 37 | 2.412 |
| | BCPB | 424 | 26 | 12 | 38 | 1.328 | 295 | 33 | 32 | 140 | 2.034 |
| | PT | 42 | 8 | 34 | 416 | 3.648 | 147 | 37 | 51 | 265 | 2.868 |
| 200 | SB | 21 | 55 | 387 | 37 | 2.88 | 35 | 187 | 205 | 73 | 2.632 |
| | PB | 24 | 397 | 58 | 21 | 2.152 | 45 | 232 | 184 | 39 | 2.434 |
| | BCPB | 412 | 24 | 19 | 45 | 1.394 | 240 | 37 | 45 | 178 | 2.322 |
| | PT | 44 | 23 | 37 | 396 | 3.57 | 182 | 42 | 67 | 209 | 2.606 |

Based on the procedure above, a Matlab algorithm for calculating the required sample size is developed as follows:

Algorithm for the required sample size

- Step 1. Input the value of characteristics v, the designated estimation accuracy R_{PU} and the initial sample size values of *Lo* and *Hi*. Compute $R_{PU}(Hi)$ and $R_{PU}(Lo)$ to ensure that $R_{PU}(Hi) > R_{PU}$ and $R_{PU}(Lo) < R_{PU}$.
- Step 2. Let n = (Lo + Hi)/2. Compute $R_{PU}(n)$. If $-Hi Lo \leq 1$, stop and choose $n = \{x | Min | R_{PU}(x) - R_{PU} |, x \in (Hi, Lo)\}$, and then return n (always rounding up if n is not an integer) as the required sample size.
- Step 3. If $R_{PU}(n) > R_{PU}$, $Hi \leftarrow n$; otherwise, $Lo \leftarrow n$. Go back to Step 2.We implement the algorithm and develop a MATLAB program to compute the required sample size. Tables 4, 5 tabulate the required sample size for $R_{PU} = 0.75(0.01)$ 0.95 and $\gamma = 0.9, 0.95, 0.975, 0.99$.

Let the desired estimation accuracy be R_{PU} and the confidence level be γ , and then the minimum sample size n(always rounding up if n is not an integer) can be calculated. Tables 4, 5 display the sample size n required for $R_{\gamma} \ge R_{PU}$ with quality characteristic v = 3, $R_{PU} = 0.75(0.01)0.95$ and $\gamma = 0.9$, 0.95, 0.975, and 0.99 when $C_{PU}^T = 1$ and 1.33. For example, if R_{PU} is set to 0.89, $C_{PU}^T = 1$, and $\gamma = 0.95$, the sample size needed is n = 76. We conclude that a minimum sample size of n = 76 is required to be 95% so that the true C_{PU} is no less than $R_{\gamma} = 89.12\%$ of the sample estimate \hat{C}_{PU} . Thus, if the sample estimate $\hat{C}_{PU}^T = 1.2$, the true value of C_{PU}^T is no less than $1.2 \times 89.12\% = 1.069$, with 95% confidence.

From Tables 4 and 5, we can find that as R_{PU} and γ increase, the required sample size *n* increases. However, some values of sample size can not be obtained (see the sign "–" in the column of the sample size *n*) when the values of R_{PU} and confidence level γ are small. This is due to the problem of the bootstrap resampling procedure.

Table 13 The average rank of four bootstrap methods as $C_{PU} = 1,1.33$ and v = 5

