行政院國家科學委員會專題研究計畫 期中進度報告

子計畫四:OFDM FFT 架構下軟體無線電訊號處理之軟、硬體

輔成設計及其數位通信之應用設計(2/3)

<u>計畫類別:</u>整合型計畫 <u>計畫編號:</u>NSC92-2220-E-009-021-<u>執行期間:</u>92年08月01日至93年07月31日 <u>執行單位:</u>國立交通大學電子工程研究所

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報告類型: 完整報告

<u>報告附件</u>:出席國際會議研究心得報告及發表論文 處理方式:本計畫可公開查詢

中 華 民 國 93 年 6 月 1 日

行政院國家科學委員會補助專題研究計畫

期中進度報告

用於軟體無線電基頻處理之系統晶片設計技術-子計畫四: OFDM FFT 架構下軟體無線電訊號處理之軟、硬體輔成設計及

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計畫類別: 個別型計畫 整合型計畫 計畫編號:NSC 92 - 2220 - E - 009 - 021 -執行期間: 92 年 8 月 1 日至 93 年 7 月 31 日

計畫主持人:陳紹基

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成果報告類型(依經費核定清單規定繳交): 精簡報告 完整報告

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摘要

在這個計劃期中報告中已經得到了五個進展成果。第一個部分是關於可變長度的快速 傅利葉轉換處理器所使用的資料位址產生器設計;另一方面,對於傅利葉轉換中所需要的 旋轉因數指標產生器亦是可變長度快速傅利葉轉換處理器中的重要設計,在這裡共有二個 用於固定基數演算法與一個用於分裂基數演算法的旋轉因數指標產生器設計將會在第二部 分提出。為了減少儲存旋轉因數所佔用的硬體成本,第三部份會介紹一個以遞迴方程式來 產生正弦與餘弦函數的旋轉因數產生器設計。第四部份是一個範例性質的可變長度快速傅 利葉轉換處理器整合實作。最後一部份是一個結合 DCT 技術設計出之一新的高效能之 OFDM 通道估測演算法。

Abstract

There are five intermediate results generated so far from our on-going project. All results are targeted on the FFT processor design for the modulation and demodulation of OFDM-based communication systems including DAB, DVB, 802.11a, 802.16 and VDSL systems. The results are: (1) a data address generator designed for memory-based, variable-length FFT processor; (2) three new architectures for coefficient index generation, which can work efficiently with the mentioned variable-length data address generator, where the first two are for fixed-radix FFT algorithms and the third one is for split-radix 2/4 FFT algorithm; (3) a new coefficient generator which can replace conventional high-cost coefficient ROM; (4) a variable-length FFT processor which integrates the advance technologies is proposed in part 4; (5) a high-performance DCT-based channel estimation algorithm for non-sample spaced channel impulse response.

關鍵字:快速傅利葉轉換、位址產生器、係數產生器、正交分頻多工、數位聲訊廣播、數 位視訊廣播。

Keyword: FFT, Address generator, Coefficient generator, OFDM, DAB, DVB.

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1. Introduction and Project Goals

本子計劃主要在於研究多標準之正交分頻調變技術(OFDM)軟體無線電(software defined radio) FFT/IFFT 演算法及架構之設計,考慮其整合性、低功率、快速計算、超大型 積體電路設計實現及其在數位通信之應用設計,特別是數位聲訊廣播(DAB)。FFT/IFFT運 算為正交分頻調變技術(OFDM) 之核心運算,而 OFDM 為 DAB、DVB、802.11a、 HyperLAN、802.16 等寬頻技術之調變方式。OFDM 也被視為未來 3G 之後之主要之無線通 信技術,而在有線寬頻之非對稱性數位用戶迴路通信技術(ADSL)亦利用相近技術,這兩種 數位通信技術均被視為現在及未來寬頻上網通信之主流技術,有鑑於此多標準、寬頻之廣 大應用及需求,本研究特別著重於多標準之相關於 FFT 信號處理之軟硬體整合設計如: FFT/IFFT 設計。本計劃將為三年之多年計劃,第一年將著重於現有及未來 OFDM 傳輸理 論 相關應用如 DAR DVR 802.11a HyperLAN ADSL 標準之研究及 software defined radio 理論研究,同時也將探討低功率、低複雜度、高速度 FFT/IFFT 演算法之研究及設計,此 外其它相關於 FFT 之數位通信應用也將作整體性之探討,如頻域適應性等化、回音消除濾 波器理論與技術,並訂定出 FFT/IFFT 模組之設計規格,此規格將考慮到多標準、多模式 軟體無線電 FFT/IFFT 核心模組整合設計。為了配合總計劃及第二子計劃, DAB FFT/IFFT 模組之設計實現亦為主要考量。第二年除了繼續及改善第一年的研究外,將設計出適用數 位信通信應用、及多標準之之 FFT/IFFT 架構及電路模組,特別是應用於 DAB OFDM,除 了設計出軟智慧財外(soft IP), 我們也將作模組之 FPGA 實現以驗證設計之正確性,若時 間許可則將 FFT/IFFT 模組委託晶片廠實現之並作驗證。第三年除了繼續及改善第二年之 研究外將開始與其他模組作整合設計及驗證,基本之整合系統仍將以 FPGA 實現為主,但 同時也將實作改進版之 FFT/IFFT 模組晶片實現。

