This article was downloaded by: [National Chiao Tung University 國立交通大學] On: 28 April 2014, At: 06:42 Publisher: Taylor & Francis Informa Ltd Registered in England and Wales Registered Number: 1072954 Registered office: Mortimer House, 37-41 Mortimer Street, London W1T 3JH, UK



# **Molecular Crystals and Liquid Crystals Science and Technology. Section A. Molecular Crystals and Liquid Crystals**

Publication details, including instructions for authors and subscription information: <http://www.tandfonline.com/loi/gmcl19>

# **In-Line Fiber Polarization Selector and Intensity Modulator**

Tien-Kjng Chen  $^{\rm a}$  , Jer-MIng Hsu  $^{\rm a}$  b & Shu-Hsia Chen  $^{\rm a}$  b

<sup>a</sup> Department of Electronics, Chienhsin College of Technology & Commerce, Chungli, Taiwan, 320, R. O. C.

**b** Institute of Electro-optical Engineering, National Chiao Tung University, Hsinchu, Taiwan, 300, R. O. C.

Published online: 04 Oct 2006.

**To cite this article:** Tien-Kjng Chen , Jer-Mlng Hsu & Shu-Hsia Chen (1997) In-Line Fiber Polarization Selector and Intensity Modulator, Molecular Crystals and Liquid Crystals Science and Technology. Section A. Molecular Crystals and Liquid Crystals, 304:1, 415-421, DOI: [10.1080/10587259708046990](http://www.tandfonline.com/action/showCitFormats?doi=10.1080/10587259708046990)

**To link to this article:** <http://dx.doi.org/10.1080/10587259708046990>

# PLEASE SCROLL DOWN FOR ARTICLE

Taylor & Francis makes every effort to ensure the accuracy of all the information (the "Content") contained in the publications on our platform. However, Taylor & Francis, our agents, and our licensors make no representations or warranties whatsoever as to the accuracy, completeness, or suitability for any purpose of the Content. Any opinions and views expressed in this publication are the opinions and views of the authors, and are not the views of or endorsed by Taylor & Francis. The accuracy of the Content should not be relied upon and should be independently verified with primary sources of information. Taylor and Francis shall not be liable for any losses, actions, claims, proceedings, demands, costs, expenses, damages, and other liabilities whatsoever or howsoever caused arising directly or indirectly in connection with, in relation to or arising out of the use of the Content.

This article may be used for research, teaching, and private study purposes. Any substantial or systematic reproduction, redistribution, reselling, loan, sub-licensing, systematic supply, or distribution in any form to anyone is expressly forbidden. Terms & Conditions of access and use can be found at [http://](http://www.tandfonline.com/page/terms-and-conditions) [www.tandfonline.com/page/terms-and-conditions](http://www.tandfonline.com/page/terms-and-conditions)

*Mol. Cryst. Liq. Cryst.*, 1997, Vol. 304, pp. 415-421 **Reprints available directly** from **the publisher Photocopying permitted by license only** 

*0* **1997 OPA (Overseas Publishers Association) Amsterdam** B.V. **Published in The Netherlands under license by Gordon and Breach Science Publishers Printed in India** 

IN-LINE FIBER POLARIZATION SELECTOR *AND* INTENSITY MODULATOR

TIEN-JUNG CHEN, JER-MING HSU', and SHU-HSIA CHEN' Department of Electronics, Chienhsin College of Technology & Commerce, Chungli, Taiwan **320,** R. 0. C. \*Institute of Electro-optical Engineering, National Chiao Tung University, Hsinchu,

Taiwan 300, R. *0.* C.

Abstract Liquid-crystal-based fiber components that exploit the high birefringence and electrooptic effect of liquid crystals, are versatile. A single-mode fiber enclosed with planar-aligned liquid crystals is reported on in this paper. The fiber was etched nearly to its core. The output light was exercised through the evanescent field coupling between the fiber and surrounding liquid crystals. To achieve an effective access to the evanescent field, the etch depth was studied first. When the fiber was etched to 10-µm diameter, obvious light leakage occurred. Once the electric field was switched on, the polarization selection and intensity modulation were examined. A theoretical description of the optical characteristics were also given.

