Contents

4-5. Conclusions 72

Table captions

Table 3-1: Main properties of parylene.

Figure captions

- Figure 1-1: System-level schematic detail of the front-end design for a typical wireless transceiver.
- Figure 1-2: Micromachined microstrip antenna with a portion of substrate material below the patch removed by backside etching.
- Figure 1-3: Microstrip antenna with micromachined trenches below its radiating edges.
- Figure 1-4: A micromachined horn antenna for W-band application: (a) schematic; (b) photograph of fabricated antenna in test jig.
- Figure 1-5: Micromachined microstrip antenna with the ability of beam steering.
- Figure 1-6: Micromachined Vee antenna for both beam shaping and beam steering.
- Figure 1-7: (a) Schematic of the proposed reconfigurable pixel-patch antenna architecture; RF MEMS actuator; (b) top view; (c) side view (down position); (d) side view (up position).
- Figure 1-8: The open-end effect with different length (2λ0, 4λ0).
- Figure 1-9: (a) Array topology for the suppression of the reflected wave. (b) Taper end and active feed back for the suppression of the reflected wave.
- Figure 1-10: A dual-band monopole antenna fabricated on a parylene membrane.
- Figure 1-11: A compact three-dimensional MEMS antenna.
- Figure 2-1: Schematic illustration of the basic process steps in surface micromachining.
- Figure 2-2: Illustration of possible bulk-micromachined structures.
	- (a) Rounded, isotropically etched pits in a silicon substrate.
- (b) Pyramidal pits etched into (100) and (110) silicon using anisotropic wet etchants, bounded by (111) crystal planes.
- (c) A pyramidal pit etched down to a buried etch-stop layer in (100) silicon, with an undercut cantilever beam.
- Figure 2-3: Typical sequence for the production of a microstructure based on the LIGA technique.
- Figure 2-4: Three dimensional plot of the radiation pattern of the dipole antenna.
- Figure 2-5: Current distribution of a monopole antenna and its equalized dipole antenna.
- Figure 2-6: The radiation pattern of the ideal monopole antenna.
	-
- Figure 2-7: Meander line antenna with a finite ground plane.
- Figure 2-8: The frequency of a meander line antenna vs. *Lax* .
- Figure 2-9: The impendence of a meander line antenna vs. L_{ax} .
- 40001 Figure 2-10: Dispersion curve for the lowest mode and the first higher modes in microstrip line with a top cover. The figure is copied from the A.A Oliner's paper.
- Figure 2-11: Top view and Rrough sketch cross view of open microstrip line operated in the first higher mode.
- Figure 2-12: The variations of β /K0 and α/K0 with frequency for a particular microstrip line with W=433mil and $y=2.2$ and $H = 20$ mil.
- Figure 2-13: Geometry and coordinate system for the microstrip leaky-wave antenna.
- Figure 2-14: Coordinate system and the physical meaning of θ_m , and $\Delta\theta$.
- Figure 3-1: Detailed geometry and dimensions of designed dual-band meander monopole antenna.
- Figure 3-2: Simulation of the dual-band monopole antenna.
- Figure 3-3: Equipment for parylene deposition, PDS 200.
- Figure 3-4: Deposition process of parylene.
- Figure 3-5: Fabrication process of designed antenna on parylene-coated silicon substrate.
- Figure 3-6: Fabricated dual-band meander monopole antenna (a) before and (b) after being stacked on Bluetooth dongle.
- Figure 3-7: Measured and simulated return losses for the dual-band monopole antenna (2.4 and 5.2 GHz for Bluetooth and WLAN). بالللاق
- Figure 3-8: x-z plane radiation pattern measurement setup of MEMS membrane monopole antenna under far-field conditions.
- Figure 3-9: Measured x-z and y-z plane radiation patterns for the proposed antenna at 2.4GHz. $\eta_{\rm thermal}$