2. Discussion and Results

2.1 Variable-length FFT Processor

In order to realize multi-mode and multi-standard OFDM communication systems, the FFT processor must support length-independent computation and meet the worst-case hardware requirement. Consequently, the FFT processor design must contains an efficient processing element, a variable-length data address generator and a variable-length twiddle factor generator.

2.1.1 Variable-length Data Address Generator

In in-place memory-based FFT processor design, data address generator is decided by the order of butterfly operations. A conventional processing order and control scheme for radix-2 FFT are proposed by Cohen (1976) [1], and the algorithm was then extended and generalized by [2], [3], [4], [5]. However, we can find out that Cohen's scheme is not suitable for a variable-length FFT when analyzing a sub-segment of signal flow graph for a shorter-length FFT. To give an example of 16-point radix-2 DIF FFT operation, the direct-order scheme processes butterflies from top to down and from left stage to right stage as marked by the numbers on the right-hand sides of ellipses in Fig. 2.1. On the other hand, since the main idea of Cohen's processing order is grouping butterflies associated with the same twiddle factor together to reduce signal switching frequency of the coefficient circuits, it results in decimation in butterfly (DIB) order as marked by the numbers on the left-hand sides of ellipses in Fig. 2.1.

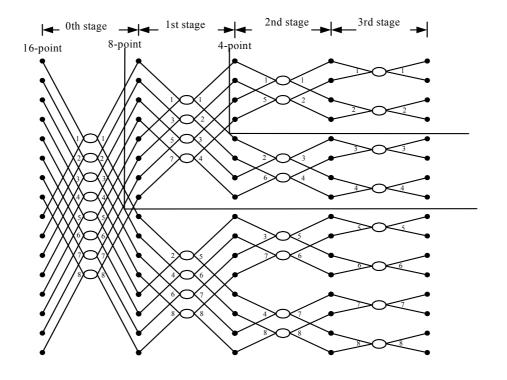


Fig. 2.1 DIF butterfly processing sequence for fixed-length and variable-length memory based FFT processors

	BF 0	BF 1	BF 2	BF 3	BF 4	BF 5	BF 6	BF 7
Stage 1	<0, 8>	<1,9>	<2, 10>	<3, 11>	<4, 12>	<5, 13>	<6, 14>	<7, 15>
Stage 2	<0,4>	<1, 5>	<2, 6>	<3, 7>	<8, 12>	<9, 13>	<10, 14>	<11, 15>
Stage 3	<0, 2>	<1, 3>	<4,6>	<5,7>	<8, 10>	<9, 11>	<12, 14>	<13, 15>
Stage 4	<0, 1>	<2, 3>	<4, 5>	<6, 7>	<8,9>	<10, 11>	<12, 13>	<14, 15>

Table 2.1 Data addresses needed for butterfly PE in direct processing order.

	BF 0	BF 1	BF 2	BF 3	BF 4	BF 5	BF 6	BF 7
Stage 1	<0, 8>	<1,9>	<2, 10>	<3, 11>	<4,12>	<5, 13>	<6, 14>	<7, 15>
Stage 2	<0, 4>	<8, 12>	<1, 5>	<9, 13>	<2, 6>	<10, 14>	<3, 7>	<11, 15>
Stage 3	<0, 2>	<4, 6>	<8, 10>	<12, 14>	<1, 3>	<5, 7>	<9, 11>	<13, 15>
Stage 4	<0, 1>	<2, 3>	<4, 5>	<6, 7>	<8,9>	<10, 11>	<12, 13>	<14, 15>

Table 2.2 data address pairs for butterfly PE in Cohen's scheme.

In Fig 2.1, when we isolate the sub-SFG of a shorter-length FFT from the longer SFG, the Cohen's butterfly order is unmatchable with the variable-length FFT design concept. On the contrary, the direct processing order is suited to the varied FFT lengths, and therefore the architecture of Cohen's data address generator has to be modified to deal with the operations of different lengths FFT.