#### **INTRODUCTION**

In-line fiber components are attractive owing to their mechanical stability, low insertion loss, and miniature size. Such fiber components realized by combining optical fibers and liquid crystals have the great advantage of easy handling because of the fluid properties of liquid crystals. Moreover, the large electrooptic effect and high birefringence of liquid crystals can be exploited to modulate the optical intensity or select polarization states by applying external electric fields

Liquid-crystal-based fiber components are fabricated in a variety of ways. The most often used being the evanescent-field technique, which is based on the interaction between a guided-mode evanescent field and liquid crystals. Access to the guided-mode evanescent field can be achieved by either polishing or etching the cladding and then overlaying liquid crystals. Most in-line components made this way use side-treated fibers They can function as polarizers or modulators.<sup>1-4</sup>

In this report, a single-mode fiber was symmetrically etched to very nearly the surface of the core and enclosed with planar-aligned liquid crystals. The wave propagation behavior in this device configuration depends on the etch depth of the fiber and refractive indices of the liquid crystals. An appropriate etch depth was chosen to effectively

# **41 6/[2294] T.-J.** CHEN *rt ~l*

approach the evanescent field. When an electric field was applied to the liquid crystals, the response of the lightwave propagation to liquid crystals' refractive indices was altered. Thereby optical polarization and intensity were exercised.

### LIC)UID-CRYSTAI,-CLAD FIBER

**A** schematic view of the liquid-crystal-clad fiber is shown in Figure I(a)(b). **A** strand of 633-nm single-mode fiber, with a core diameter (2a) of 3.8  $\mu$ m and a cladding diameter of 125 **pm,** was stripped from its jacket and immersed in hydrofluoric acid (48% *HF)* to remove the cladding. One 3-cm-long section of the cladding was etched off to leave its diameter (2b) in the range of 6-12  $\mu$ m and was sandwiched between two ITO-coated glass



FIGURE I cross-sectional view (c) perpendicular-aligned liquid crystals The geometry of a liquid-crystal-clad fiber: (a) top view (b) side

slides with a spacing of 125  $\mu$ m. The liquid crystal was then inserted by capillary action. The liquid crystal used was nematic mixture 14616 obtained from Merck. The NLC used exhibited a nematic phase between 10 and  $50^{\circ}$ C over which the ordinary refractive index always remained lower than that of fused silica. The extraordinary index  $(n_e)$  and ordinary index ( $n_0$ ) are given as 1.498 and 1.452, respectively, operating at a wavelength of 633 nm and a temperature of  $25^{\circ}$ C. Whereas the fiber had a core index ( $n_{\text{co}}$ ) of 1.462 and a cladding index  $(n_{\text{cl}})$  of 1.458

In order to effectively approach the evanescent field. **we** conducted qualitative study of the effect of residual cladding thickness on lightwave propagation The liquid crystal was perpendicularly aligned in the sample, as shown in Figure l(c), where the glass slidc and etched section were coated with DMOAP (N, N-dimethyl-N-octadecyl-3-

aminopropyltrimethoxysilyl chloride). The evanescent field in the LC, which "sees" the LC's extraordinary index  $n_e$ , greater than the core index  $n_e$ , leaked out. This allowed us to observe the effect of cladding thickness on access to the evanescent field. For  $b=6 \mu m$ , the light leakage during propagation through the etched section of the fiber sample was not clear, while for  $b=5 \mu m$ , the light obviously leaked out in the etched section, but output at the fiber end continued. For  $b=3 \mu m$ , the light propagation decayed dramatically and disappeared completely from the output end. The observed results are shown in Figure **2.** The radiation formed a conic fan with an angle of about **24** degrees obeying Snell's law.



