

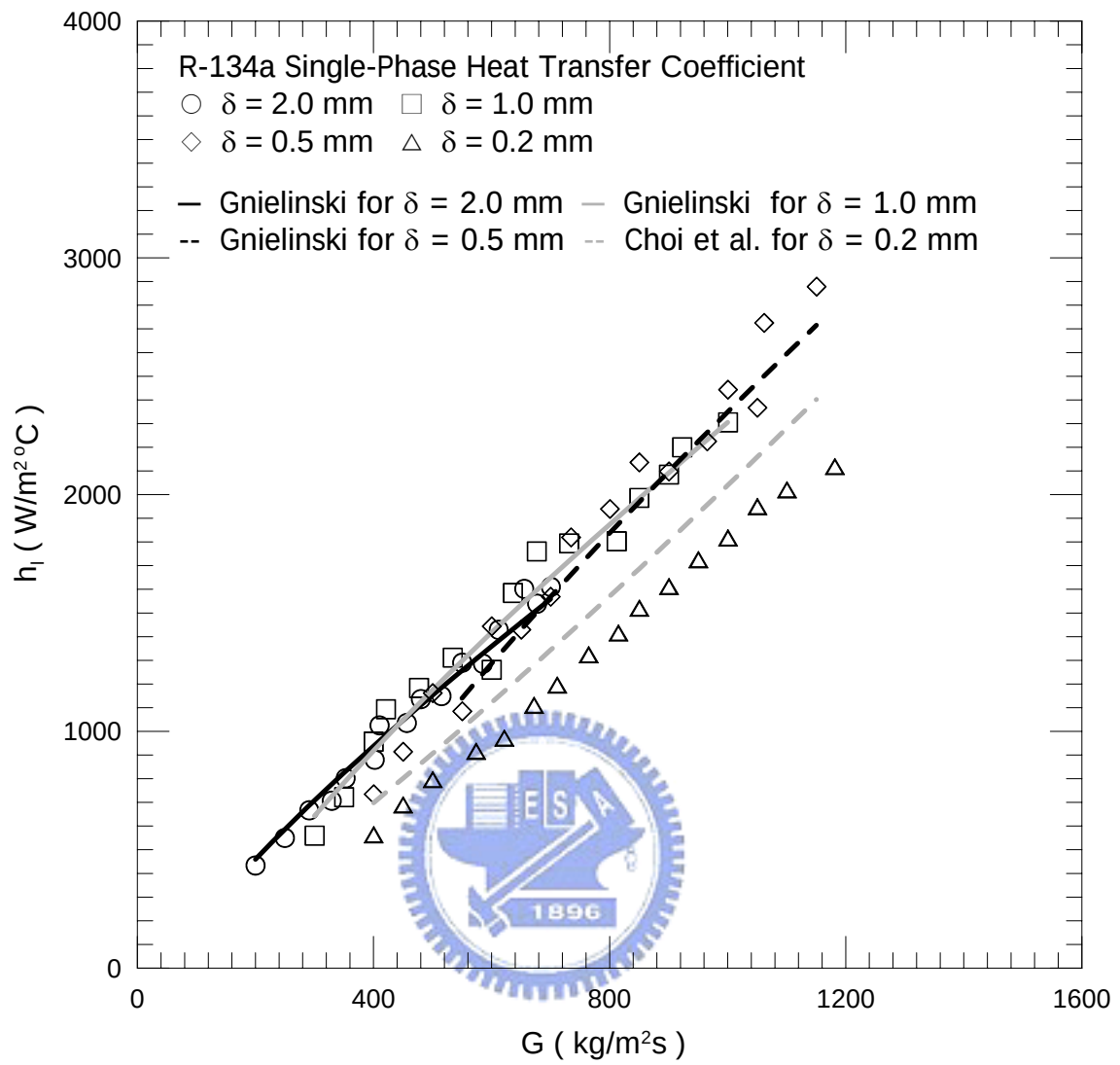


Fig. 4.1 Comparison of the present single-phase liquid convection heat transfer data with the correlation of Gnielinski [70] and Choi et al. [71].

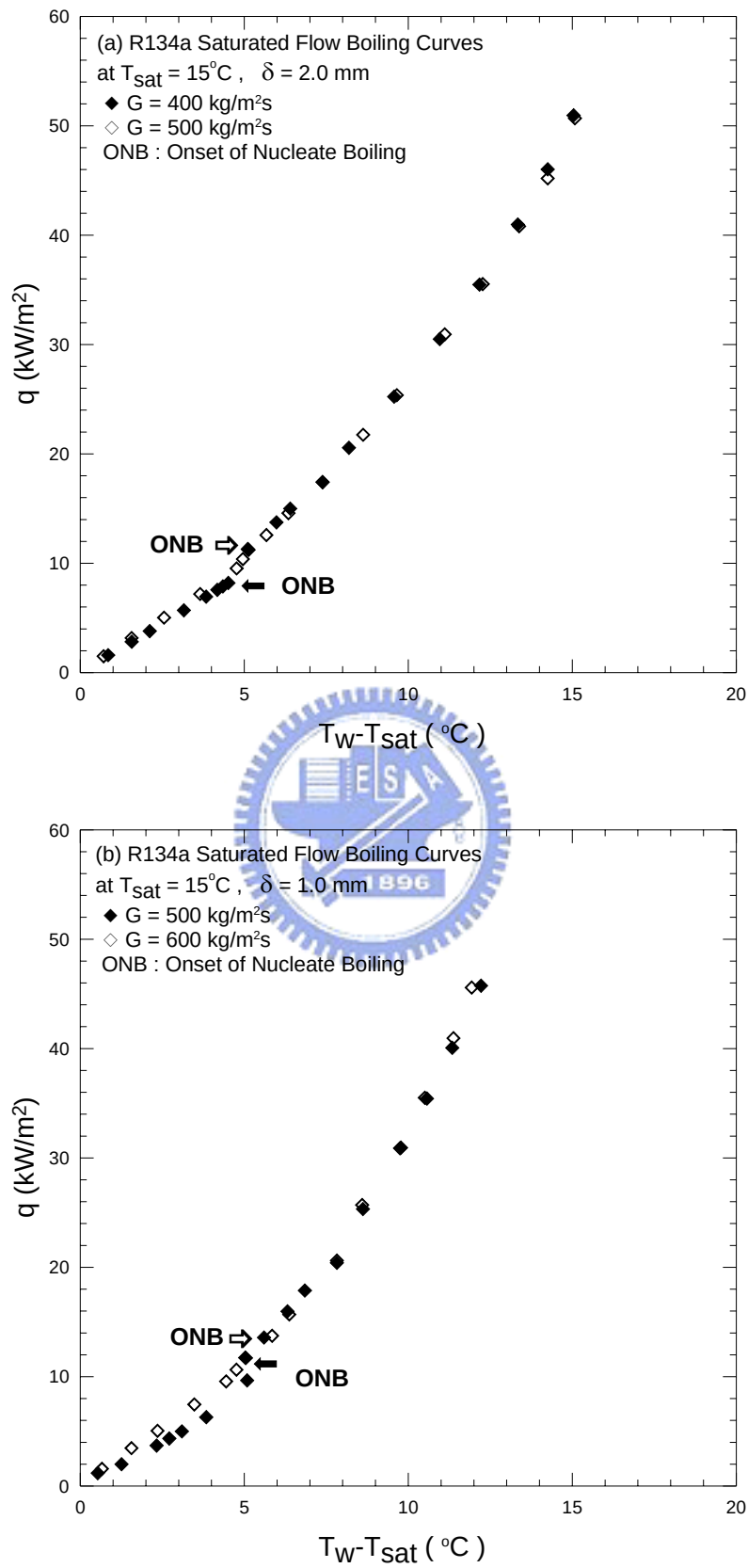


Fig. 4.2 Saturated flow boiling curves for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 2.0 \text{ mm}$ and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 1.0 \text{ mm}$.

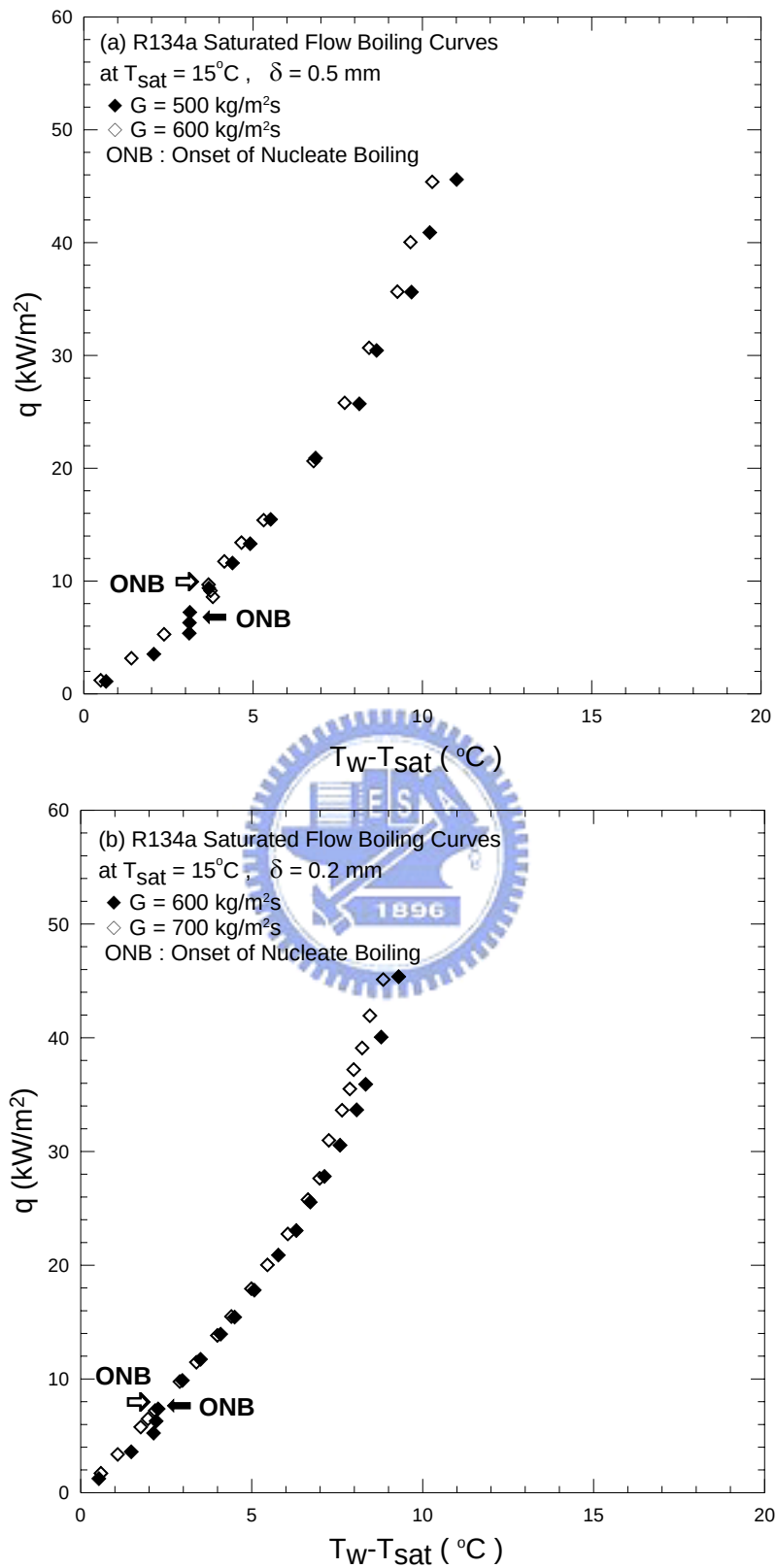


Fig. 4.3 Saturated flow boiling curves for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 0.5 \text{ mm}$ and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 0.2 \text{ mm}$.

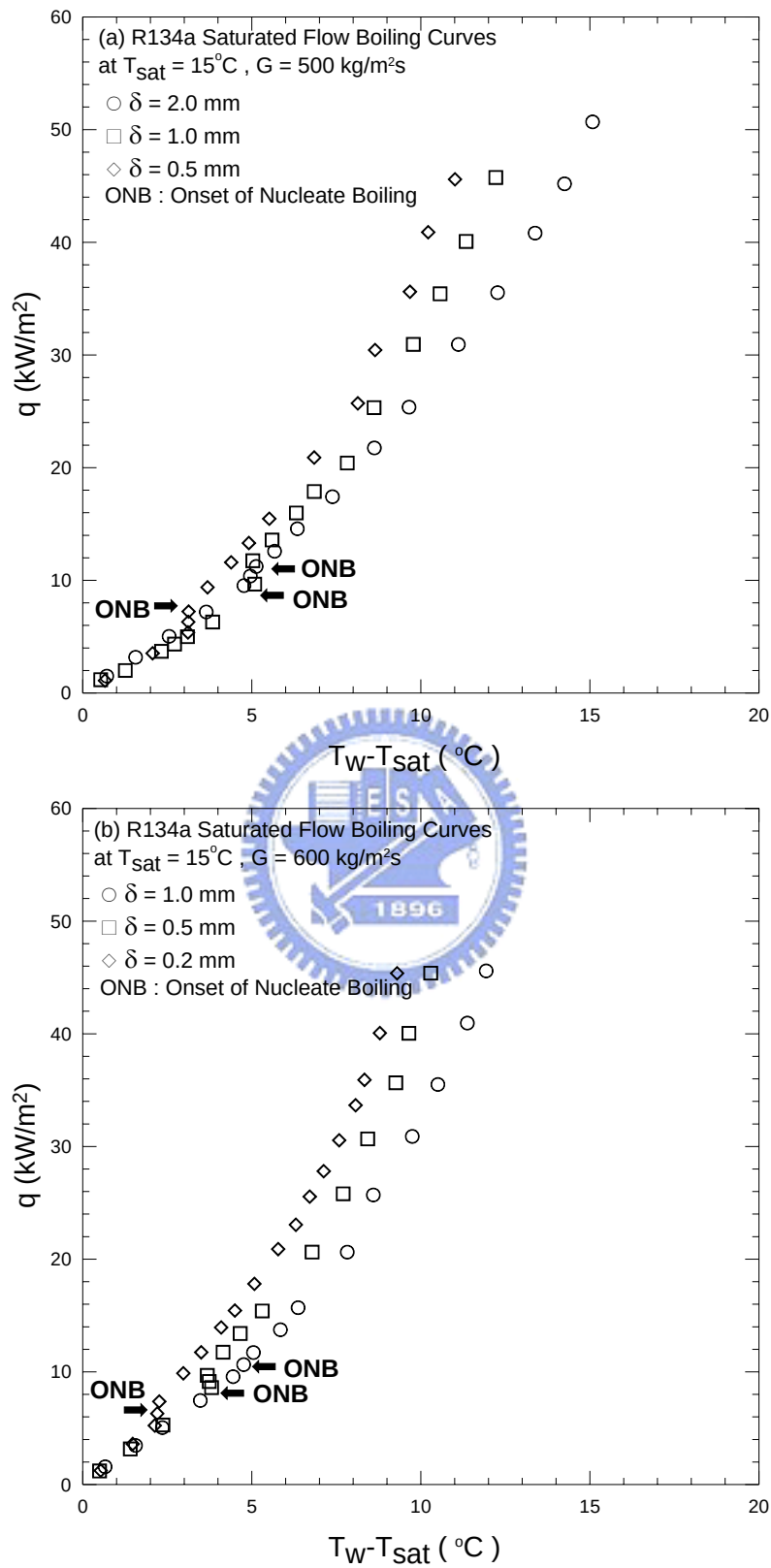


Fig. 4.4 Saturated flow boiling curves for various gap sizes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $G = 500 \text{ kg/m}^2\text{s}$ and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $G = 600 \text{ kg/m}^2\text{s}$.

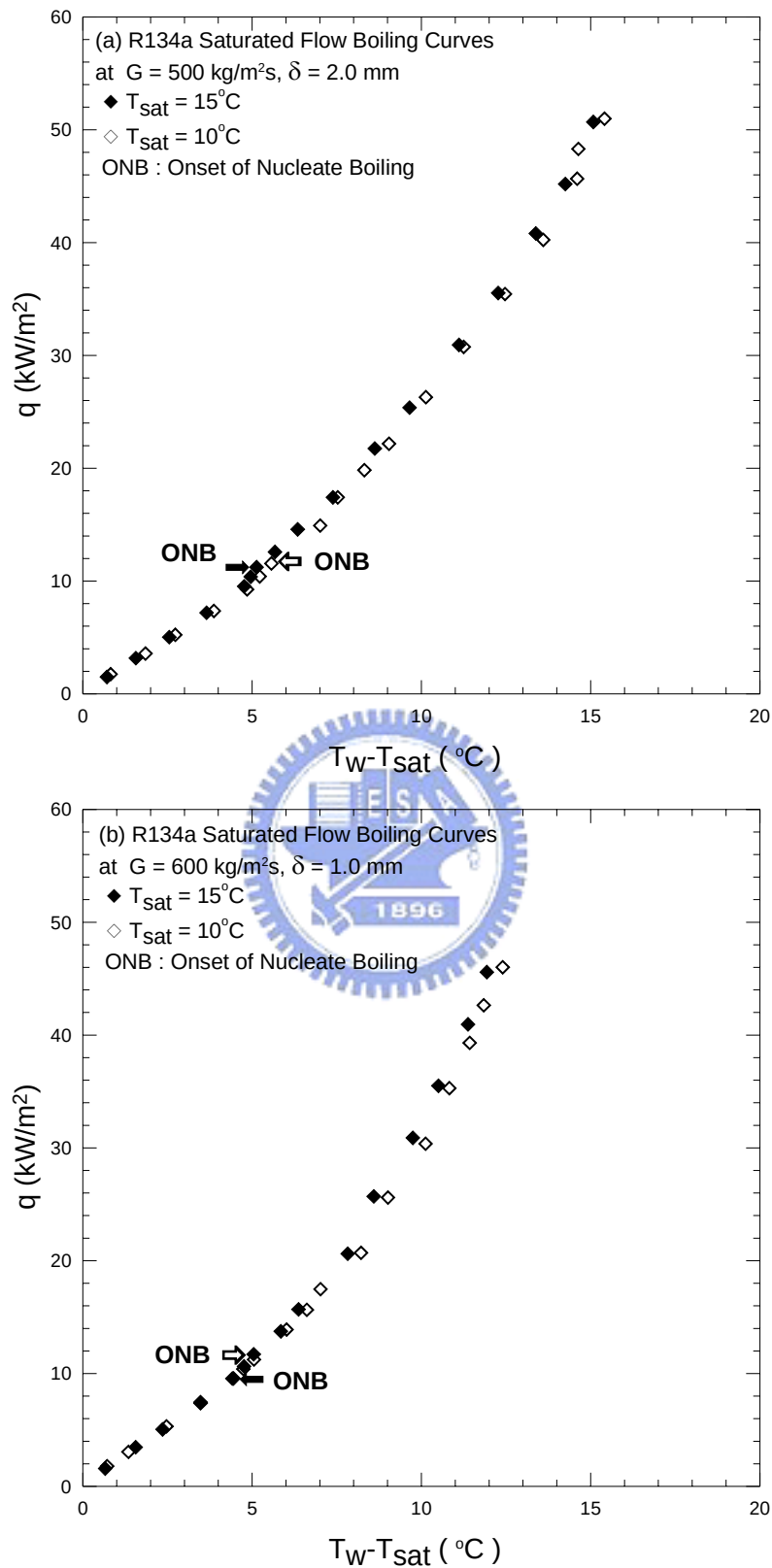


Fig. 4.5 Saturated flow boiling curves for various refrigerant saturated temperatures at
 (a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 2.0 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 1.0 \text{ mm}$.