In the example shown above, the data addresses needed for butterfly PE in direct processing order and in Cohen's processing order are listed in Table 2.1 and Table 2.2 respectively. In the table, $\langle s, t \rangle$ denotes data address pair for both input and output data for radix-2 butterfly PE, and *s* and *t* are indices of one dimension memory array. Note that the address translation and mapping from one dimension index to multi-bank memory system are considered later.

Data address pair $\langle s, t \rangle$ needed for the i-th butterfly of the k-th stage in Cohen's scheme can be described as (2.1), while the operator ROTATE_n(X, m) circularly rotates X right by m bits within n bits.

$$n = \log_2 N$$

$$s = ROTATE_n(i,k) , i = 0 \sim \frac{N}{2} - 1, \quad k = 0 \sim n - 1$$
(2.1)

$$t = ROTATE_n(i + \frac{N}{2}, k)$$

To realize equation (2.1), Cohen proposed the efficient address generator architecture as shown in Fig. 2.2. The main idea is appending 0 and 1 to MSB of the content of butterfly counter then using barrel shifters to realize the rotation.

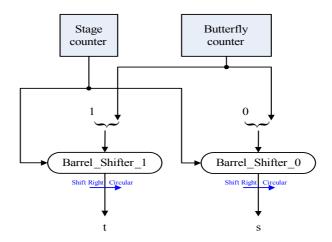


Fig. 2.2 Data address generator for radix-2 FFT in Cohen's scheme

We can modify Cohen's DIB-ordered addressing scheme to direct ordered addressing scheme to suit with variable-length FFT design. The data address pair $\langle s, t \rangle$ can be described as the following equation (2.2) composed of the contents of the butterfly counter and the stage counter.

$$s = \{i_{\log(N)-2}, i_{\log(N)-3}, ..., i_{k-1}, 0, i_{k-2}, i_{k-3}, ..., i_1, i_0\}$$

$$t = \{i_{\log(N)-2}, i_{\log(N)-3}, ..., i_{k-1}, 1, i_{k-2}, i_{k-3}, ..., i_1, i_0\}$$

$$i = [i_{\log_2(N)-2}i_{\log_2(N)-3}i_2i_1i_0]_2 : \text{bit - wise butterfly counter content}$$

k : the stage counter content
N : the longest FFT length supported
(2.2)

Chang [6] proposed a variable-length data address generator, which was modified from Cohen's fixed-length data address generator. Chang's design includes an extra barrel shifter that rotates the content of butterfly counter circular left before bit appending operations and then rotates circular right followed by bit appending operations. This design not only alternates Cohen's scheme to direct butterfly operation order, but also adapts to varying FFT lengths. The block diagram is shown in Fig. 2.3.

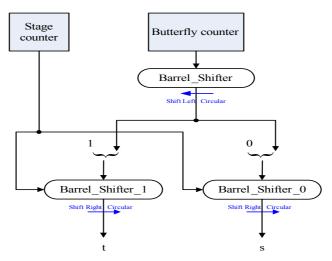


Fig. 2.3 Chang's variable-length data address generator.

In order to achieve high-performance variable-length FFT operations and data accesses, we propose the following data address generator. The design covers seven different FFT lengths including 64, 256, 512, 1024, 2048, 4096, and 8192 points, which cover all the required FFT lengths by 802.11a, 802.16a, DAB, DVB-T, VDSL and ADSL. Furthermore, the proposed data address generator significantly improves the address generator mentioned above, by considering radix-2² DIF FFT algorithm and variable-length FFT operations, and by simplifying the original area-consuming barrel-shifter based designs with simpler multiplexer-based addressing functions.

The four addresses required by radix-2² butterfly PE correspond to the 4 different banks. The addresses are denoted as <s, t, u, v> which can be calculated by the equation (2.3), where N is the longest FFT length supported, k is the stage counter content, and $i = [j_{\log_2(N)-2}j_{\log_2(N)-3} \dots j_2j_1 j_0]_2$ is butterfly counter content.