FIGURE *2* The effect of residual cladding thickness on lightwave propagation (a) For  $b=5 \mu m$ , the light leaked out in propagating through the etched section of the fiber, but output from the fiber end continued. (b) For  $b=3$   $\mu$ m, the light decayed dramatically and disappeared completely from the output. (See Color Plate XVIII).

# EXPERIMENTAL SETUP

The geometry in Figure  $3(a)$  was used to investigate the electrooptic properties of liquidcrystal-clad fiber. In order to study the electrooptic effect of the fiber sample, the liquid crystal molecules were planar-aligned in the axial direction This was achieved by coating **PVA** on the ITO-coated glass slides and rubbing their surfaces in the axial direction, as shown in Figure  $3(b)$ . The fiber had an etched section with  $10$ - $\mu$ m diameter of residual cladding. *An* ac electric field of 110 volt at 60 Hz was applied to the sample. **A** polarized He-Ne laser beam with a wavelength of 633 nm was passed through the halfwave plate to



FIGURE **3**  aligned liquid-crystal-clad fiber sample: side view Schematic drawing of (a) experimental setup and (b) the planar-

**vary** the input light polarization and then focused into the fiber by a **20x** microscopic objective; input power was *5* **mW.** The output light was examined using an analyzer and measured with a photodiode.

### POLARIZATION SELECTION **AND** INTENSITY MODIJLATION

# Theoretical Description

Figure 4 shows the liquid crystal molecules' orientations when the electric field was switched off and on, and the corresponding refractive index profiles. **A** theoretical consideration of optical characteristics used the calculation for W-type fibers. For xpolarized light, there is a guided solution, denoted as  $\text{HE}_{x}$  mode. Its propagation constant **satisfies** the following equation '

$$
\left[\frac{uJ_1(ua)}{J_0(ua)} + \frac{wl_1(wa)}{I_0(wa)}\right] \frac{wK_1(wb) K_0(vb)}{K_0(wa) J_0(ua)} - \frac{K_0(wb) vK_1(vb)}{K_0(wa) J_0(ua)} \n+ \left[\frac{uJ_1(ua)}{J_0(ua)} - \frac{wK_1(wa)}{K_0(wa)}\right] \frac{wl_1(wb) K_0(vb)}{I_0(wa) J_0(ua)} + \frac{I_0(wb) vK_1(vb)}{I_0(wa) J_0(ua)} = 0,
$$
\n(1)

where  $u = (n_{co}^{2}k^{2} - \beta^{2})^{1/2}$ ,  $w = (\beta^{2} - n_{cl}^{2}k^{2})^{1/2}$ , and  $v = (\beta^{2} - n_{o}^{2}k^{2})^{1/2}$ ;  $J_{m}$ ,  $I_{m}$ ,  $K_{m}$ are the Bessel and modified Bessel functions of the mth order. The k is the free-space propagation constant and  $\beta$  is the propagation constant in the fiber. As for the y-polarized light, there is a leaky solution when the voltage **is** switched on The solution is denoted as  $HE<sub>v</sub>$  mode and has the following characteristic equation:

$$
\left[\frac{uJ_1(ua)}{J_0(ua)} + \frac{wI_1(wa)}{I_0(wa)}\right] \frac{wK_1(wb)}{K_0(wa)} \frac{H_0^{(2)}(v'b)}{J_0(ua)} - \frac{K_0(wb)}{K_0(wa)} \frac{v'H_1^{(2)}(v'b)}{J_0(ua)}\n+ \left[\frac{uJ_1(ua)}{J_0(ua)} - \frac{wK_1(wa)}{K_0(wa)}\right] \frac{wI_1(wb)}{I_0(wa)} \frac{H_0^{(2)}(v'b)}{J_0(ua)} + \frac{I_0(wb)}{I_0(wa)} \frac{v'H_1^{(2)}(v'b)}{J_0(ua)}\n\right] = 0,
$$
\n(2)

where  $v' = (n_e^2 k^2 - \beta^2)^{1/2}$ ;  $H_m^{(2)}$  is the mth-order Hankel function of the second kind