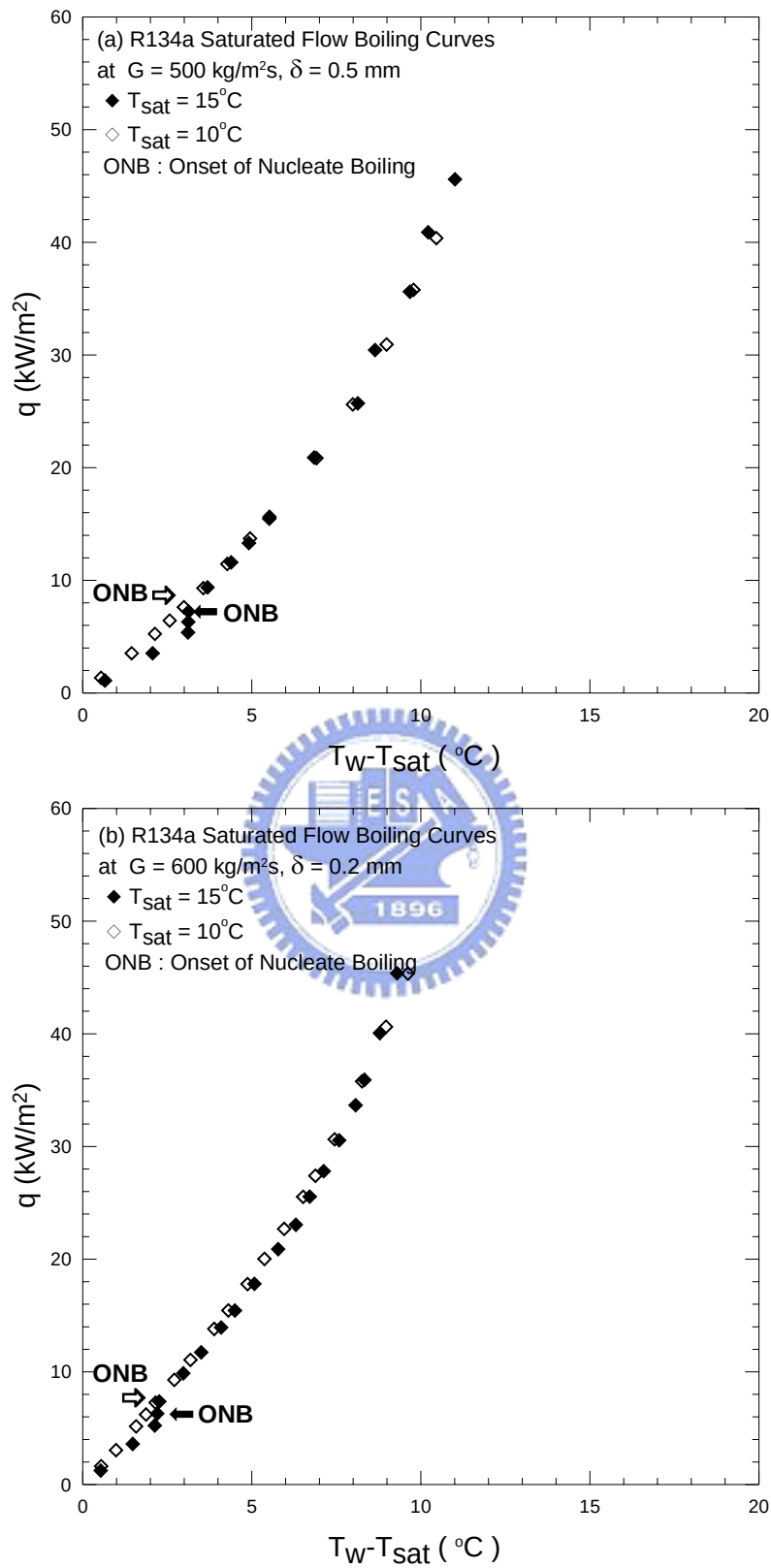


Fig. 4.6 Saturated flow boiling curves for various refrigerant saturated temperatures at
(a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 0.5 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 0.2 \text{ mm}$.

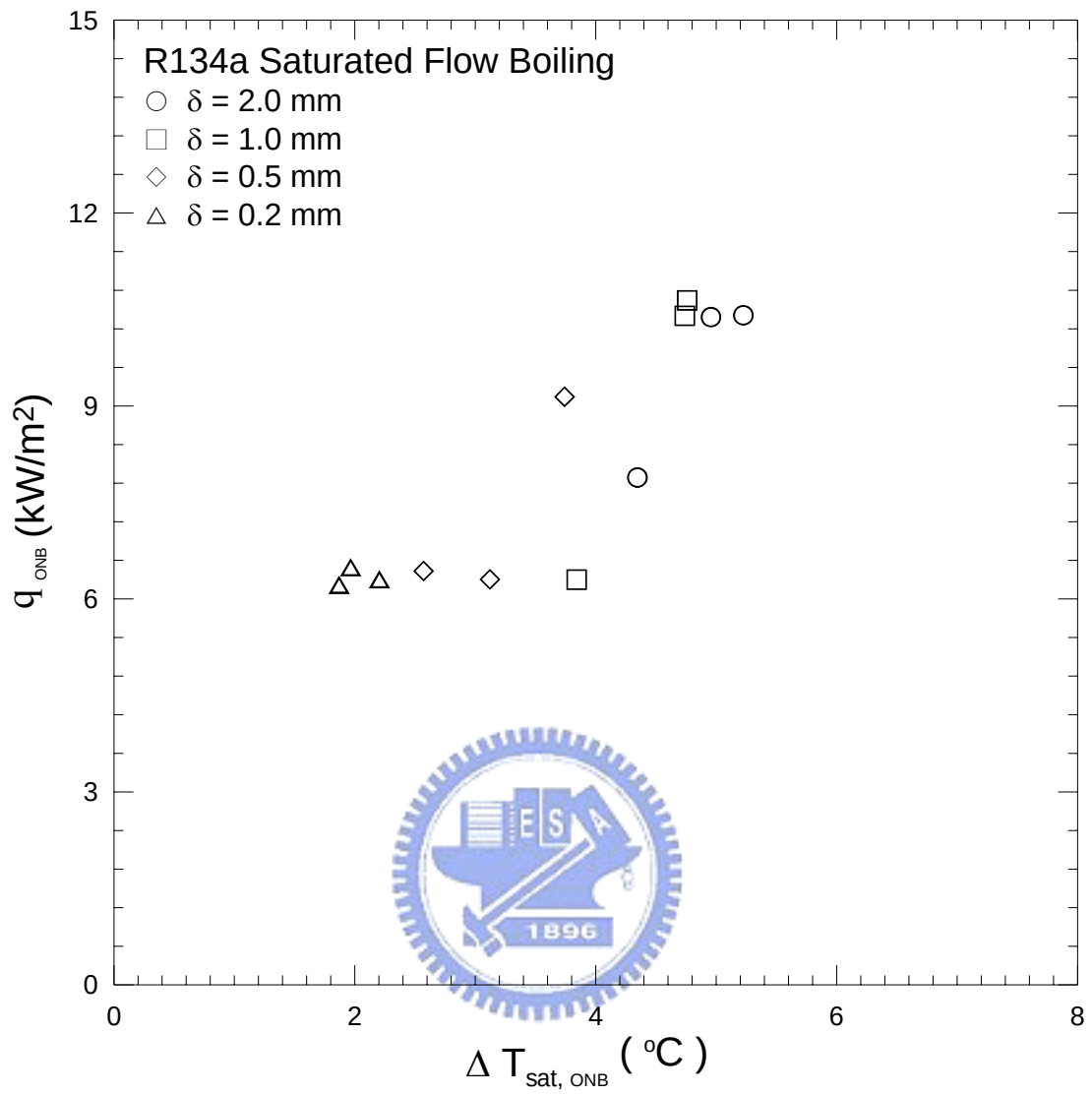


Fig. 4.7 Relation between imposed heat flux and wall superheat at the incipient boiling.

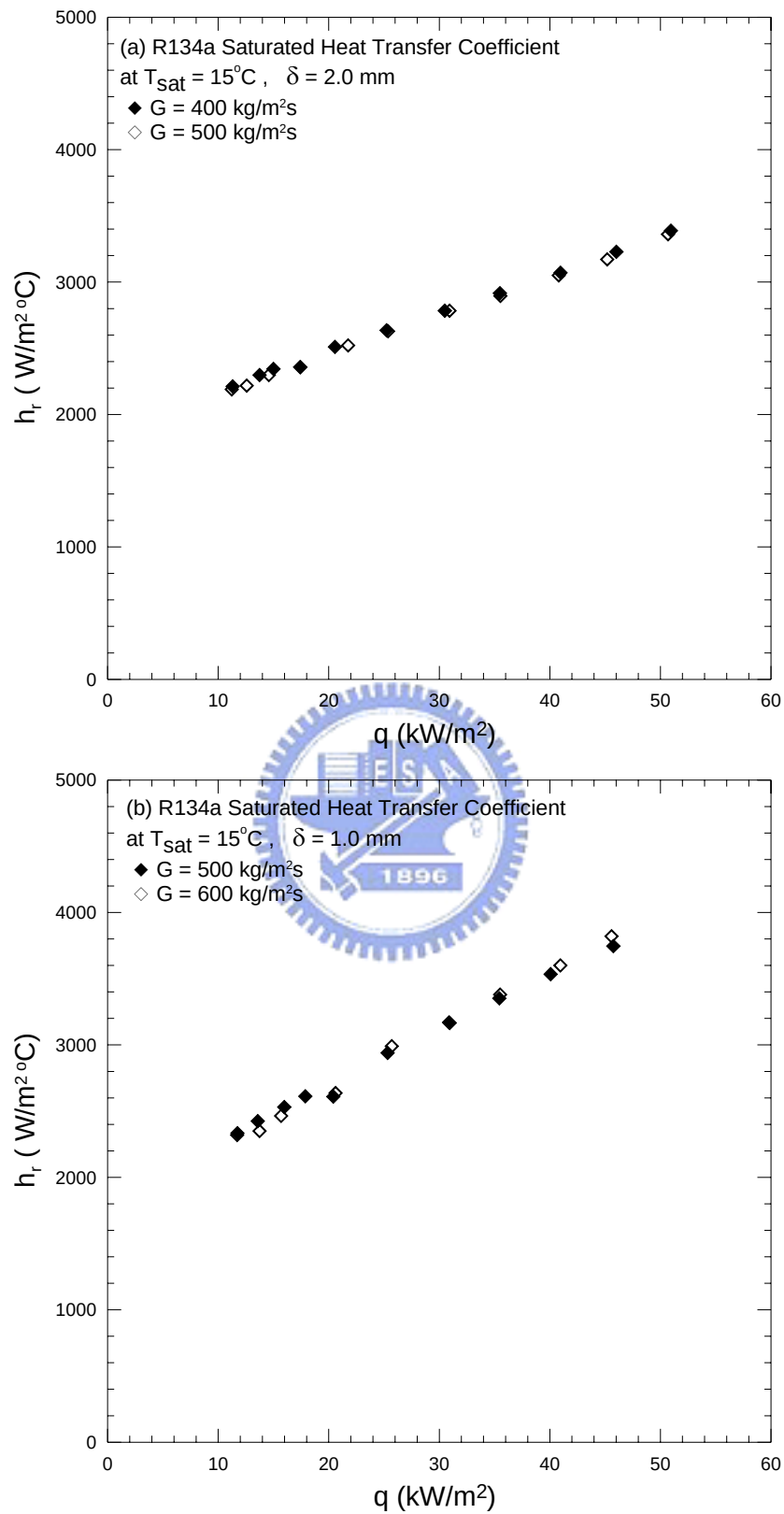


Fig. 4.8 Saturated flow boiling heat transfer coefficient for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 2.0 \text{ mm}$ and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 1.0 \text{ mm}$.

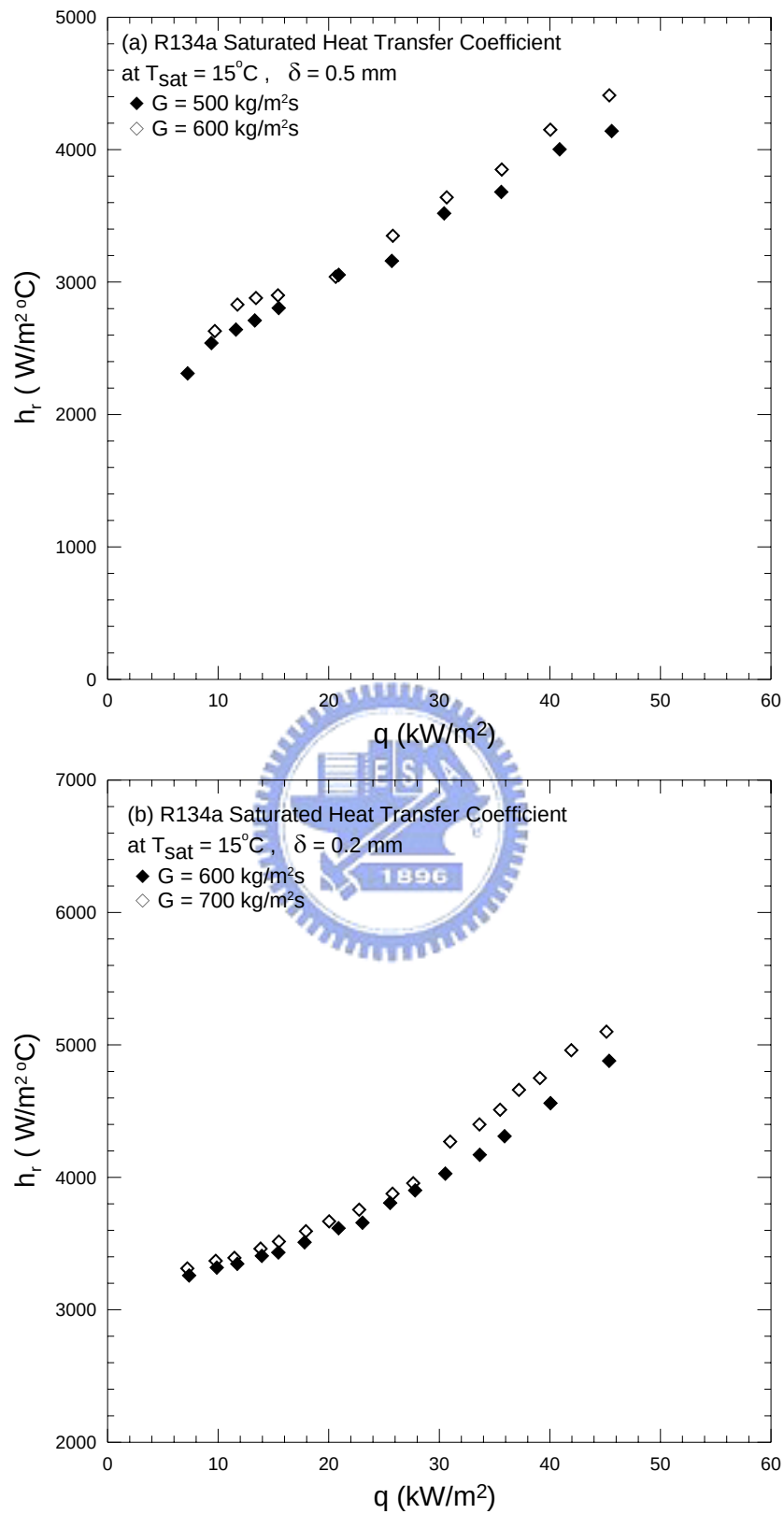


Fig. 4.9 Saturated flow boiling heat transfer coefficient for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^{\circ}\text{C}$ & $\delta = 0.5 \text{ mm}$ and (b) $T_{\text{sat}} = 15^{\circ}\text{C}$ & $\delta = 0.2 \text{ mm}$.

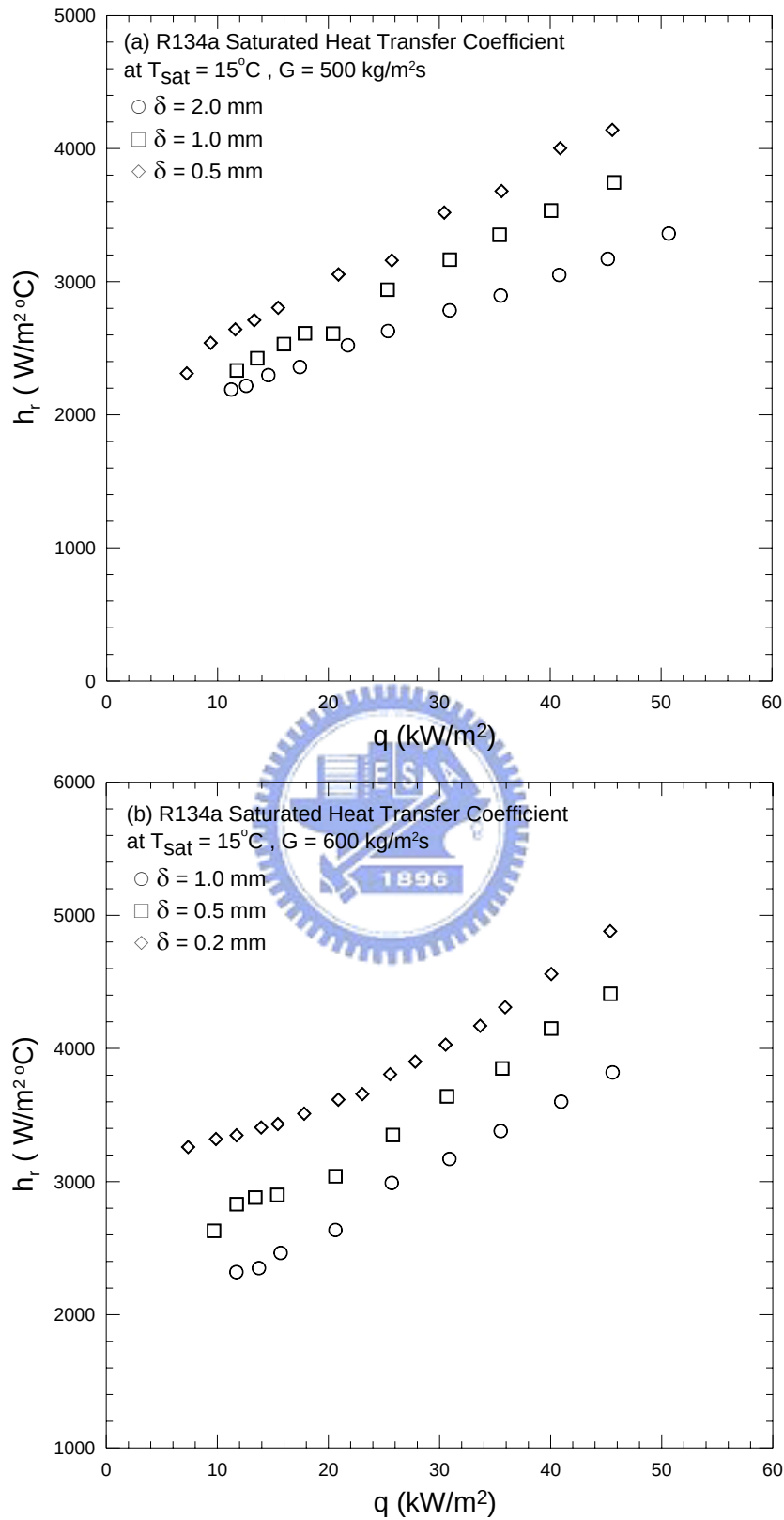


Fig. 4.10 Saturated flow boiling heat transfer coefficient for various gap sizes at (a) $T_{\text{sat}} = 15^{\circ}\text{C}$ & $G = 500 \text{ kg/m}^2\text{s}$ and (b) $T_{\text{sat}} = 15^{\circ}\text{C}$ & $G = 600 \text{ kg/m}^2\text{s}$.