| n | | $C_{PU}^T = 1$ | | | | $C_{PU}^{T} = 1.33$ | | | | | |
|-----|------|----------------|----------------|----------------|-------|---------------------|-------|-------|----------------|-------|-------|
| | | N_1 | N ₂ | N ₃ | N_4 | R | N_1 | N_2 | N ₃ | N_4 | R |
| 30 | SB | 4 | 33 | 453 | 10 | 2.938 | 8 | 64 | 418 | 10 | 2.86 |
| | PB | 4 | 455 | 36 | 5 | 2.084 | 5 | 422 | 66 | 7 | 2.15 |
| | BCPB | 458 | 5 | 5 | 32 | 1.222 | 425 | 10 | 6 | 59 | 1.398 |
| | PT | 34 | 7 | 6 | 453 | 3.756 | 62 | 4 | 11 | 423 | 3.59 |
| 40 | SB | 7 | 50 | 440 | 3 | 2.878 | 19 | 87 | 376 | 18 | 2.786 |
| | PB | 7 | 438 | 44 | 11 | 2.118 | 16 | 372 | 100 | 12 | 2.216 |
| | BCPB | 441 | 5 | 10 | 44 | 1.314 | 376 | 19 | 8 | 97 | 1.652 |
| | PT | 45 | 7 | 7 | 441 | 3.688 | 90 | 21 | 16 | 373 | 3.344 |
| 50 | SB | 11 | 51 | 419 | 19 | 2.892 | 14 | 101 | 360 | 25 | 2.792 |
| | PB | 4 | 429 | 56 | 11 | 2.148 | 13 | 372 | 97 | 18 | 2.24 |
| | BCPB | 436 | 10 | 9 | 45 | 1.326 | 376 | 15 | 18 | 91 | 1.648 |
| | PT | 50 | 10 | 15 | 425 | 3.63 | 97 | 13 | 25 | 365 | 3.316 |
| 60 | SB | 12 | 65 | 409 | 14 | 2.85 | 17 | 117 | 336 | 30 | 2.758 |
| | PB | 4 | 421 | 66 | 9 | 2.16 | 20 | 347 | 119 | 14 | 2.254 |
| | BCPB | 425 | 6 | 9 | 60 | 1.408 | 344 | 20 | 14 | 122 | 1.828 |
| | PT | 59 | 8 | 16 | 417 | 3.582 | 121 | 14 | 31 | 334 | 3.156 |
| 70 | SB | 9 | 75 | 400 | 16 | 2.846 | 14 | 156 | 303 | 27 | 2.686 |
| | PB | 12 | 407 | 71 | 10 | 2.158 | 30 | 297 | 148 | 25 | 2.336 |
| | BCPB | 415 | 9 | 12 | 64 | 1.45 | 302 | 31 | 19 | 148 | 2.026 |
| | PT | 65 | 9 | 16 | 410 | 3.542 | 158 | 12 | 31 | 299 | 2.942 |
| 80 | SB | 12 | 59 | 395 | 34 | 2.902 | 27 | 159 | 274 | 40 | 2.654 |
| | PB | 6 | 414 | 64 | 16 | 2.18 | 17 | 289 | 171 | 23 | 2.4 |
| | BCPB | 427 | 8 | 12 | 53 | 1.382 | 290 | 26 | 23 | 161 | 2.11 |
| | PT | 57 | 18 | 29 | 396 | 3.528 | 168 | 24 | 33 | 275 | 2.83 |
| 90 | SB | 8 | 82 | 374 | 36 | 2.876 | 28 | 195 | 240 | 37 | 2.572 |
| | PB | 25 | 381 | 77 | 17 | 2.172 | 33 | 249 | 187 | 31 | 2.432 |
| | BCPB | 396 | 25 | 12 | 67 | 1.5 | 259 | 28 | 23 | 190 | 2.288 |
| | PT | 71 | 12 | 37 | 380 | 3.452 | 182 | 27 | 49 | 242 | 2.702 |
| 100 | SB | 19 | 83 | 362 | 36 | 2.83 | 24 | 217 | 203 | 56 | 2.582 |
| | PB | 25 | 368 | 93 | 14 | 2.192 | 37 | 219 | 212 | 32 | 2.478 |
| | BCPB | 384 | 25 | 18 | 73 | 1.56 | 235 | 31 | 41 | 193 | 2.384 |
| | PT | 76 | 20 | 29 | 375 | 3.406 | 206 | 31 | 45 | 218 | 2.55 |
| 125 | SB | 11 | 73 | 369 | 47 | 2.904 | 25 | 225 | 195 | 55 | 2.56 |
| | PB | 30 | 378 | 76 | 16 | 2.156 | 42 | 207 | 219 | 32 | 2.482 |
| | BCPB | 388 | 30 | 19 | 63 | 1.514 | 197 | 38 | 33 | 232 | 2.6 |
| | PT | 72 | 18 | 38 | 372 | 3.42 | 236 | 30 | 55 | 179 | 2.354 |
| 150 | SB | 24 | 84 | 332 | 60 | 2.856 | 45 | 233 | 166 | 56 | 2.466 |
| | PB | 22 | 364 | 92 | 22 | 2.228 | 52 | 170 | 242 | 36 | 2.524 |
| | BCPB | 382 | 25 | 18 | 75 | 1.572 | 186 | 43 | 32 | 239 | 2.648 |
| | PT | 72 | 27 | 59 | 342 | 3.342 | 222 | 50 | 61 | 167 | 2.346 |
| 200 | SB | 26 | 88 | 329 | 57 | 2.834 | 40 | 252 | 163 | 45 | 2.426 |
| | PB | 28 | 350 | 94 | 28 | 2.244 | 49 | 146 | 254 | 51 | 2.614 |
| | BCPB | 372 | 37 | 21 | 70 | 1.578 | 137 | 54 | 42 | 267 | 2.878 |
| | PT | 74 | 27 | 54 | 345 | 3.34 | 278 | 44 | 41 | 137 | 2.074 |