FIGURE 4 refractive index profiles without (a) and with (b) an applied voltage. The orientations of liquid crystal molecules and the corresponding

We used the following parameters to calculate Equations (1)(2):  $n_{co} = 1.462$ ,  $n_{cl} = 1.458$ ,  $n_e = 1.498$ ,  $n_o = 1.452$ ,  $a = 1.9$   $\mu$ m, and  $\lambda = 633$  nm. A decay constant is defined as  $\alpha = -2\beta_i$ , where  $\beta_i$  is the imaginary part of  $\beta$ . The decay constant versus residual cladding radius b is shown in Figure **5.** Without an electric voltage, both HE, and  $HE_y$ , modes are guided. When the voltage is switched on, the  $HE_x$  mode is guided with zero decay constant, while the  $HE<sub>v</sub>$  mode becomes leaky. The cladding thickness **420/[2298] T.-J. CHEN** *era/.* 

plays an important role because  $\alpha$  for the HE<sub>y</sub> mode increases dramatically as the cladding radius b is reduced. For b= 5  $\mu$ m,  $\alpha = 1.902$  cm<sup>-1</sup> and the output attenuation are proportional to  $e^{-\alpha l} \sim 10^{-3}$ , where  $l = 3$  cm.



FIGURE *5*  radius b. The calculated results of the decay constant  $\alpha$  vs. residual cladding

## Experimental Results

The experimental output variations in x-polarized and y-polarized lights with an electric field applied are shown in Figure  $6(a)$ . When the voltage was switched on, the x-polarized light continued propagating, but the y-polarized light was attenuated. **As** the applied voltage was raised, the attenuation became more severe. This demonstrates the electrically-controlled polarization selectivity of the fiber sample.

Figure 6(b) shows the modulation of output light and its y-polarized component when an ac voltage of 110 volts was switched on and off manually over a time duration of 2 sec. for each state The optical output was out of phase with the electric input. The optical rise time is not dependent on voltage but is relative to the liquid crystal molecular relaxation response, which is determined by the elastic constants, viscosity coefficient of the liquid crystal and sample thickness. Whereas the optical decay time decreases with voltage increases and thinner samples produce faster decays. In the case of an applied voltage of 110 volt and a sample thickness of 125  $\mu$ m, the decay time constant is of the order 100 msec, while the rise time is about 15 sec. Moreover, the described modulation is obviously polarization-dependent This can be used to polarize light instantaneously along





FIGURE **6**  modulation of output light and its y-polarized component. (a) Optical polarization selection with an applied electric field and (b)

the direction for which modulation occurs. This may be important in polarizationpreserved fiber systems.

### **DISCUSSTONS AND CONCLUSIONS**

We have reported a new type of fiber-optic polarizer made of liquid-crystal-clad singlemode fiber. The key feature is the symmetrically etched fiber and planar-aligned nematic liquid crystal. The evanescent field was effectively approached with a proper cladding thickness, which can be determined by observing when light leakage occurs. Basically, the optical polarization selection and intensity modulation are based on the birefringence of liquid crystal. Therefore, the modulation is polarization-dependent. Moreover, the modulation frequency is limited by the relaxation time constant of the liquid crystal.

#### **REFERENCES**

- 1. K. Liu, W. V. Sorin, and H. J. Shaw, Opt. Lett., 11, 180 (1986).
- **2. T.** Hosaka, **K.** Okamoto, and T. Edahiro. Opt. lett.. 8, **124** (1983).
- **3. Z. K.** Ioannidis, I. P. Giles, and C. Bowry, Electron. Lett., *2,* **1453 (1988)**
- **4. Z.** K. Ioannidis, **I.** P. Giles, and **C.** Bowry, **Aod.** Opt., *2,* **328 (1991).**
- **5. M.** Monerie, IEEE J. Ouantuin Electron., **OE-18, 535** (1982).