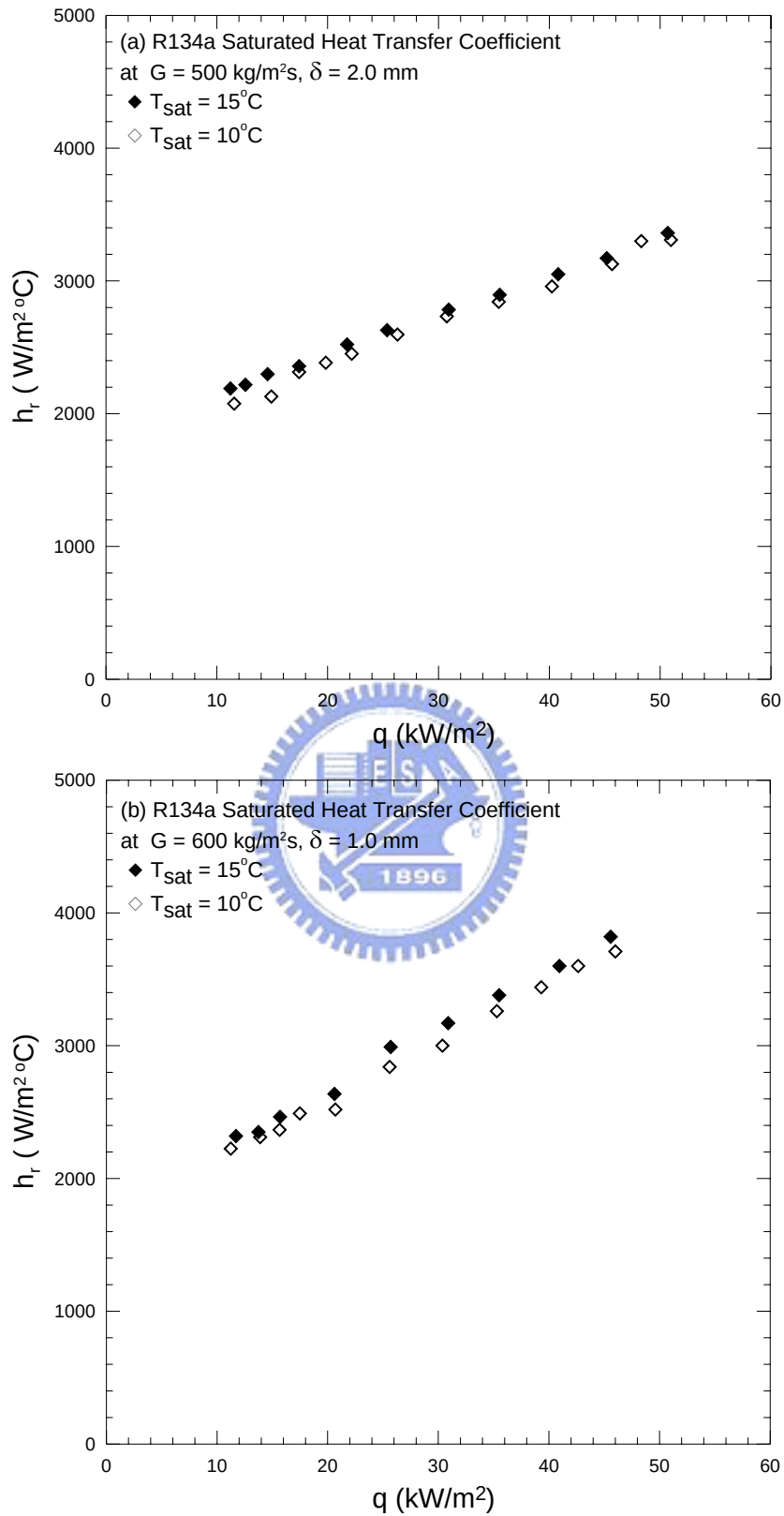


Fig. 4.11 Saturated flow boiling heat transfer coefficient for various refrigerant saturated temperatures at (a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 2.0 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 1.0 \text{ mm}$.

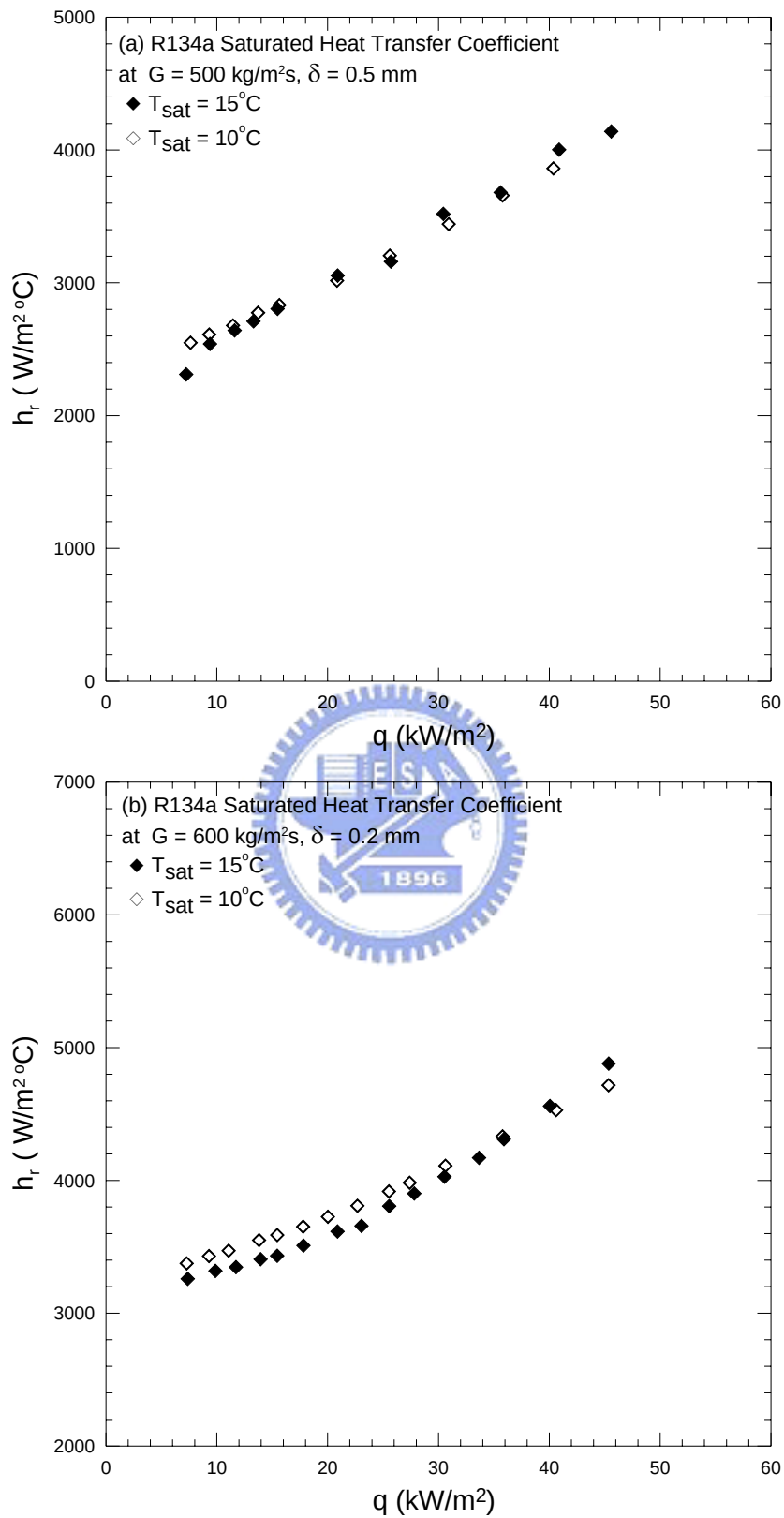
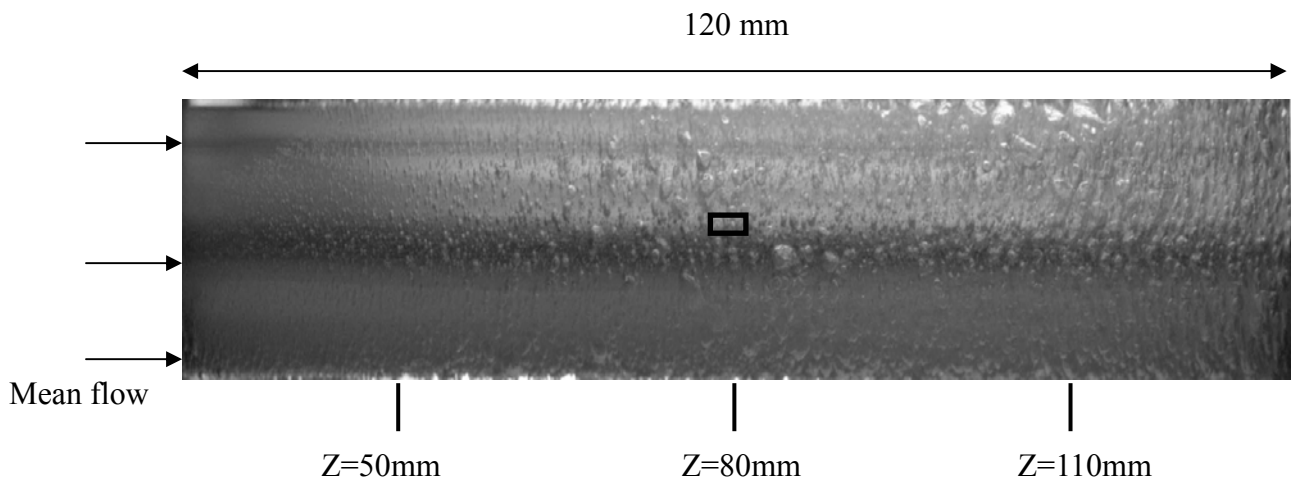
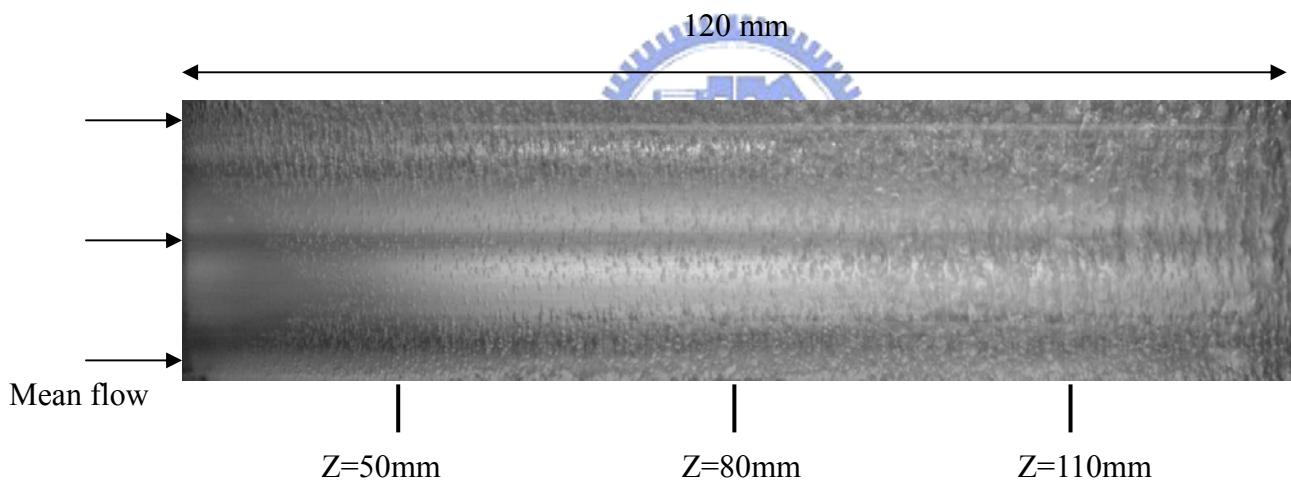


Fig. 4.12 Saturated flow boiling heat transfer coefficient for various refrigerant saturated temperatures at (a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 0.5 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 0.2 \text{ mm}$.

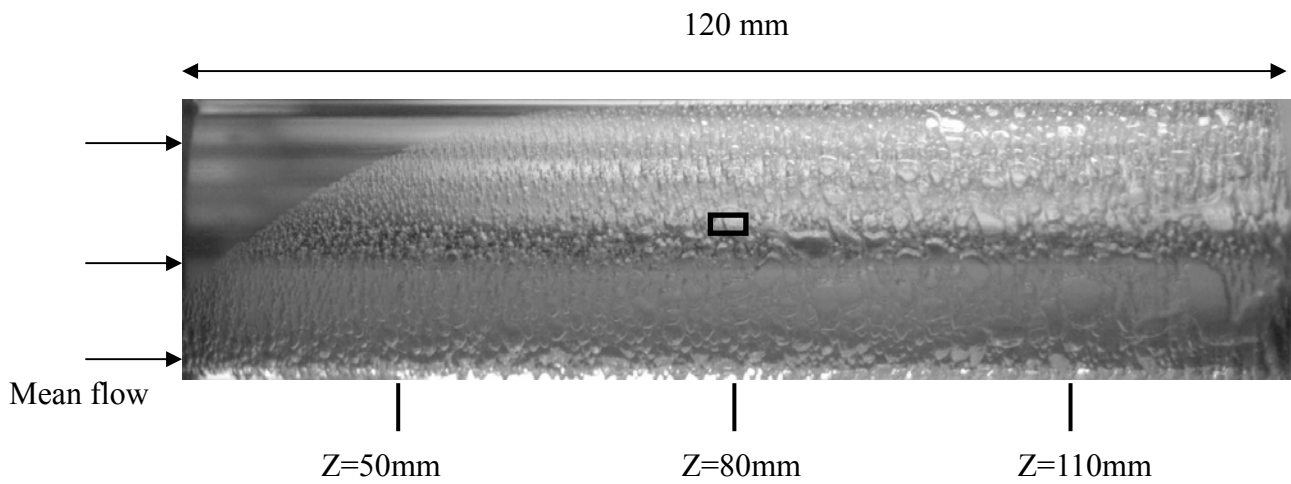


(a) Side view

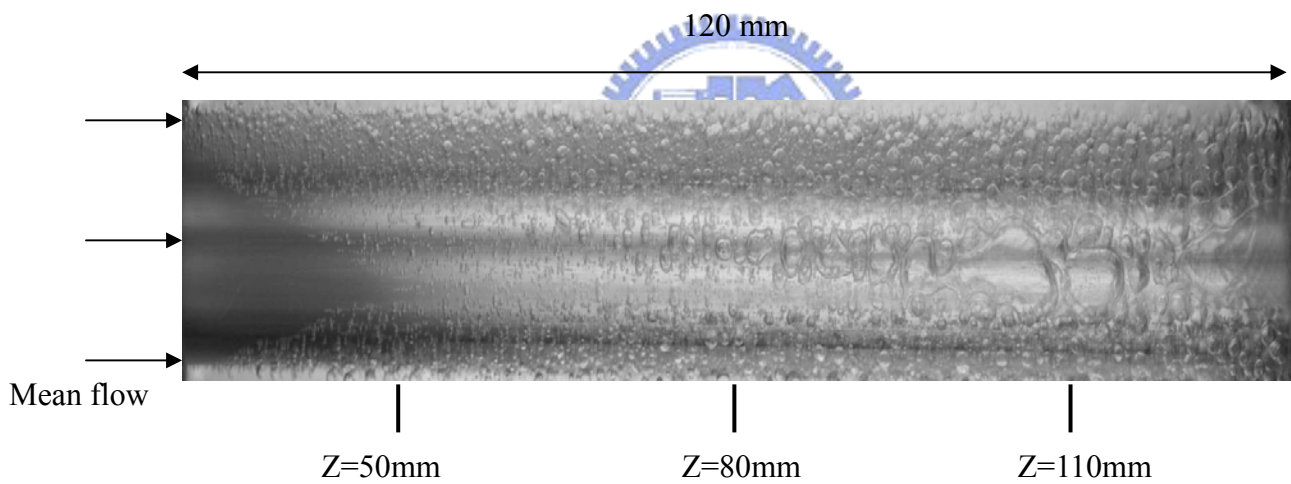


(b) Top view

Fig. 4.13 Photos of boiling flow in the saturated flow boiling of R-134a in the entire duct at $G= 500 \text{ kg/m}^2\text{s}$, $T_{\text{sat}}= 15^\circ\text{C}$, $\delta= 2.0 \text{ mm}$ and $q= 30 \text{ kW/m}^2$ from (a) side view and (b) top view.

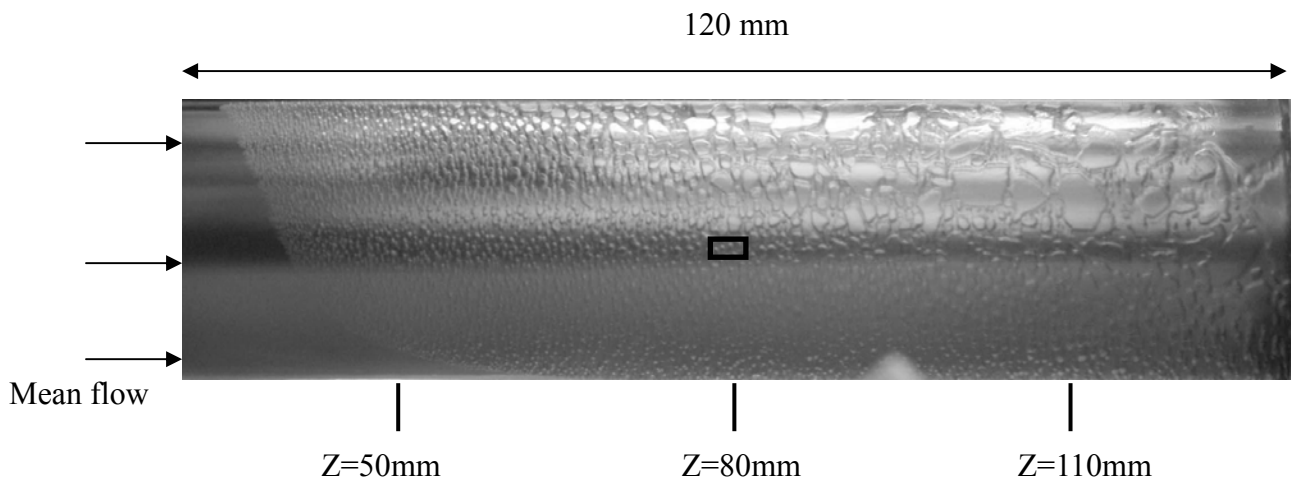


(a) Side view

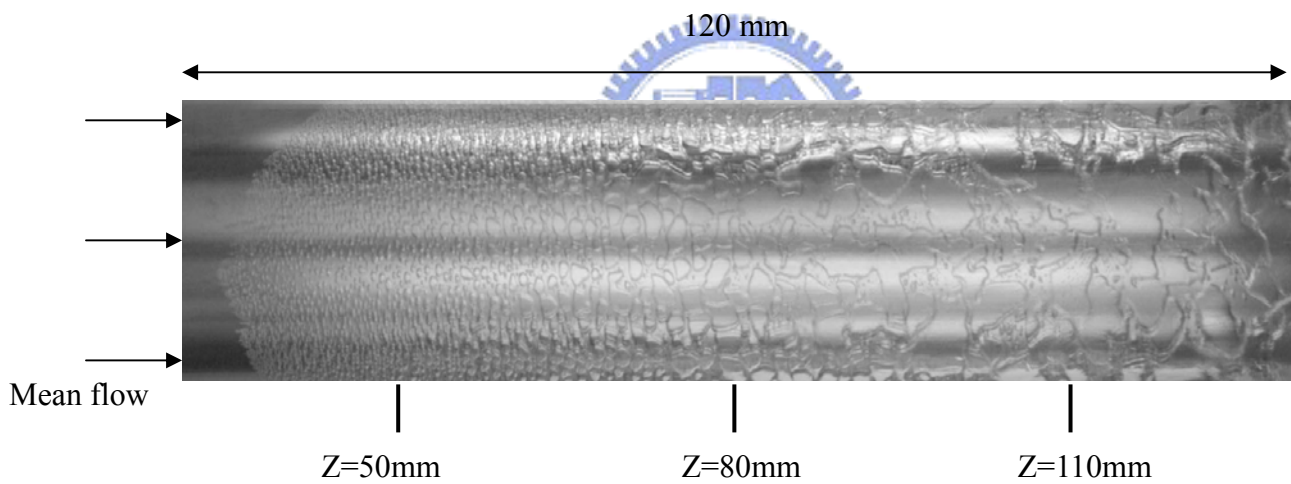


(b) Top view

Fig. 4.14 Photos of boiling flow in the saturated flow boiling of R-134a in the entire duct at $G= 600 \text{ kg/m}^2\text{s}$, $T_{\text{sat}}= 15^\circ\text{C}$, $\delta= 1.0 \text{ mm}$ and $q= 30 \text{ kW/m}^2$ from (a) side view and (b) top view.