6. Application

We consider the following case from a manufacturing factory located on the Science-Based Industrial Park in Taiwan, making the thin film transistor liquid crystal display (TFT-LCD). There are three major process groups in TFT-LCD manufacturing process, array process; cell process and module assemble process. The array process is similar to the semiconductor manufacturing process, except that transistors are fabricated on a glass substrate instead of a silicon wafer. Photolithography (one of the array process) is a critical step within LCD manufacturing process since the panel quality depends on the entire pattern formation. Film deposition is done before photolithography. Overlay is a key parameter in deposition process and uniformality is a key parameter in coating and exposure, which are two processes in photolithography. We focus on these key parameters, such as overlay, critical dimension and uniformality.

In Fig. 3, between one deposited layer and another, a distance called overlay may be existed. There are three steps in photolithog-

raphy process, coating, exposure, and development. It might result deviation as exposure on panel window, called critical dimension (see Fig. 4). In addition, coating photoresist on panel has to be uniform. The specifications of these three key parameters are shown in Table 6. Since the assumption of normality for each single characteristic is required for the process yield calculation, the historical data of each key characteristic indicates the process being pretty approximate to a normal distribution. Thus, we can conclude that each characteristic data collected from the process is in control and normally distributed.

To obtain the sample size required *n* under the desired estimation accuracy $R_{pm}^{(PS)}$, we can find it in Table 4. If the practitioners set $R_{pm}^{(PS)}$ to be 0.92, and $\gamma = 0.95$ the sample size needed is n = 146. We conclude that a minimum sample size of n = 146 is required to be 95% so that the true C_{PU}^{T} is no less than $R_{\gamma} = 92.11\%$ of the sample estimator \widehat{C}_{PU}^{T} . Thus, if the sample estimator $\widehat{C}_{PU}^{T} = 1.3$, the true value of C_{PU}^{T} is no less than $1.3 \times 92.11\% = 1.197$, with 95% confidence. Hence, sample data collected from 150 LCD is displayed in Table 9 of the Appendix. And the upper specification limit, the calculated

sample mean, location departure, sample standard deviation, the estimated C_{PU_j} and the lower confidence bound L_C for each characteristic are summarized in Table 7.

6.1. Overall process yield analysis

The sample estimators of C_{PU}^{T} and the BCPB method lower confidence bound of C_{PU}^{T} for the single characteristic overlay, critical dimension and uniformality coupler can be summarized in Table 8.

Table 8 displays the manufacturing capability and its corresponding NCPPM for the LCD process using the estimated \hat{C}_{PU}^{T} values (uncorrected) and the lower confidence bounds $C_{PU}^{T(LB)}$ (corrected). The $C_{PU}^{T(LB)}$ (the LCB of C_{PU}^{T}) obtained using BCPB method is certainly more reliable than the estimated \hat{C}_{PU}^{T} index values (an approach widely used in current industrial applications), since the sampling errors are considered in the LCB approach. In fact, as the sample estimate \hat{C}_{PU}^{T} may overestimate the true capability (overall process yield), it conveys unreliable and misleading information, which should be avoided in factory applications. Based on the value of $C_{PU}^{T(LB)}$, we thus can assure that the production yield is 99.7308%, and the number of the nonconformities is less than 2692 PPM.

7. Conclusions

In this paper, we considered the problem of finding the lower confidence bound and sample sizes required for specified estimation accuracy for the C_{PU}^{T} . Since the sampling distribution of C_{PU}^{T} is analytically intractable, we applied the bootstrap method to cal-culate the estimator of C_{PU}^{T} and compared the estimation accuracy of the four bootstrap methods. The results indicated that the BCPB method has good performance when the sample size is smaller than 125. The lower confidence bounds present a measure on the minimum capability of the process based on the sample data. We also investigated the lower confidence bound values and sample sizes required for specified estimation accuracy using BCPB method. The proposed approach ensures that the risk of making incorrect decisions is no larger than the preset Type I error $1 - \gamma$. We also provided tables for the engineers/practitioners to use for their in-plant applications. A real-world example from TFT-LCD manufacturing process is investigated to illustrate the applicability of our approach. In the future, we can consider same approach for indices with two-sided specifications, such as C_{pk} , C_{pm} and C_{pmk} . We also consider multiple characteristics with some correlations.

Appendix

See Tables 9–13.

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