- Figure 3-10: Measured x-z and y-z plane radiation patterns for the proposed antenna at 5.2GHz.
- Figure 3-11: Geometry of dual-band monopole antenna with another design. (a) Detail geometry and dimensions (b) On parylene substrate (c) Fabricated on a Bluetooth dongle
- Figure 3-12: Measured and simulated return loss for the dual-band monopole antenna with another design (2.4 and 5.2 GHz for Bluetooth and WLAN).
- Figure 3-13: Measured x-z and y-z plane radiation patterns at 2.4 GHz of the antenna with G-shape design.
- Figure 3-14: Measured x-z and y-z plane radiation patterns at 5.2 GHz of the antenna with G-shape design.
- Figure 3-15: RFID antennas with different dimensions were fabricated on a flexible parylene membrane.
- Figure 4-1: (a) the structure of the 3-D MEMS monopole antenna, (b) Top view of the antenna. (Not to scale)
- Figure 4-2: Simulation of the 3D monopole antenna.
- Figure 4-3: the process flow of the 3-D MEMS helical meander antenna.
- Figure 4-4: The schematic set of the electroplating equipment.
- Figure 4-5: The photo of the equipment for electroplating experiment.
- Figure 4-6: The SEM photograph of the cross section of the copper via.
- Figure 4-7: The photograph of the 3D monopole antenna.
	-
- Figure 4-8: Measured and simulated return losses for the proposed antenna.
- Figure 4-9: The setup for radiation pattern measurement.
- Figure 4-10: Measured radiation patterns for the proposed antenna.
- Figure 4-11: EM fields neutralization between adjacent lines.
- Figure 4-12: The structure of the 3D antenna on silicon base
- Figure 4-13: The process flow of the 3-D MEMS helical meander antenna.
- Figure 4-14: Frequency-tunable 3-D MEMS monopole antenna.
- Figure 5-1: The configuration of the short leaky-wave antenna integrated with the 1-,
	- 2- and 4-element aperture-fed patch antenna arrays.
- Figure 5-2: The geometry and coordinate system for the aperture-coupled patch antenna.
- Figure 5-3: The schematic diagram of the varactor-tuned phase shifter.
- Figure 5-4: The simulated and measured return loss of the short LWA with the open end.
- Figure 5-5: The simulated and measured return loss of the short LWA integrated with an aperture-coupled patch antenna.
- Figure 5-6: The comparison of the measured radiation patterns of the proposed antenna structure comparing to the traditional LWA at 10.5 GHz.
- Figure 5-7: The measured radiation patterns of the short LWA integrated with an aperture- coupled patch antenna at 9.0GHz and 10.5GHz.
- Figure 5-8: The simulated and measured return loss of the short LWA integrated with 2-element aperture-coupled patch antenna arrays.
- Figure 5-9: The comparison between the short LWA integrated with the 2-element aperture-coupled patch arrays and the traditional LWA.
- Figure 5-10: The comparison between the short LWA integrated with the 2-element aperture-coupled patch arrays and the traditional LWA.
- Figure 5-11: The simulated and measured radiation pattern of the 2-element aperturecoupled patch antenna arrays.
- Figure 5-12: The comparison between the short LWA integrated with the 4-element aperture-coupled patch arrays and the traditional LWA.
- Figure 5-13: The measured radiation pattern of the short LWA integrated with 2-element aperture-coupled patch arrays at the bias of –15V.
- Figure 6-1: Layout of torsion RF MEMS switch and CPW circuit
- Figure 6-2: The schematic of CPW nonlinear delay line
- Figure 6-3: Tunable RF nonlinear delay line
- Figure 6-4: Brief describe of EPIES process.
- Figure 6-5: The cross-section SEM photography of Cu structure after the XeF2 isotropic Si etching.
- Figure 6-6: The SEM photography of Cu (a) relay/switch and (b) tunable capacitor after the XeF2 isotropic Si etching.