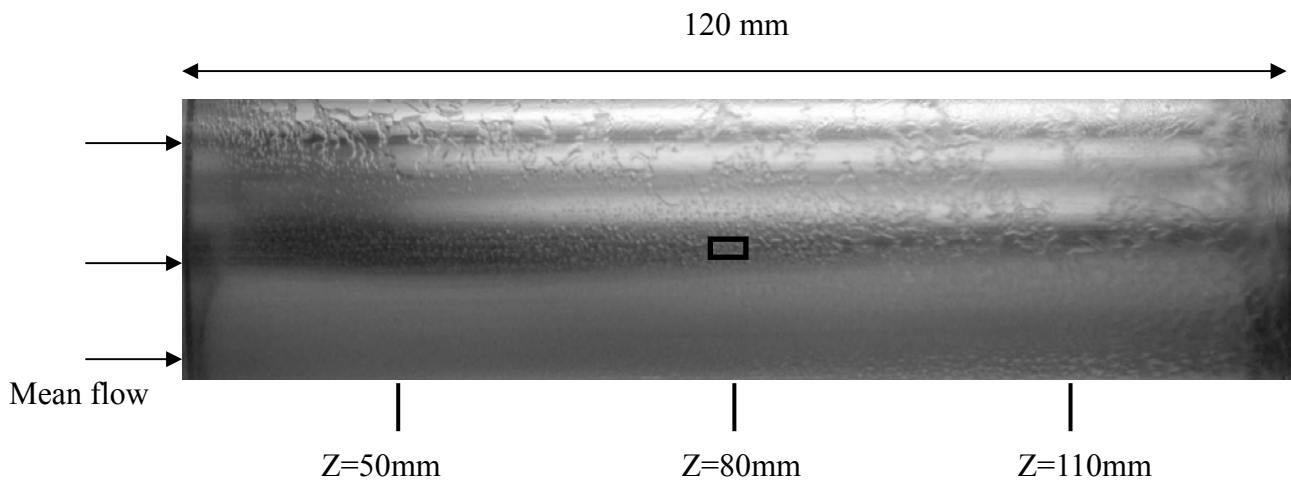


(a) Side view

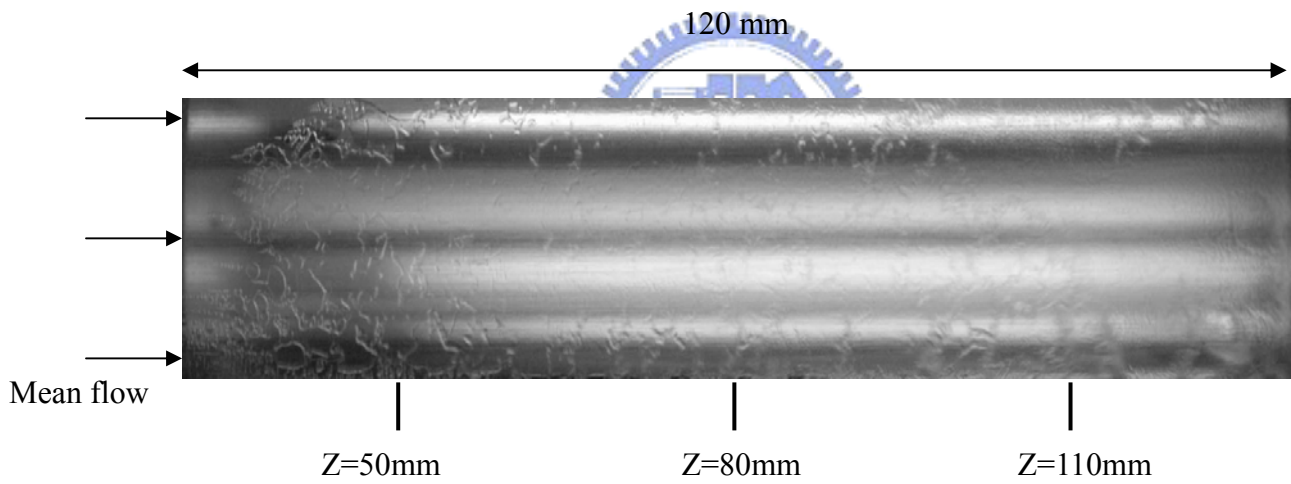


(b) Top view

Fig. 4.15 Photos of boiling flow in the saturated flow boiling of R-134a in the entire duct at $G= 600 \text{ kg/m}^2\text{s}$, $T_{\text{sat}}= 15^\circ\text{C}$, $\delta= 0.5 \text{ mm}$ and $q= 30 \text{ kW/m}^2$ from (a) side view and (b) top view.



(a) Side view



(b) Top view

Fig. 4.16 Photos of boiling flow in the saturated flow boiling of R-134a in the entire duct at $G= 600 \text{ kg/m}^2\text{s}$, $T_{\text{sat}}= 15^\circ\text{C}$, $\delta= 0.2 \text{ mm}$ and $q=30 \text{ kW/m}^2$ from (a) side view and (b) top view.

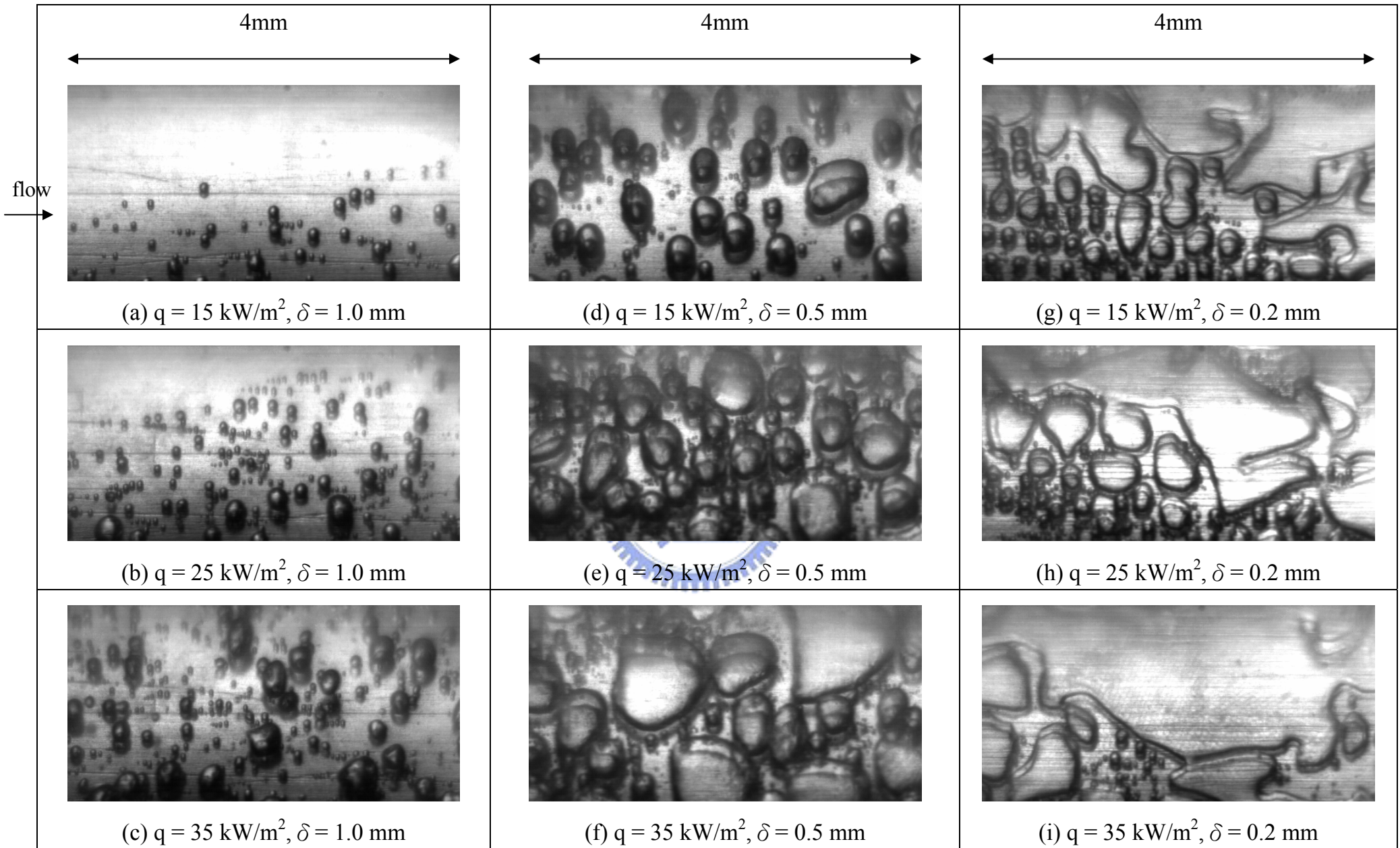


Fig. 4.17 Photos of bubbles in the saturated flow boiling of R-134a in a small region around middle axial location at $T_{\text{sat}} = 15^\circ\text{C}$ and $G = 600\text{-kg/m}^2\text{s}$ for various imposed heat flux and gap sizes.

Fig. 4.18 Photos of bubbles in the saturated flow boiling of R-134a in a small region around middle axial location at $\delta=0.5$ mm for various imposed heat flux, mass fluxes and refrigerant saturated temperatures.

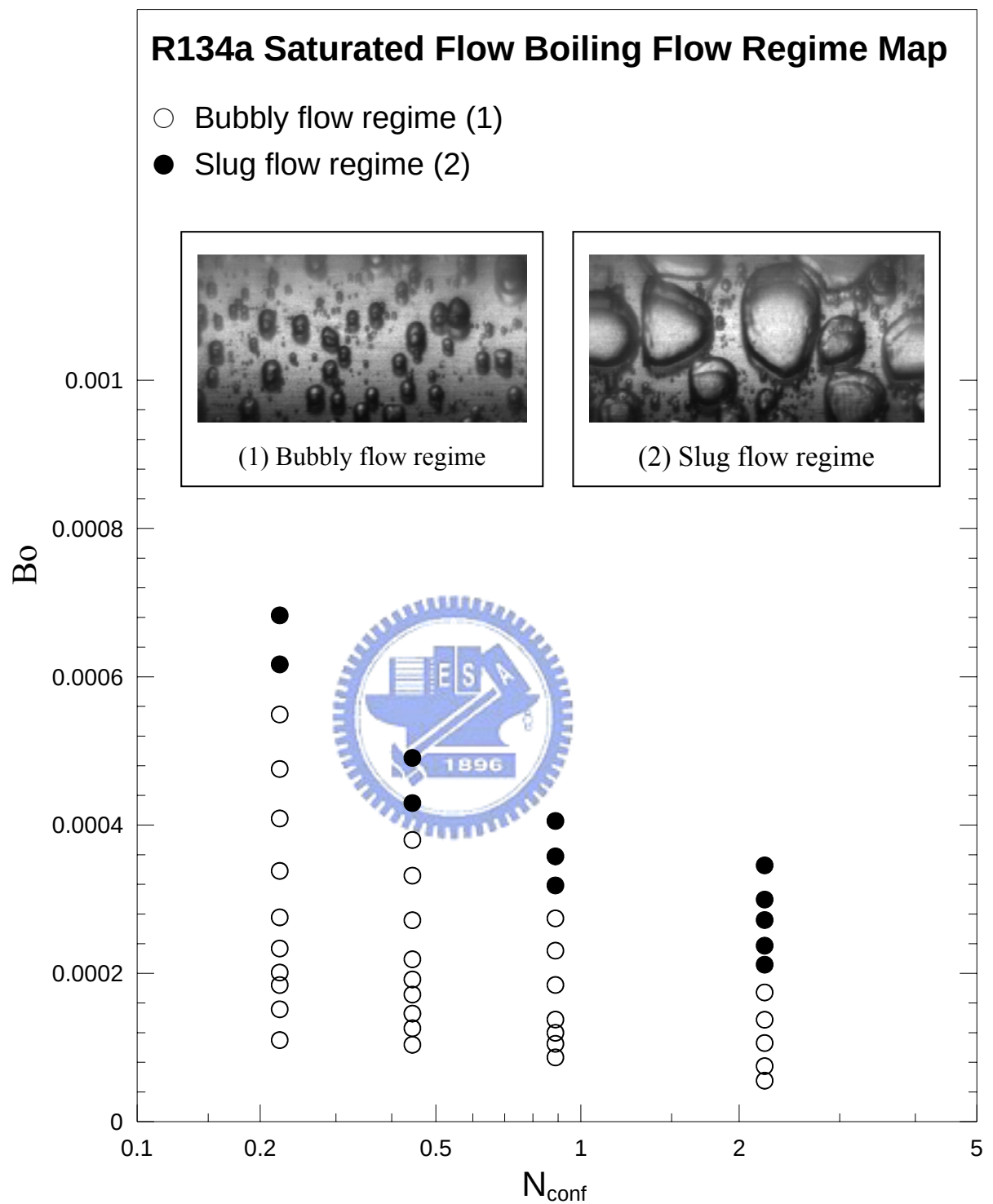


Fig.4.19 Flow regime map for different flow patterns at statistically steady-state observed from flow visualization (43 cases).

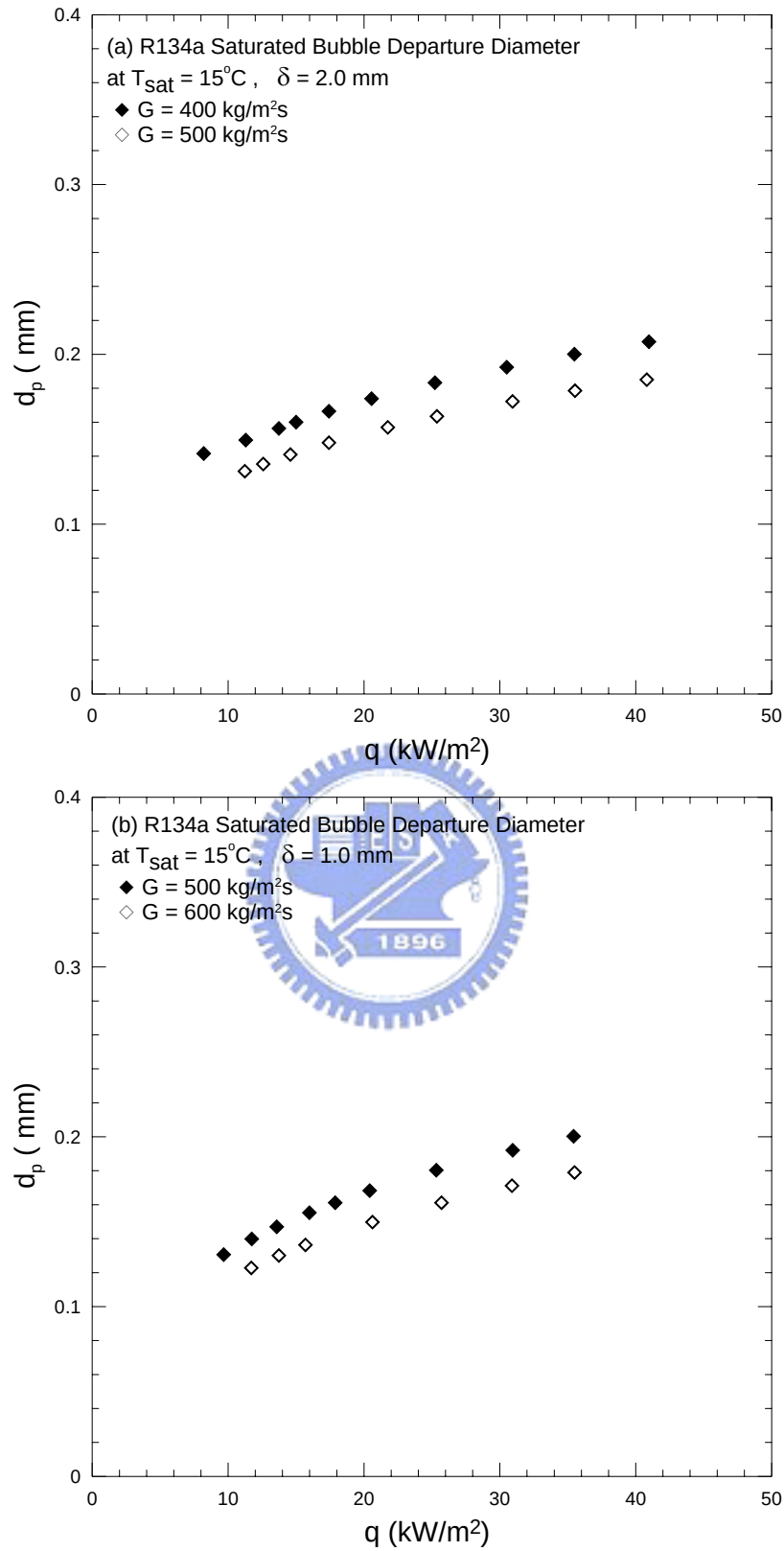


Fig. 4.20 Saturated flow boiling mean bubble departure diameter for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 2.0 \text{ mm}$ and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 1.0 \text{ mm}$.

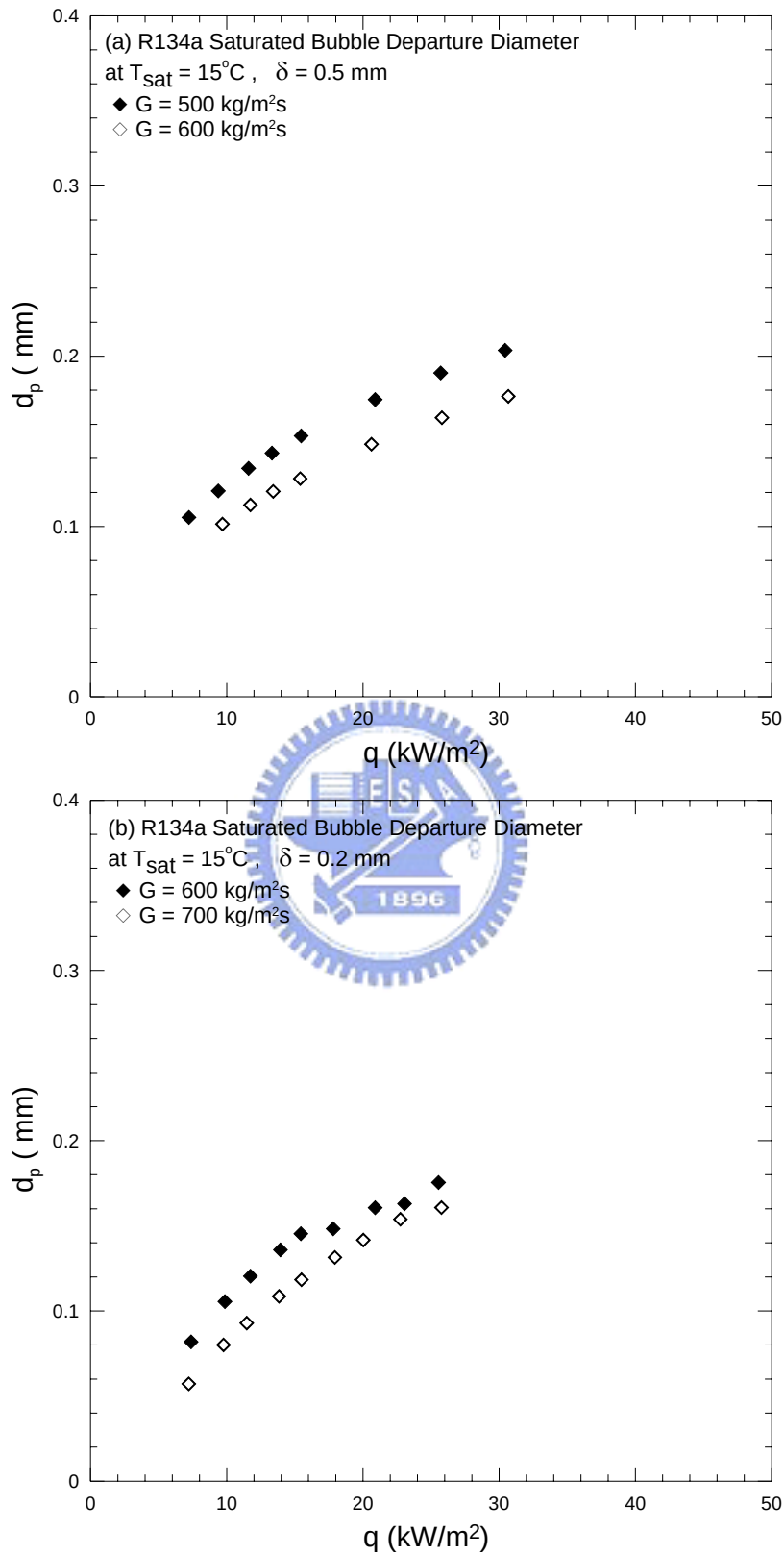


Fig. 4.21 Saturated flow boiling mean bubble departure diameter for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 0.5 \text{ mm}$ and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 0.2 \text{ mm}$.

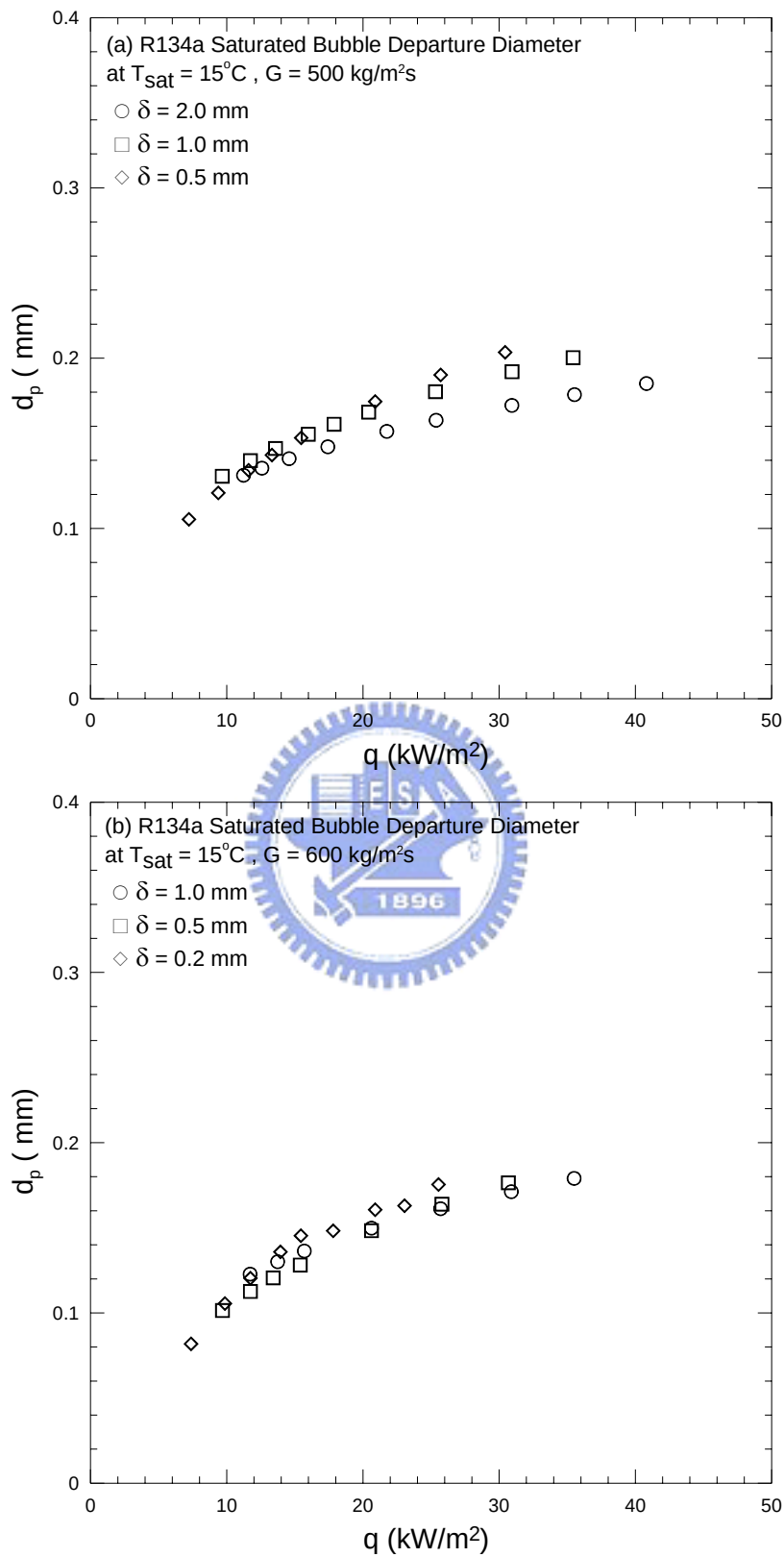


Fig. 4.22 Saturated flow boiling mean bubble departure diameter for various gap sizes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $G = 500 \text{ kg/m}^2\text{s}$ and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $G = 600 \text{ kg/m}^2\text{s}$.

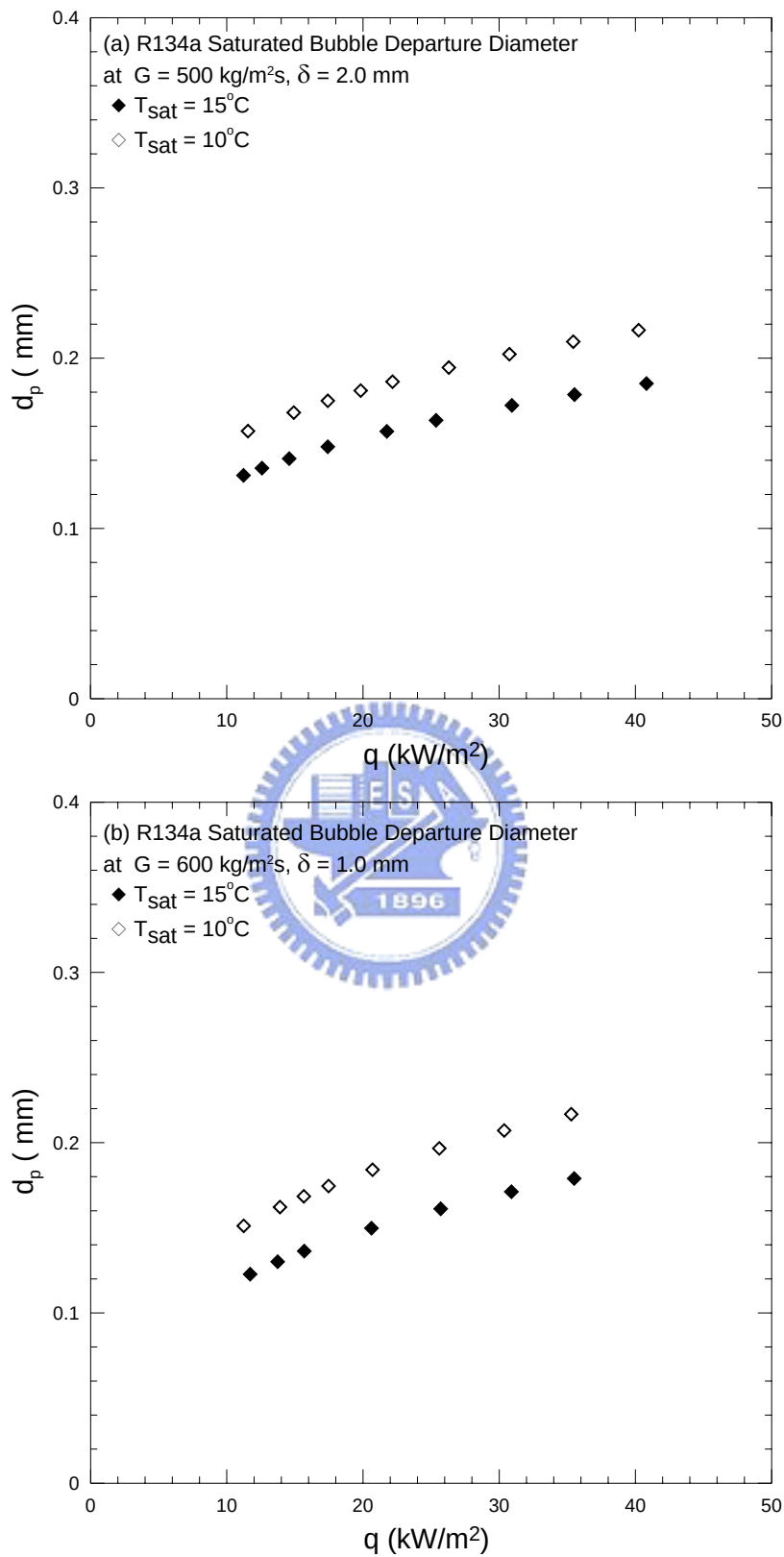


Fig. 4.23 Saturated flow boiling mean bubble departure diameter for various refrigerant saturated temperatures at (a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 2.0 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 1.0 \text{ mm}$.

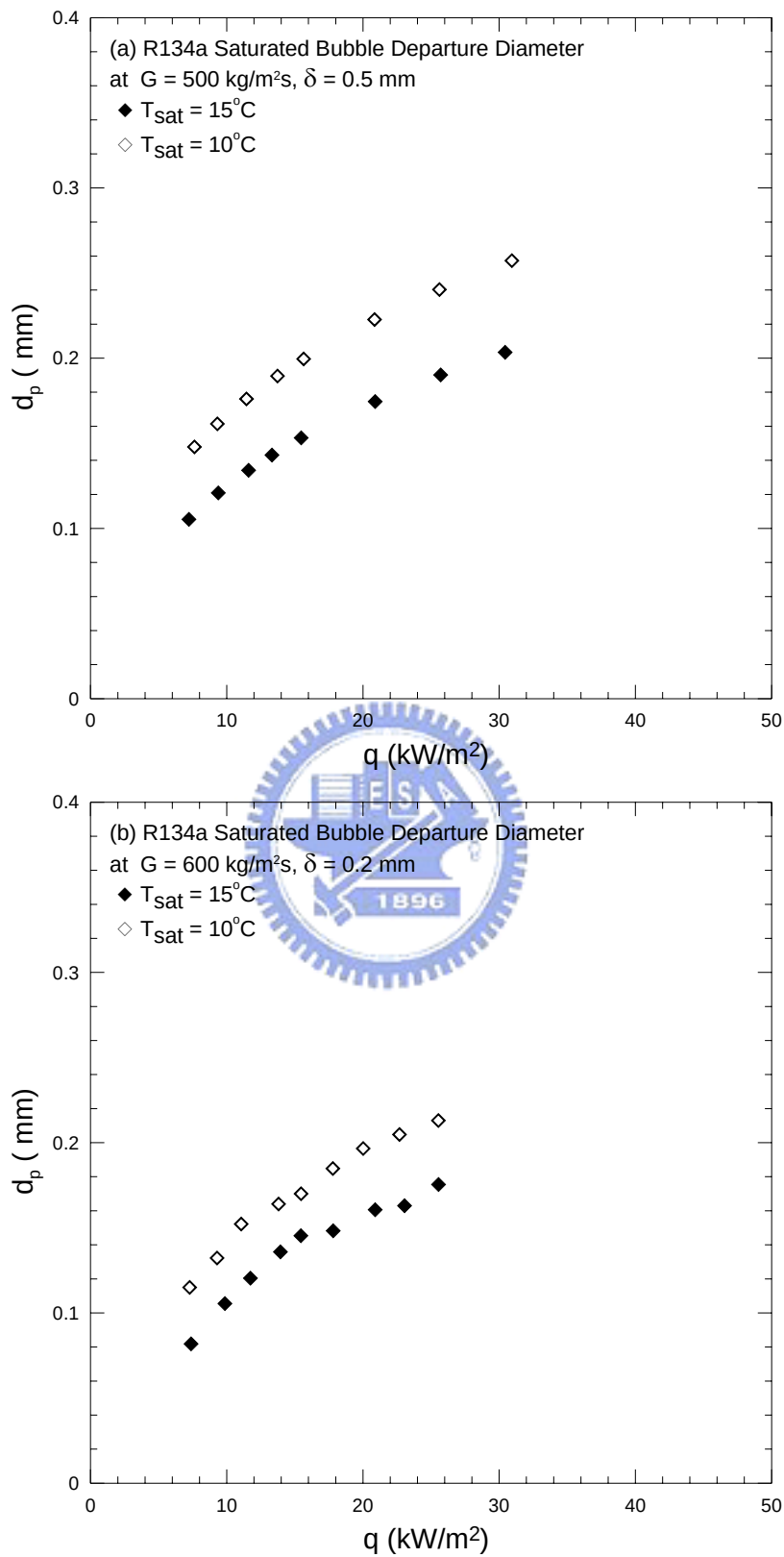


Fig. 4.24 Saturated flow boiling mean bubble departure diameter for various refrigerant saturated temperatures at (a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 0.5 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 0.2 \text{ mm}$.

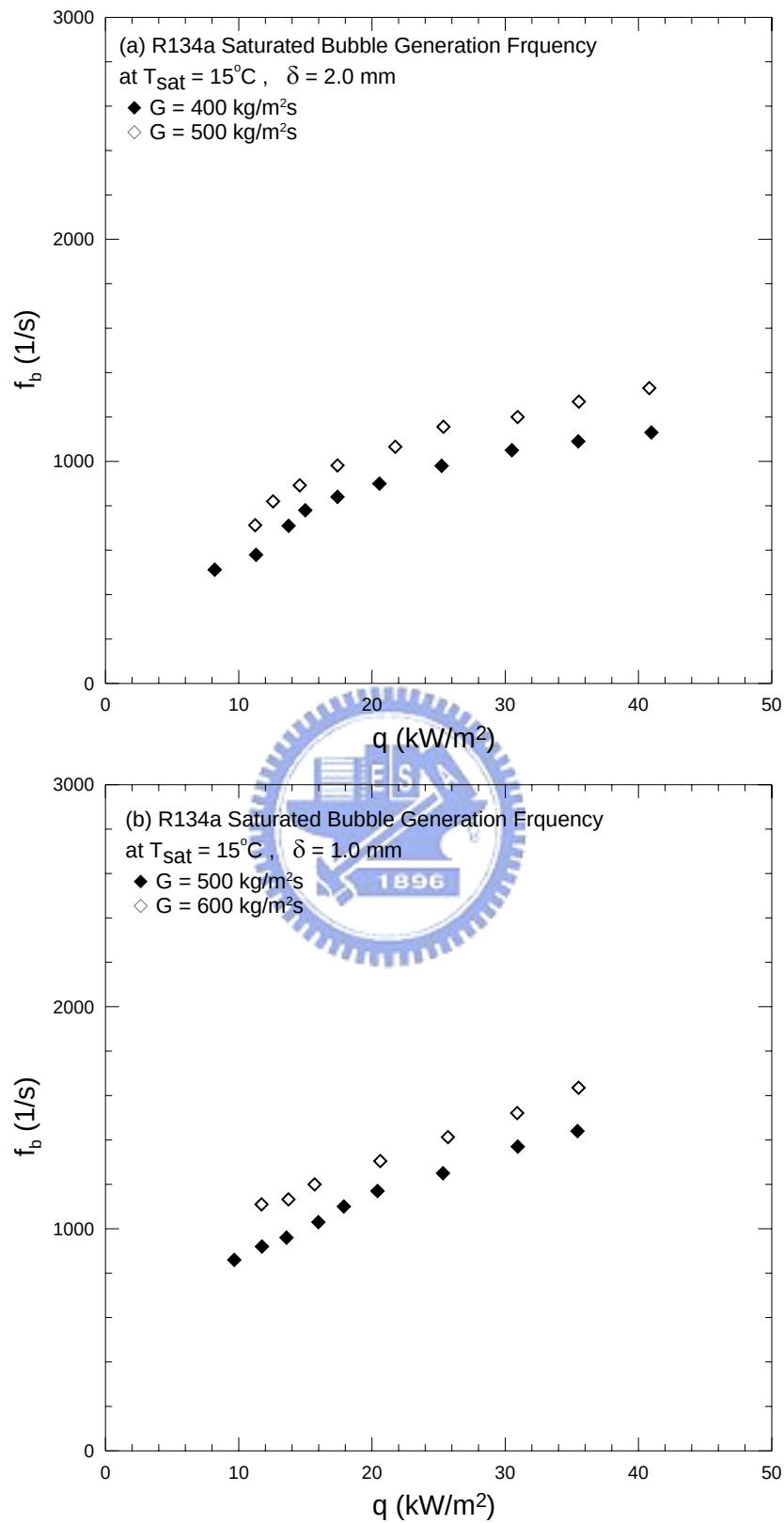


Fig. 4.25 Saturated flow boiling mean bubble departure frequency for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 2.0$ mm and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 1.0$ mm.

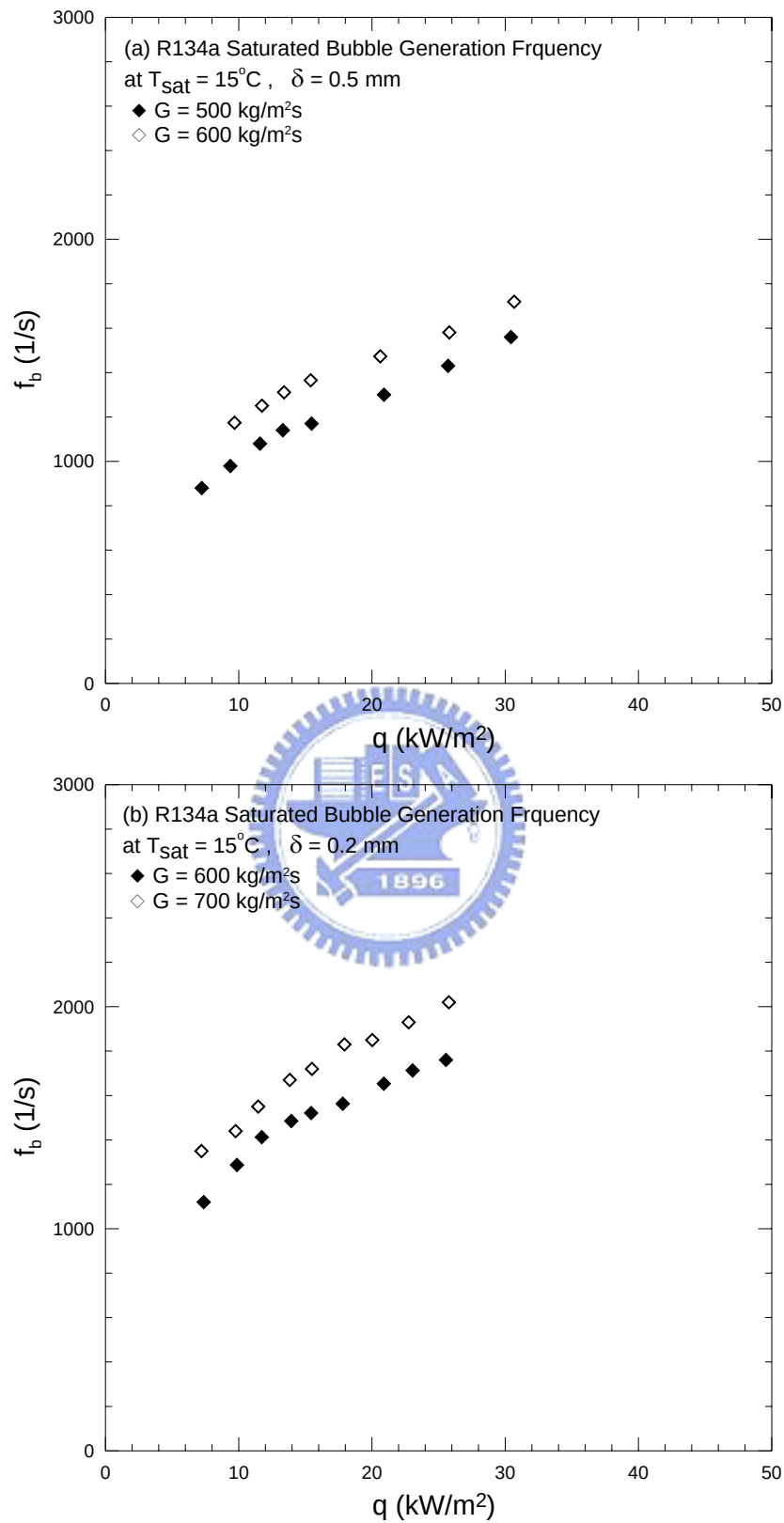


Fig. 4.26 Saturated flow boiling mean bubble departure frequency for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 0.5 \text{ mm}$ and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $\delta = 0.2 \text{ mm}$.

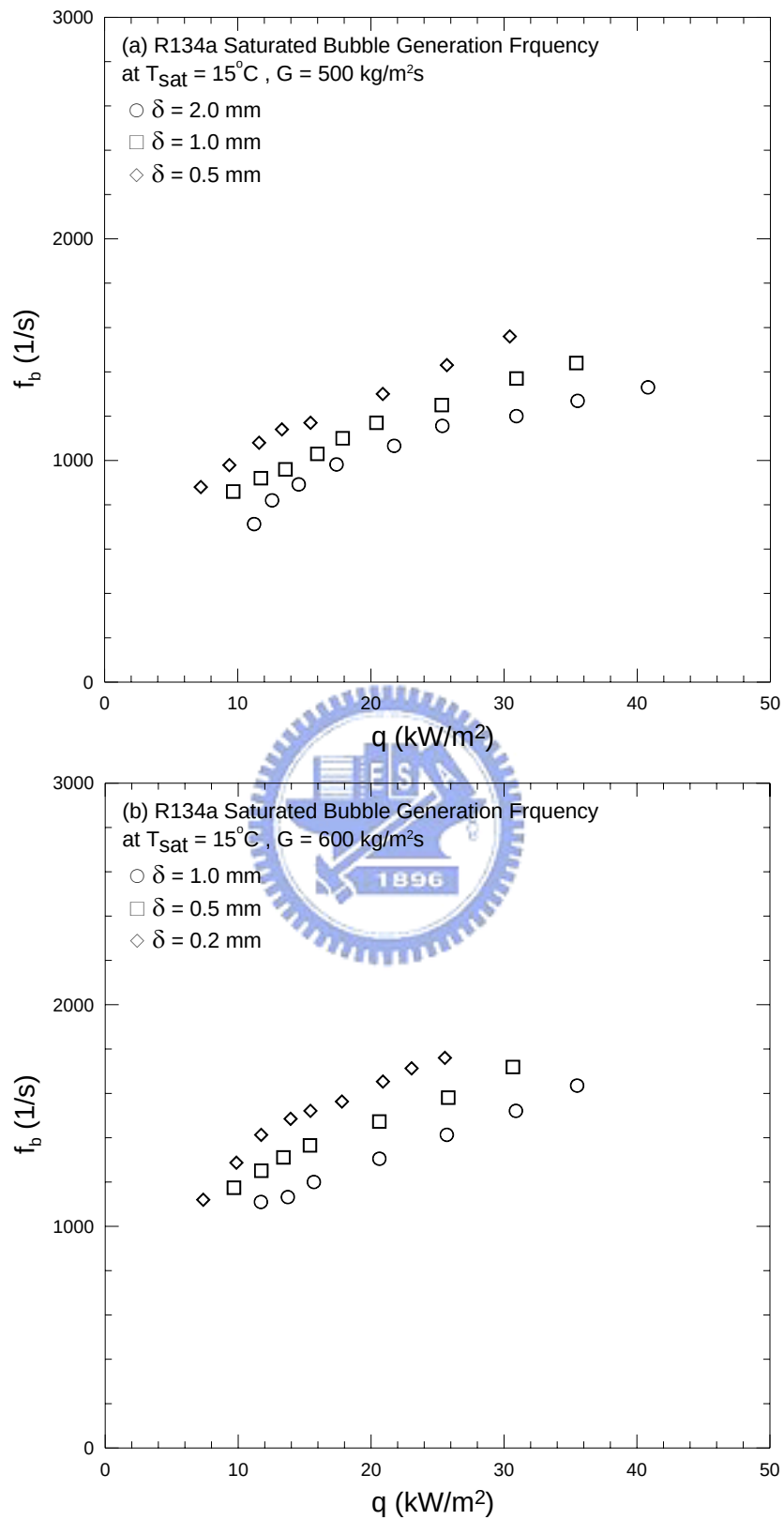


Fig. 4.27 Saturated flow boiling mean bubble departure frequency for various gap sizes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $G = 500 \text{ kg/m}^2\text{s}$ and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $G = 600 \text{ kg/m}^2\text{s}$.

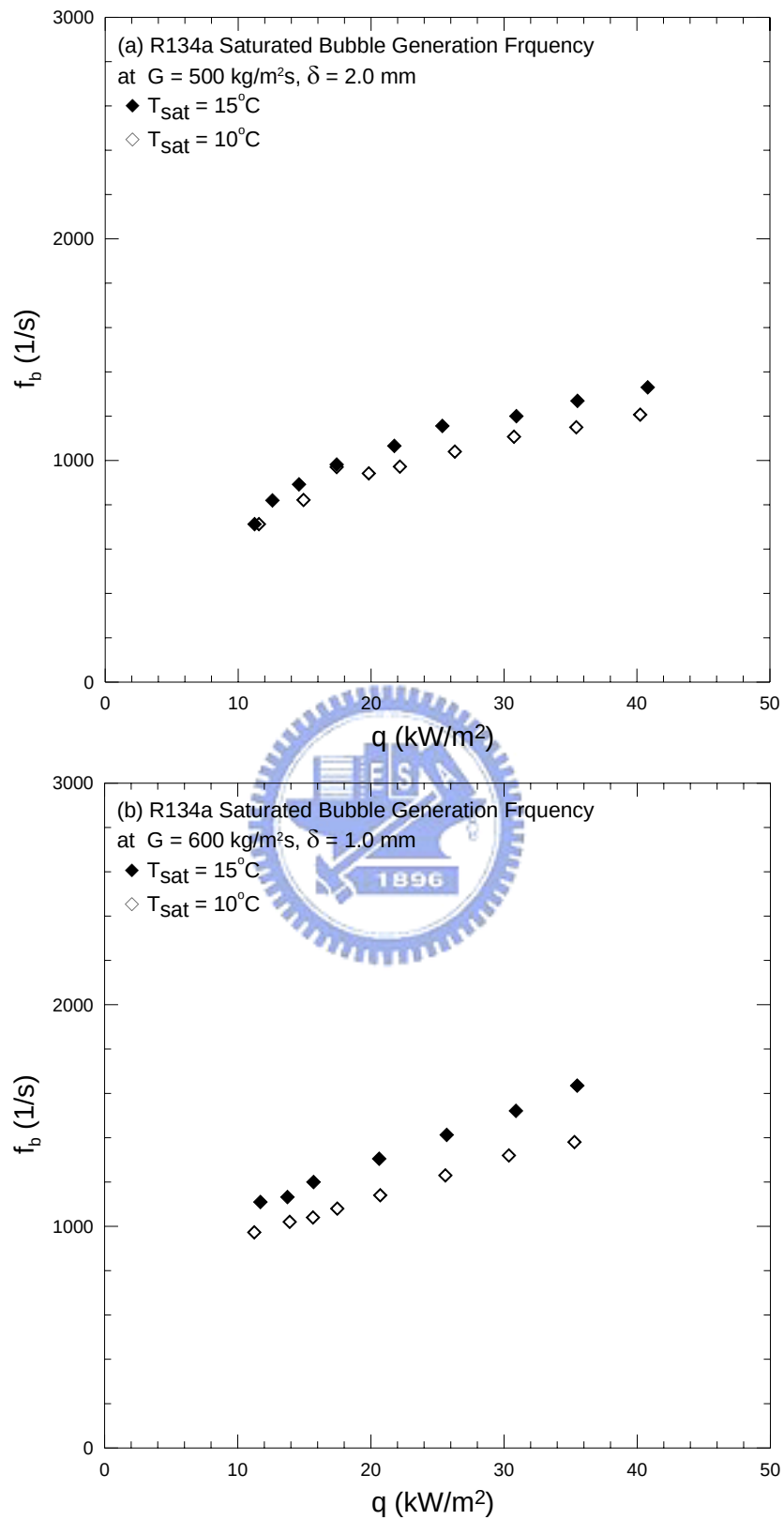


Fig. 4.28 Saturated flow boiling mean bubble departure frequency for various refrigerant saturated temperatures at (a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 2.0 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 1.0 \text{ mm}$.

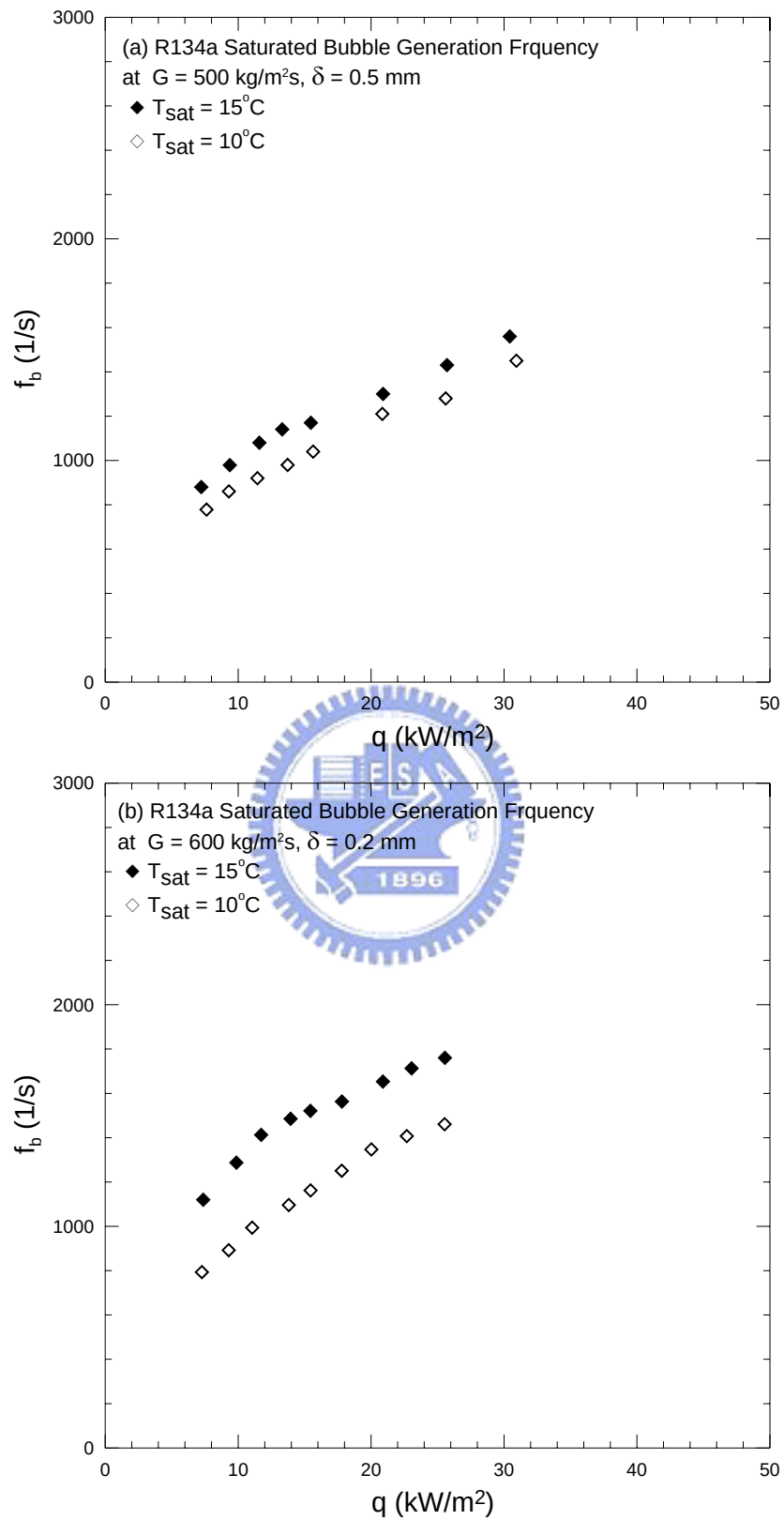


Fig. 4.29 Saturated flow boiling mean bubble departure frequency for various refrigerant saturated temperatures at (a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 0.5 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 0.2 \text{ mm}$.

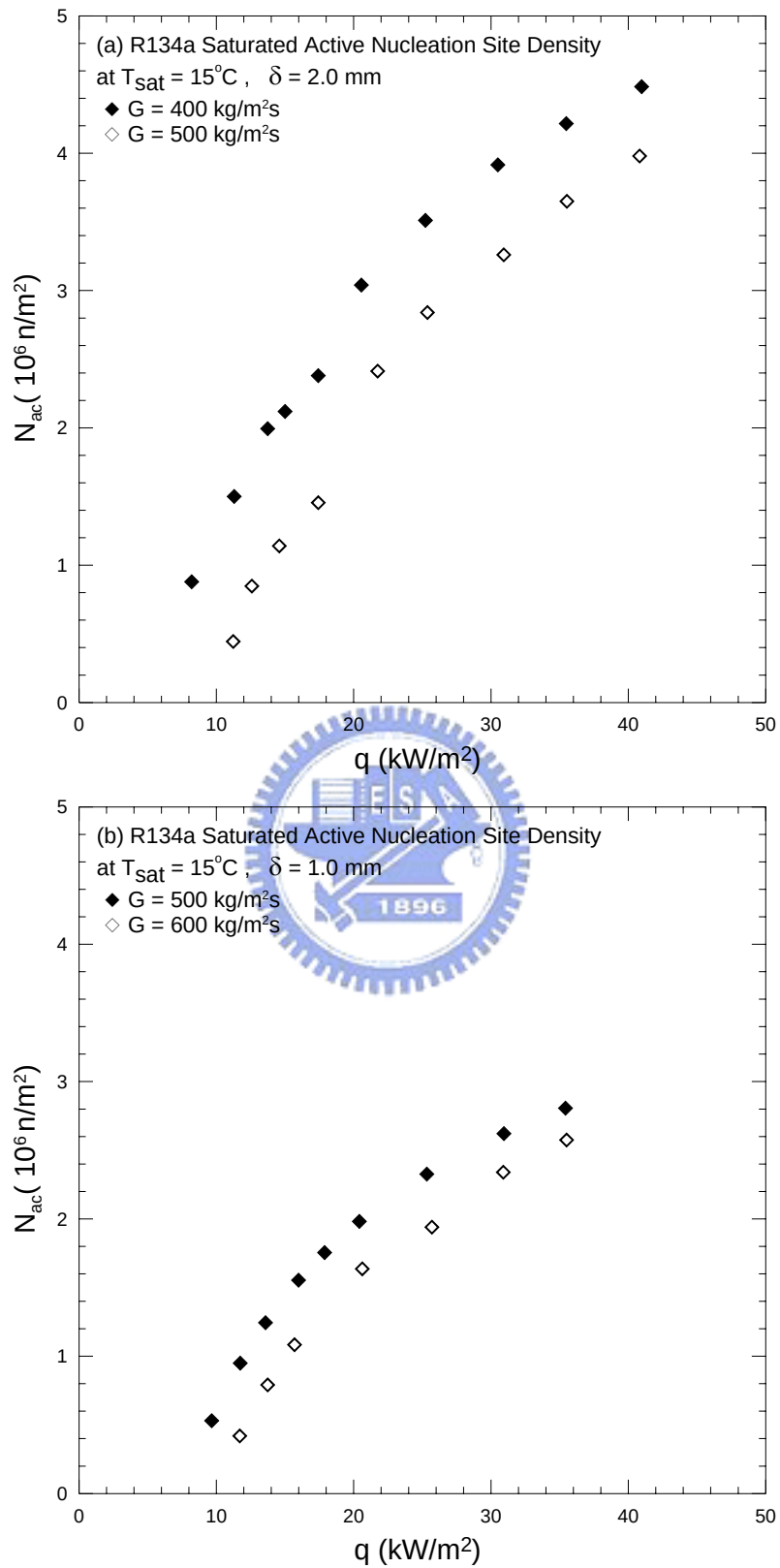


Fig. 4.30 Saturated flow boiling mean active nucleation site density for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^{\circ}\text{C}$ & $\delta = 2.0 \text{ mm}$ and (b) $T_{\text{sat}} = 15^{\circ}\text{C}$ & $\delta = 1.0 \text{ mm}$.

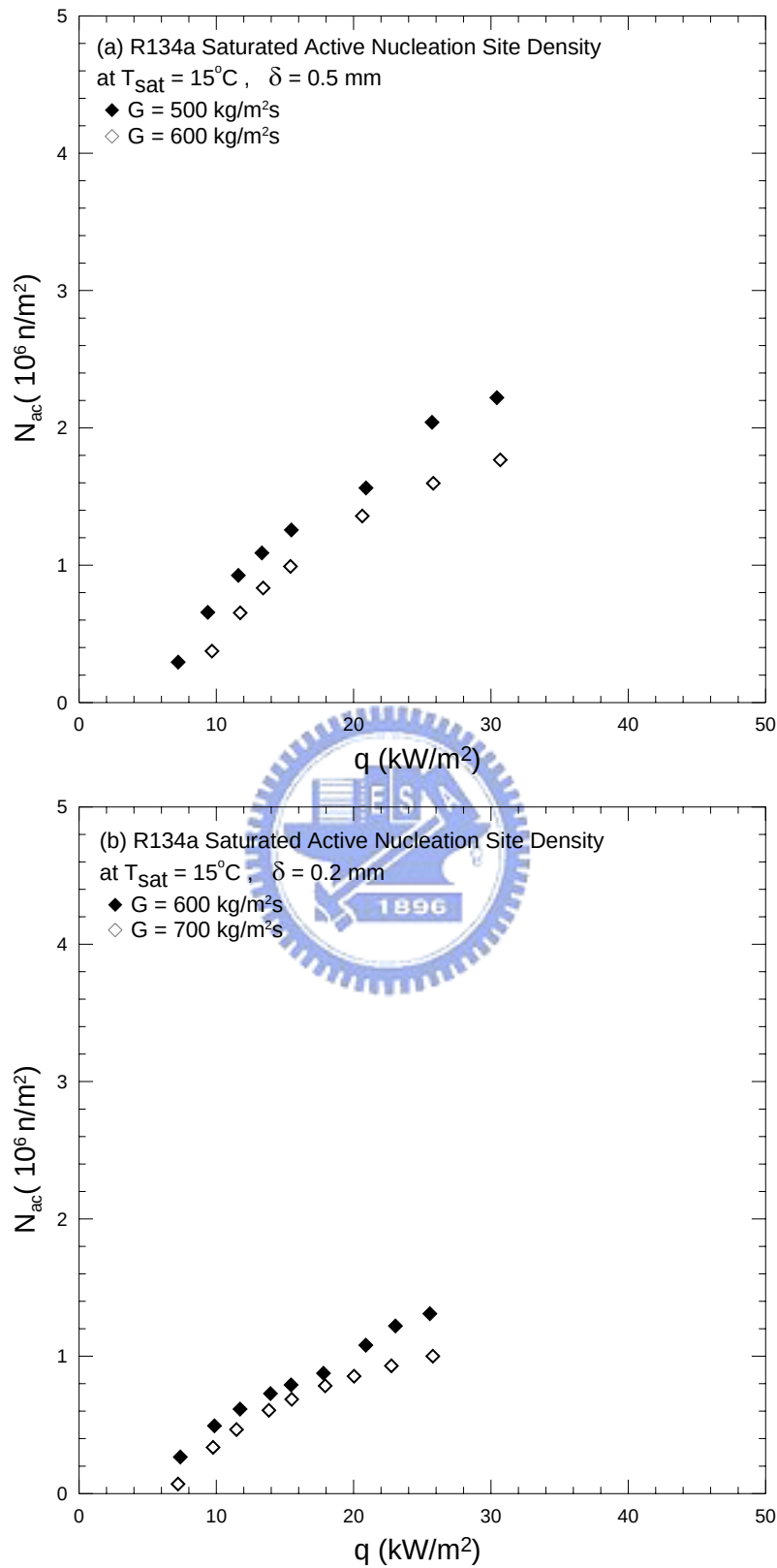


Fig. 4.31 Saturated flow boiling mean active nucleation site density for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^{\circ}\text{C}$ & $\delta = 0.5 \text{ mm}$ and (b) $T_{\text{sat}} = 15^{\circ}\text{C}$ & $\delta = 0.2 \text{ mm}$.

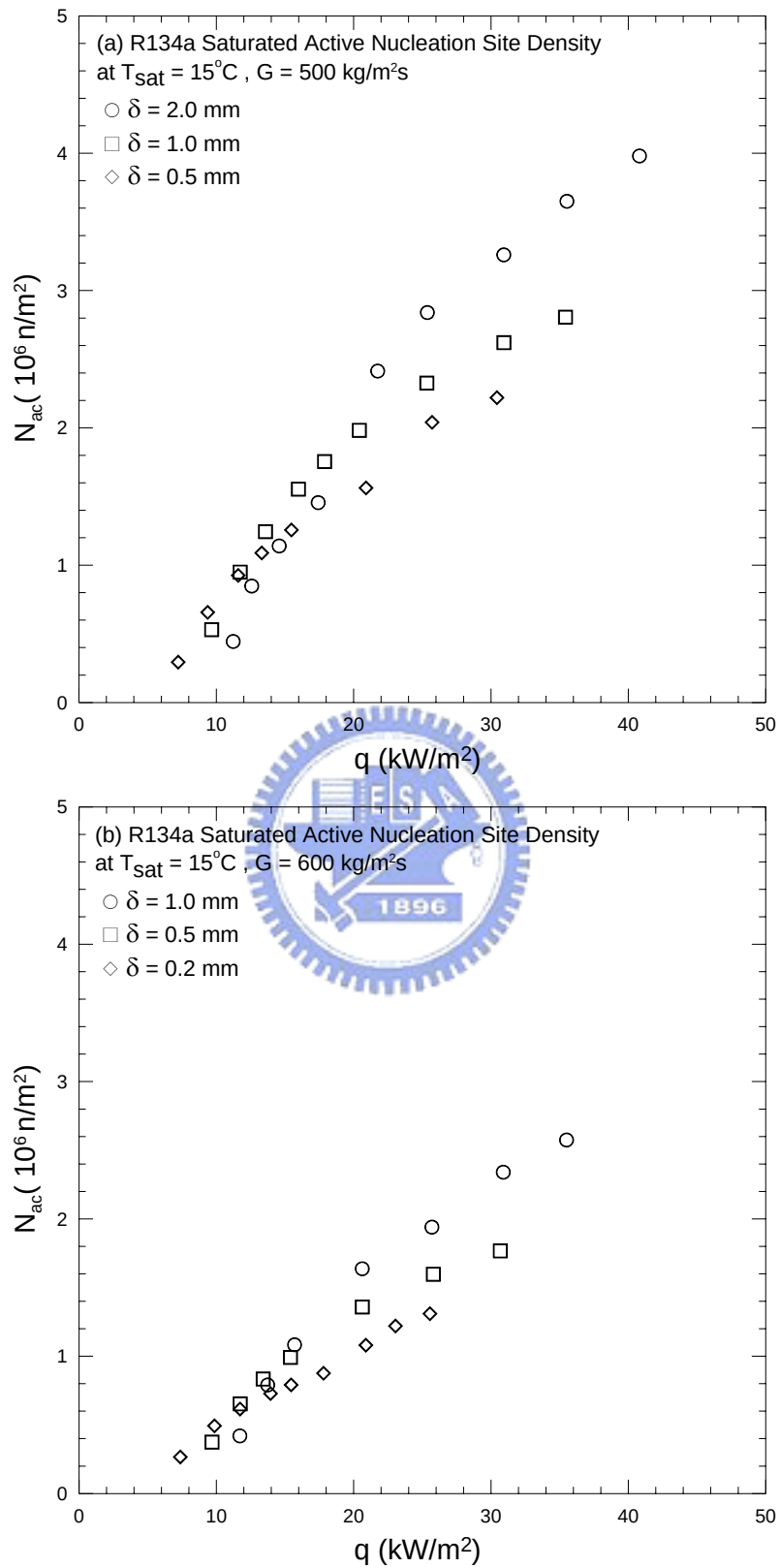


Fig. 4.32 Saturated flow boiling mean active nucleation site density for various gap sizes at (a) $T_{\text{sat}} = 15^\circ\text{C}$ & $G = 500 \text{ kg/m}^2\text{s}$ and (b) $T_{\text{sat}} = 15^\circ\text{C}$ & $G = 600 \text{ kg/m}^2\text{s}$.

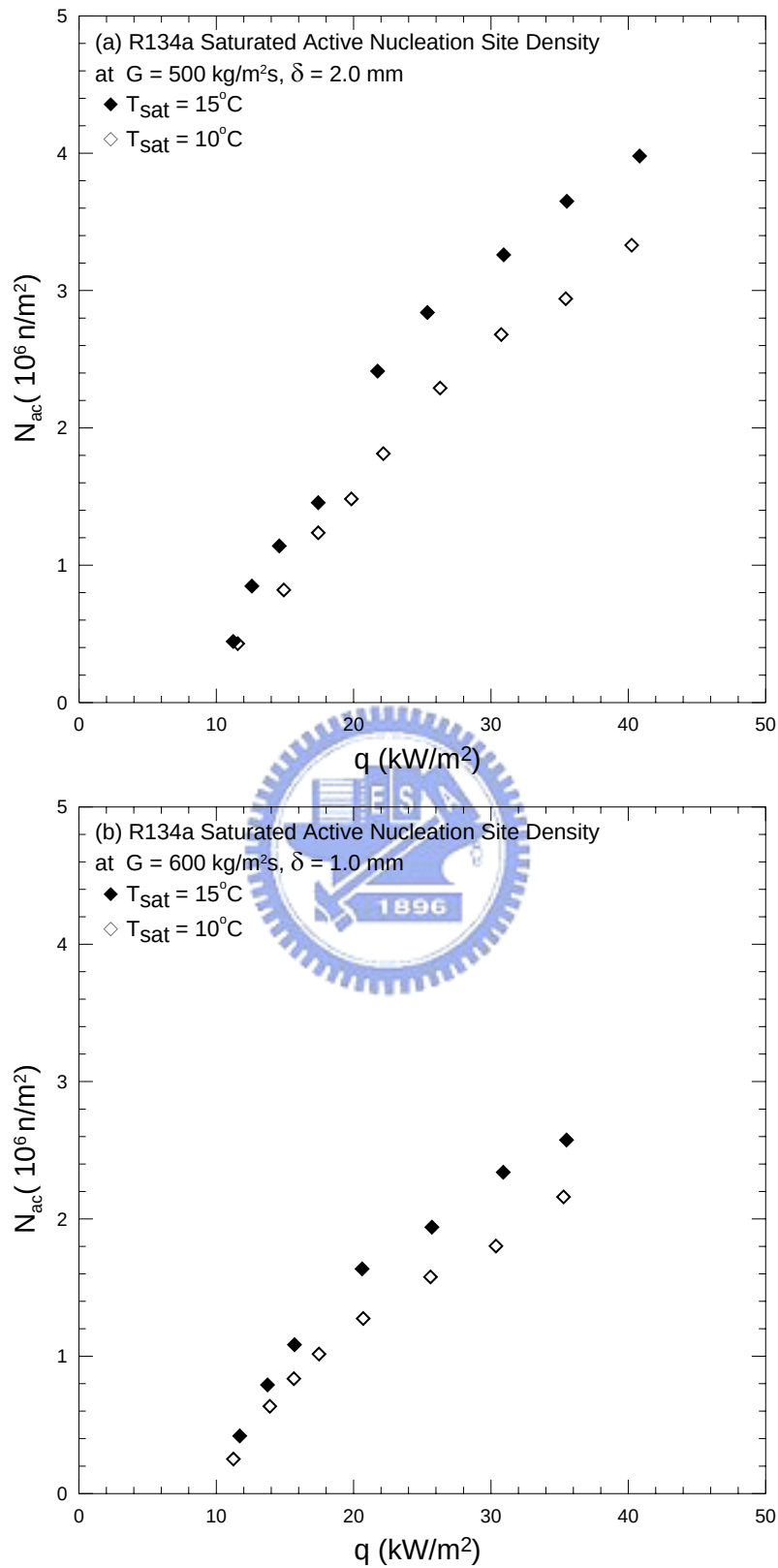


Fig. 4.33 Saturated flow boiling mean active nucleation site density for various refrigerant saturated temperatures at (a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 2.0 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 1.0 \text{ mm}$.

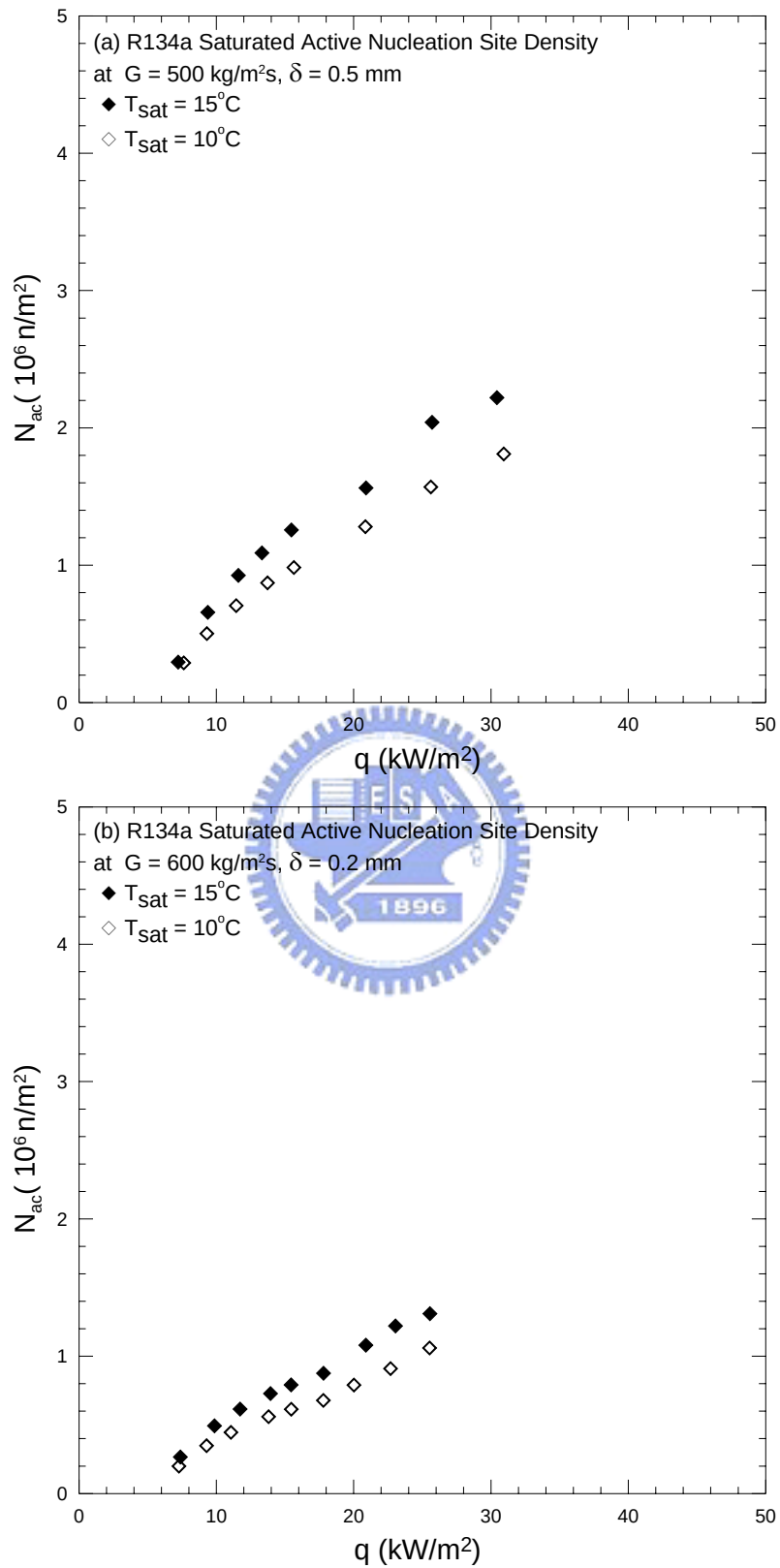


Fig. 4.34 Saturated flow boiling mean active nucleation site density for various refrigerant saturated temperatures at (a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 0.5 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 0.2 \text{ mm}$.

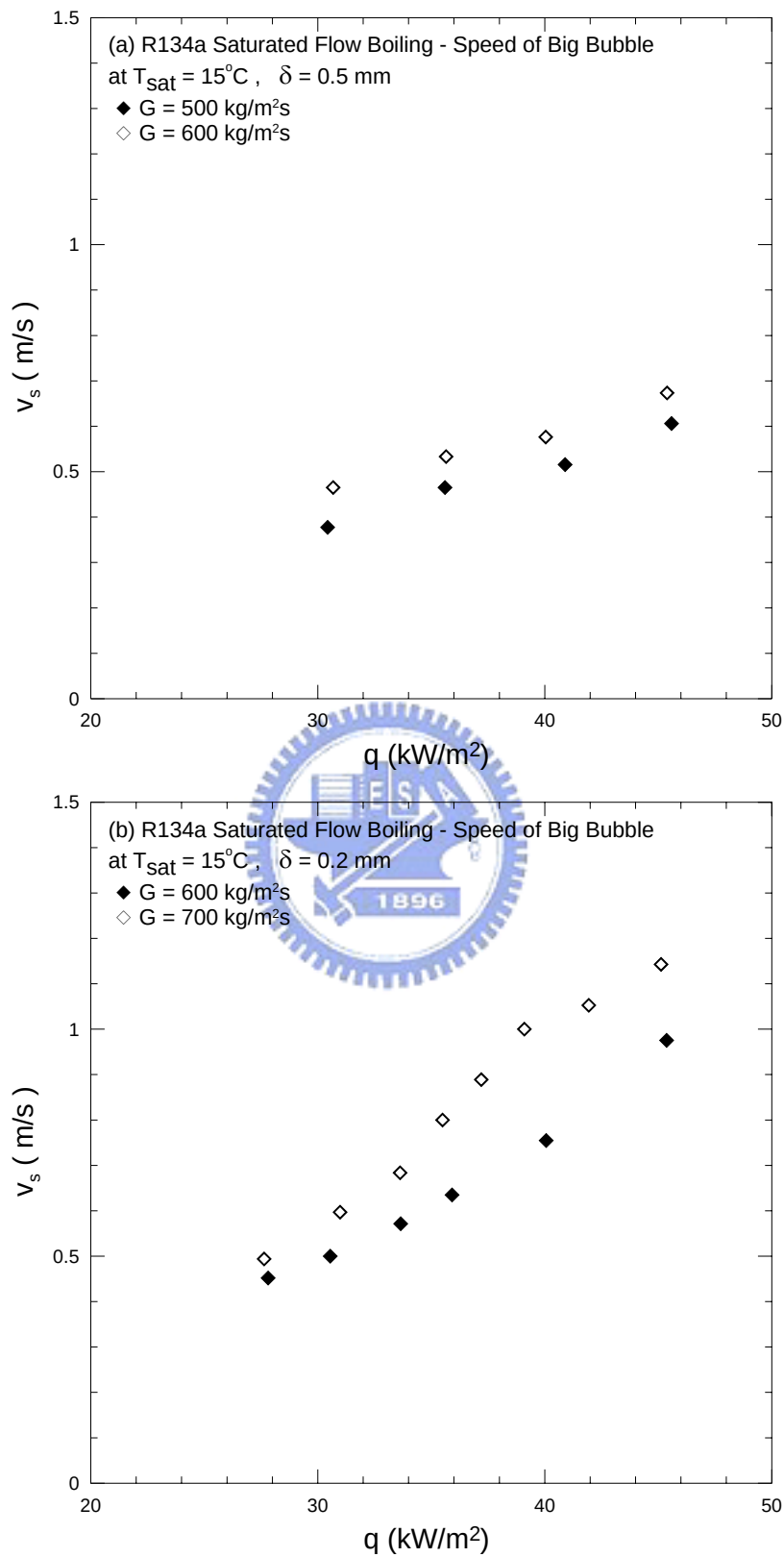


Fig. 4.35 Mean axial speed of the big bubbles in slug flow for various refrigerant mass fluxes at (a) $T_{\text{sat}} = 15^{\circ}\text{C}$ & $\delta = 0.5 \text{ mm}$ and (b) $T_{\text{sat}} = 15^{\circ}\text{C}$ & $\delta = 0.2 \text{ mm}$.

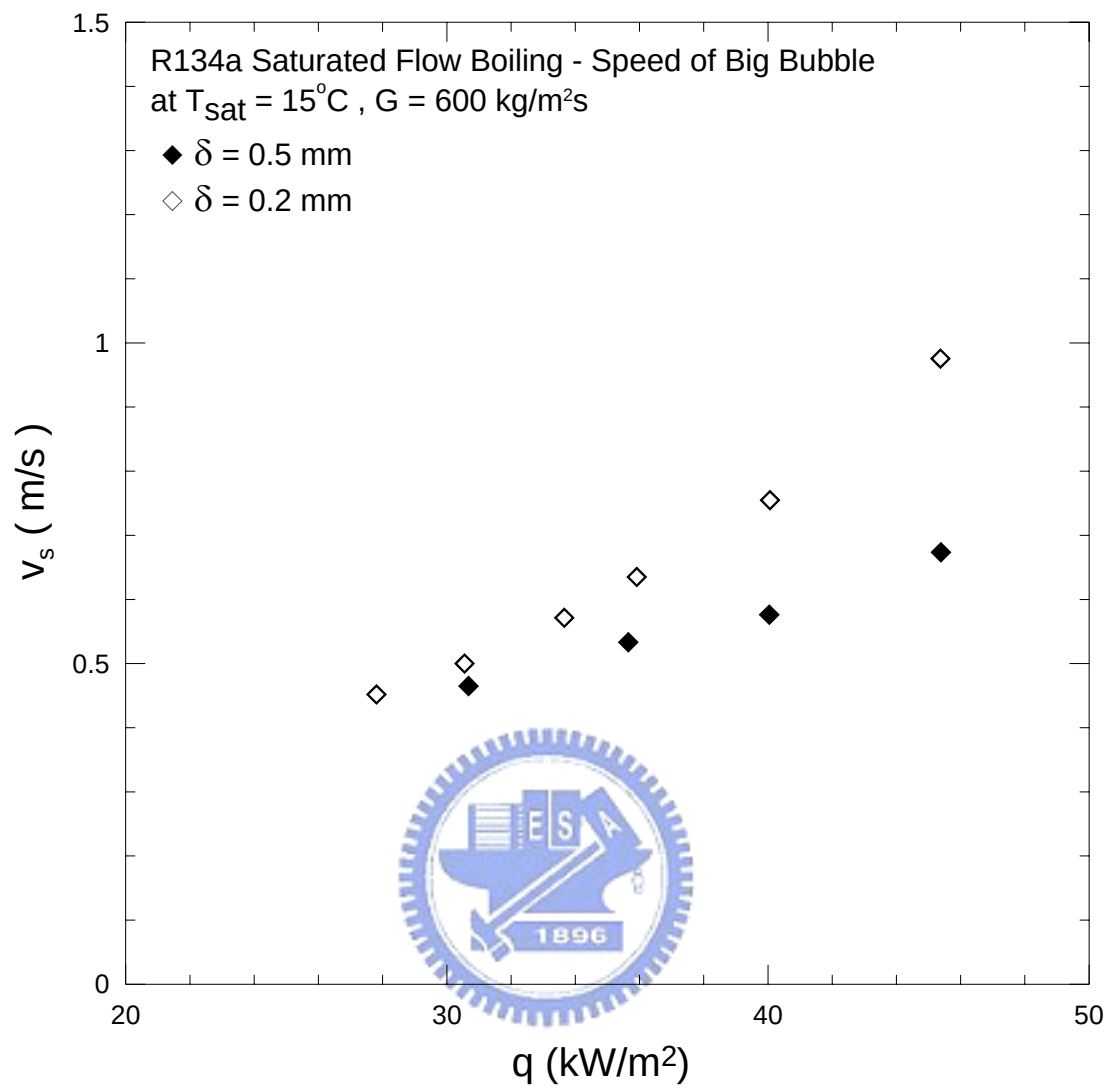


Fig. 4.36 Mean axial speed of the big bubbles in slug flow for various gap sizes at $T_{\text{sat}} = 15^\circ\text{C}$ & $G = 600 \text{ kg/m}^2\text{s}$.

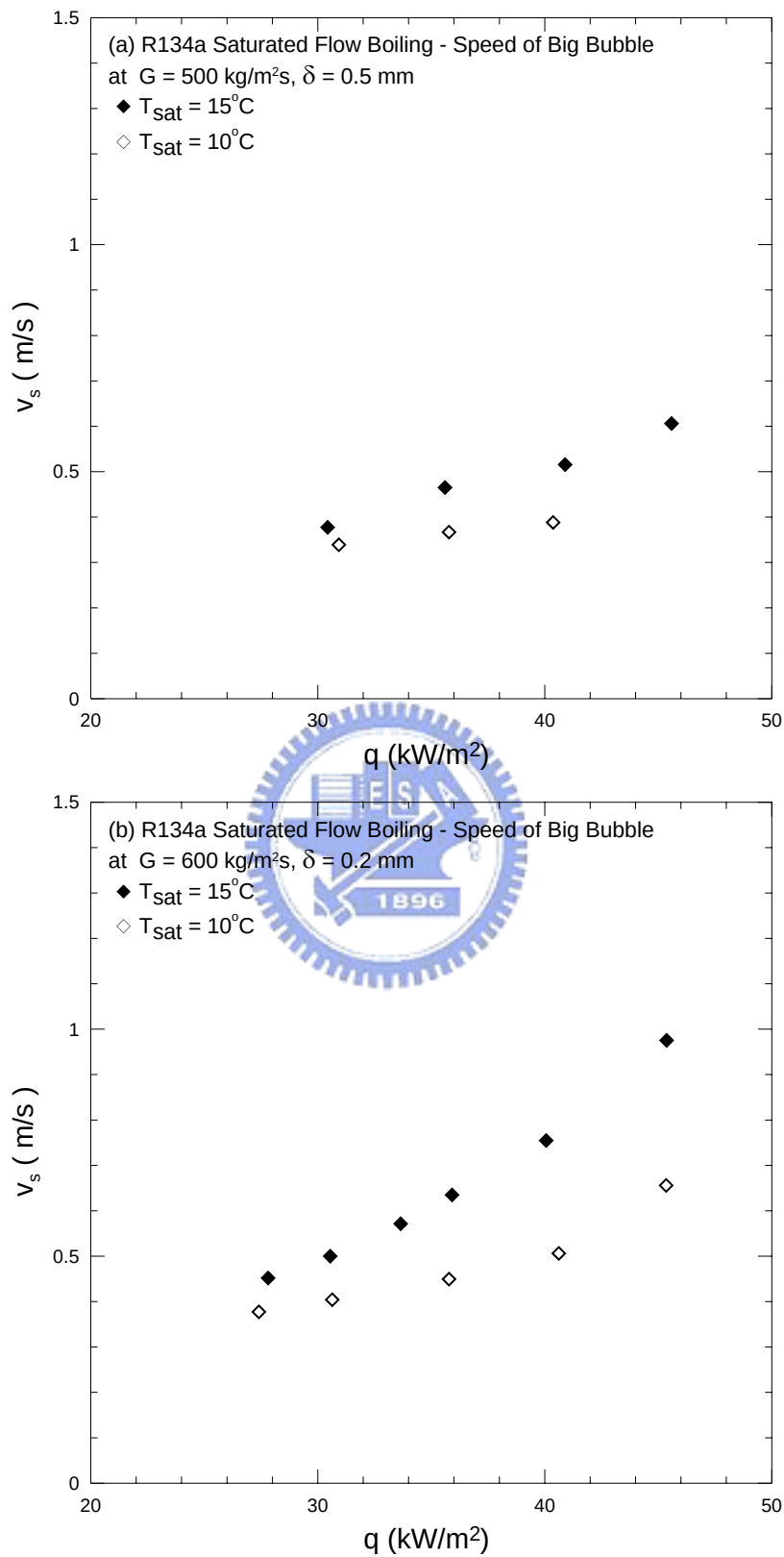


Fig. 4.37 Mean axial speed of the big bubbles in slug flow for various refrigerant saturated temperatures at (a) $G = 500 \text{ kg/m}^2\text{s}$ & $\delta = 0.5 \text{ mm}$ and (b) $G = 600 \text{ kg/m}^2\text{s}$ & $\delta = 0.2 \text{ mm}$.

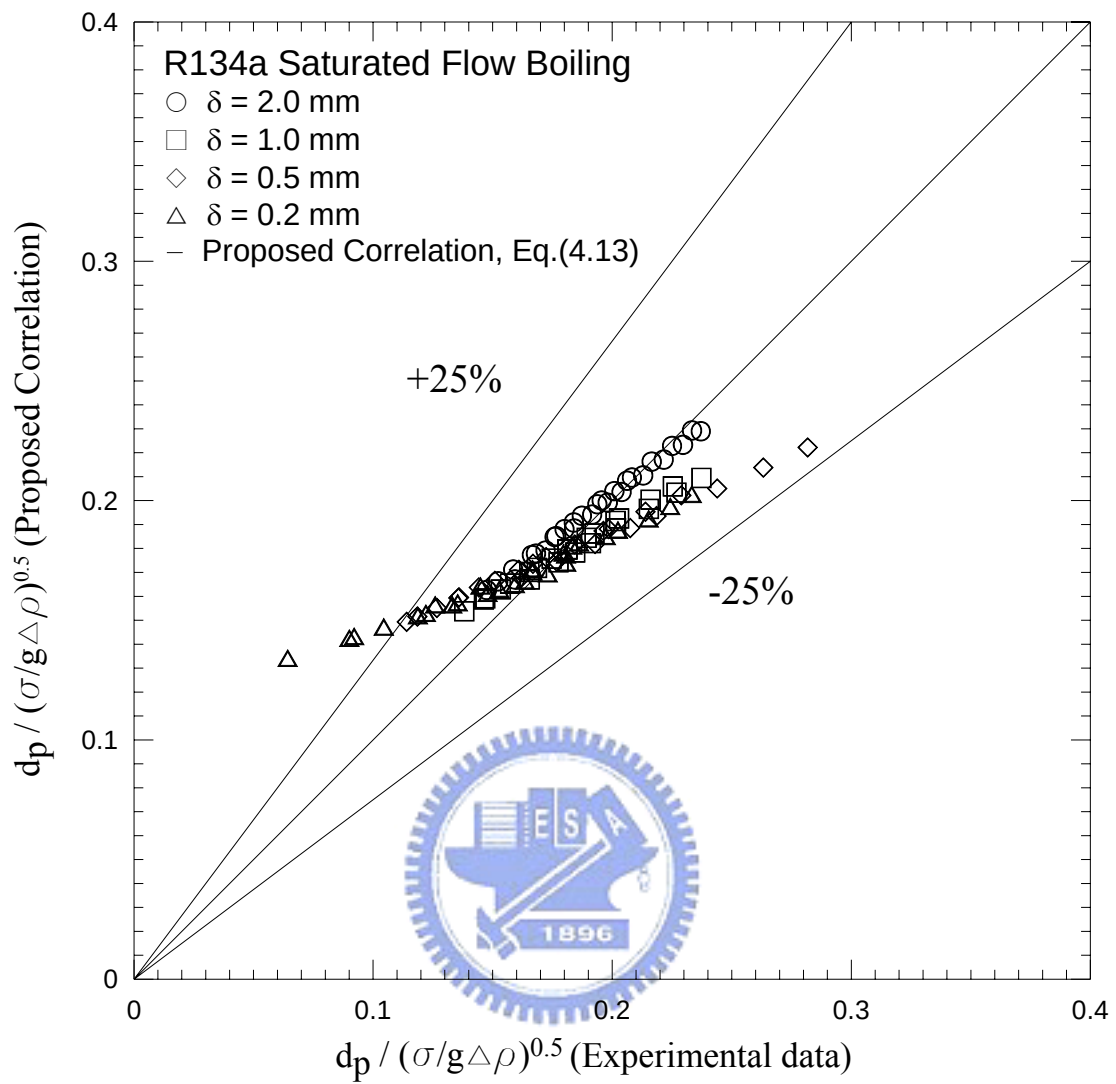


Fig. 4.38 Comparison of the measured data for mean bubble departure diameter in the saturated flow boiling of R-134a with the proposed correlation.

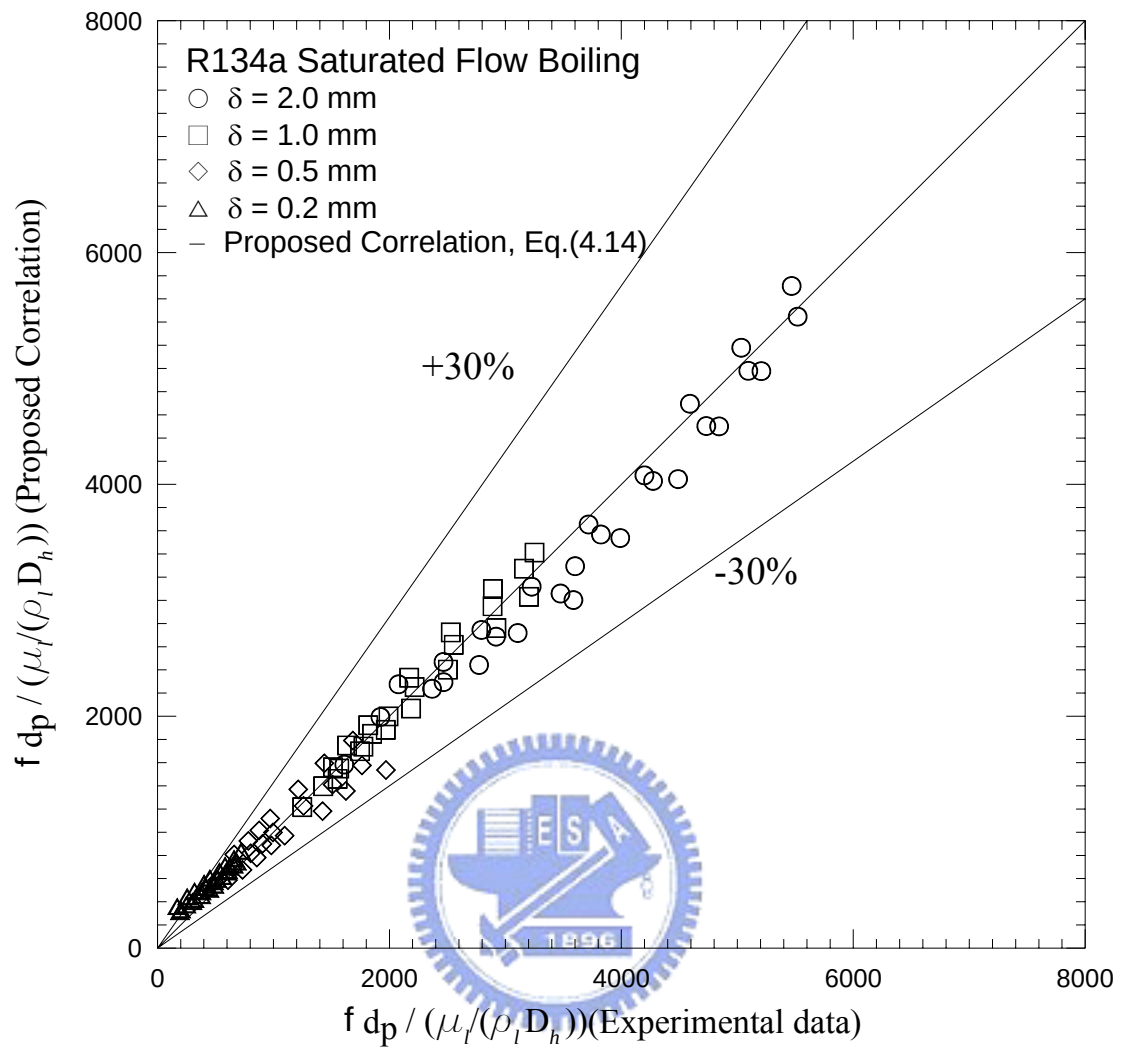


Fig. 4.39 Comparison of the measured data for mean bubble departure frequency in the saturated flow boiling of R-134a with the proposed correlation.

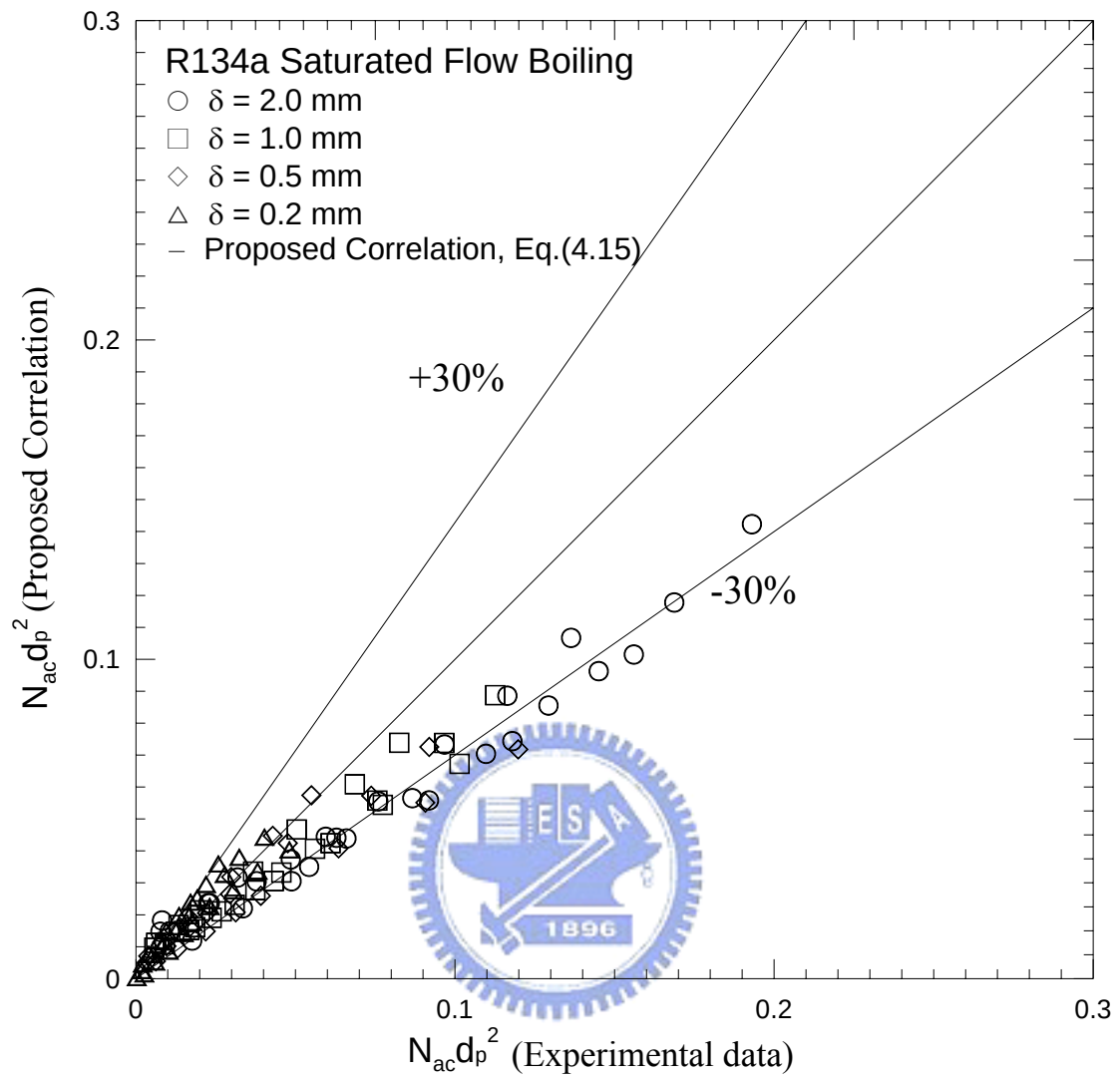


Fig. 4.40 Comparison of the measured data for mean active nucleation site density in the saturated flow boiling of R-134a with the proposed correlation.

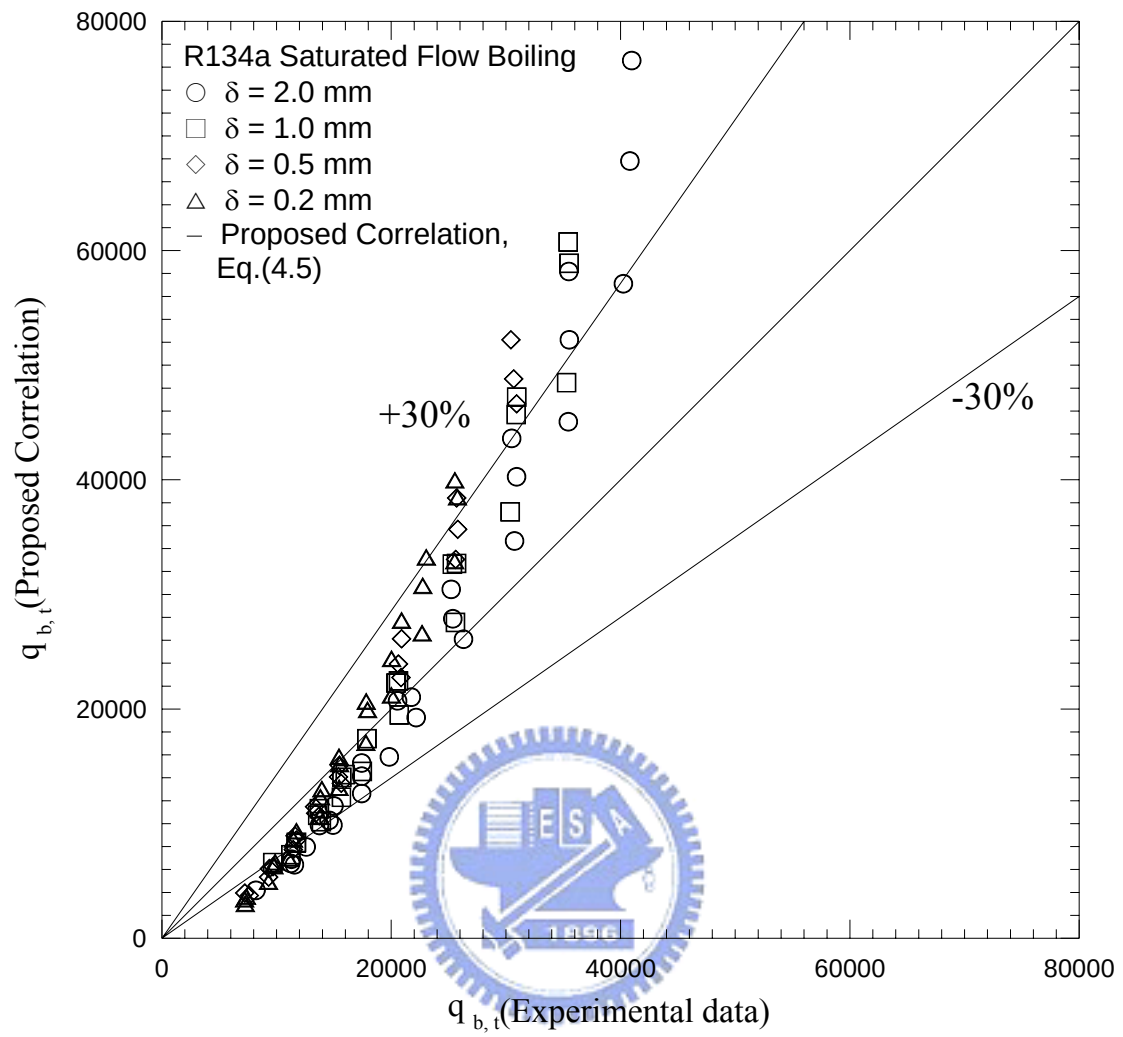


Fig. 4.41 Comparison of the measured data for heat transfer coefficient in the saturated flow boiling of R-134a in the bubbly flow regime with the proposed correlation.

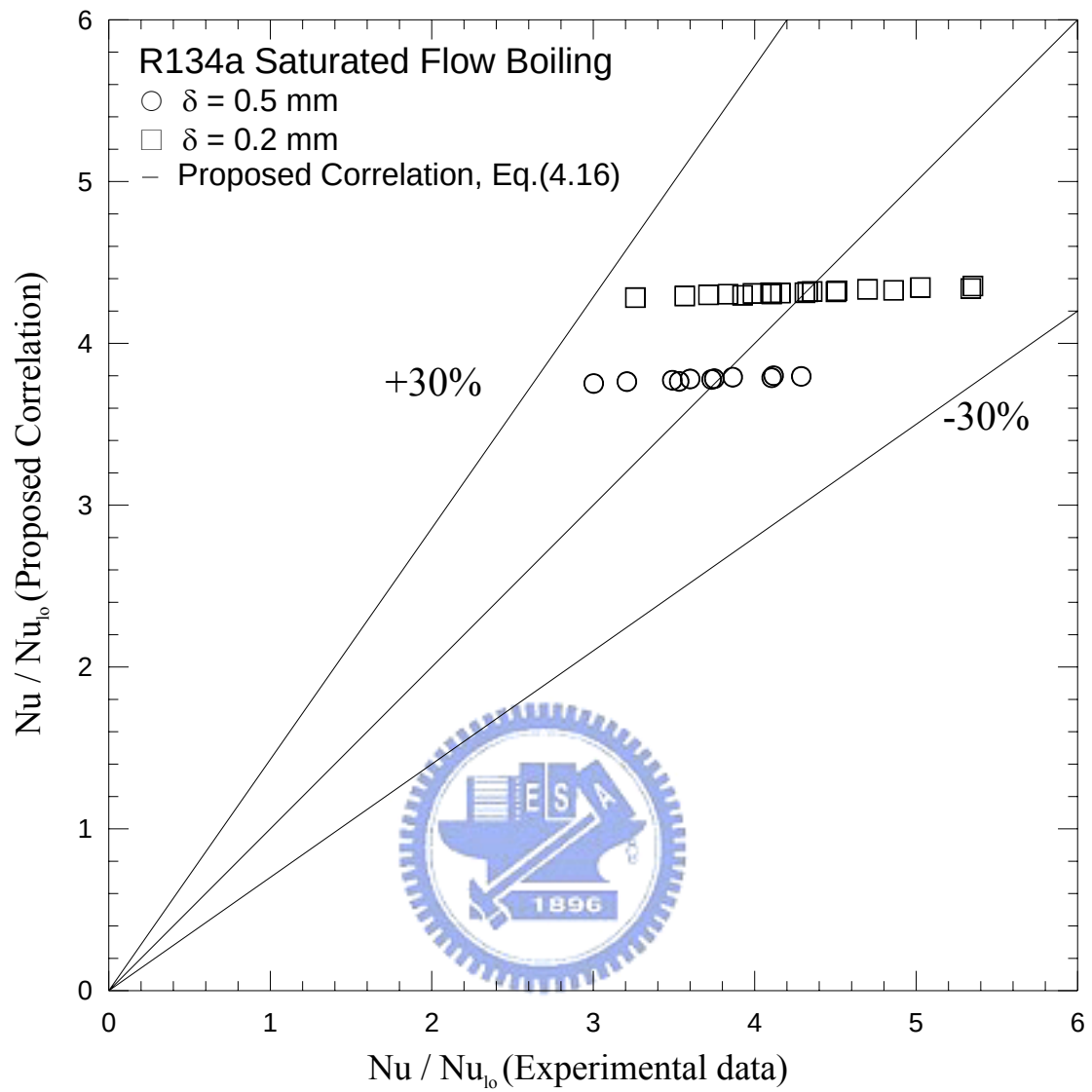


Fig. 4.42 Comparison of the measured data for heat transfer coefficient in the saturated flow boiling of R-134a in the slug flow regime with the proposed correlation.