$$s = [j_{\log N-1} \ j_{\log N-2} \ \dots \ j_{\log N-K} \ 00 \ j_{\log N-K-1} \ j_{\log N-K-2} \ \dots \ j_1 \ j_0]_2$$

$$t = [j_{\log N-1} \ j_{\log N-2} \ \dots \ j_{\log N-K} \ 01 \ j_{\log N-K-1} \ j_{\log N-K-2} \ \dots \ j_1 \ j_0]_2$$

$$u = [j_{\log N-1} \ j_{\log N-2} \ \dots \ j_{\log N-K} \ 10 \ j_{\log N-K-1} \ j_{\log N-K-2} \ \dots \ j_1 \ j_0]_2$$

$$v = [j_{\log N-1} \ j_{\log N-2} \ \dots \ j_{\log N-K} \ 11 \ j_{\log N-K-1} \ j_{\log N-K-2} \ \dots \ j_1 \ j_0]_2$$

(2.3)

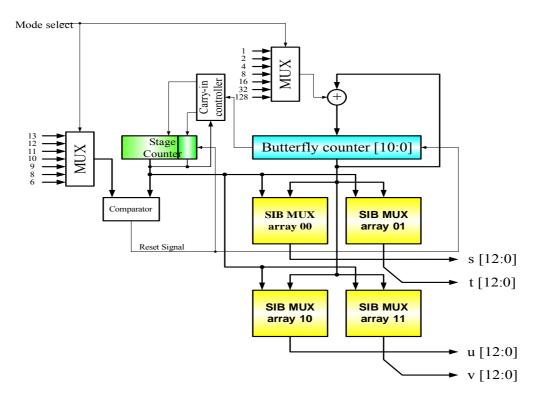


Fig. 2.4 Block diagram of the proposed variable-length data address generator

The hardware block diagram of variable-length data address generator is shown in Fig. 2.4. In the figure, "carry-in controller" adds the carry-out signal from butterfly counter to the LSB or its left immediate bit of the stage counter to alternate the counter step of the stage counter between one and two; "comparator" compares stage counter content with the maximum stage

count corresponding to each FFT length and reset all counters if they are equal; input signal "mode select" controls the butterfly counter step and maximum stage count to vary FFT length; "SIB MUX array" denotes shift-insertion-bypass multiplexer array. It greatly simplifies the address generator of Fig. 2.5 and Fig. 2.6, as will be detailed below.

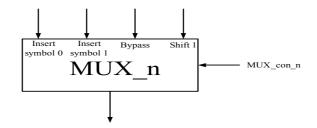


Fig. 2.5 Block diagram of MUX_n module

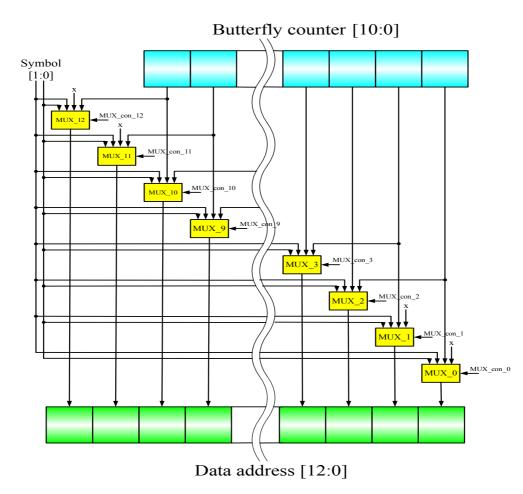


Fig. 2.6 The architecture of Shift-insert-bypass MUX array

In our design, we define several functions to simplify the design to replace those area-consuming barrel shifters with much simpler multiplexers. The functions include the required left shift operations, symbol bit insertion operations, and bypass the remaining bits, for the realization of the variable-length data address generation algorithm. Detailed architecture of the shift-bypass-insertion multiplexer array is shown in Fig. 2.6. In the figure, the input signal "symbol" to MUX_n module can be 00, 01, 10, or 11, where block diagram of MUX_n is shown in Fig. 2.5, and function of MUX n out-put is explained in Table 2.3. Timing and area

comparisons of data address generator between SIB-MUX array approach and barrel shifter approach are shown in Table 2.4, and the result is synthesized by TSMC 0.25µm standard cell library with Synopsis Design Analyzer.

	Table 2.5 Output functions of the MOA_II.				
Output	Function				
Insert symbol 0 (I0)	Select symbol bit 0 as the n-th bit of data address.				
Insert symbol 1 (I1)	Select symbol bit 1 as the n-th bit of data address.				
Bypass (BP)	Select the n-th bit of butterfly counter as the n-th bit of data address.				
Shift 2 (S2)	Select the (n-2)-th bit of butterfly counter as the n-th bit of data address.				

Table 2.3 Output functions of the MUX_n.

Table 2.4 Comparison of DAG units.

	SIB-MUX array	Barrel shifter (Fig.2.3)
No. of cells	143	229
Total gate counts	169	352
Path delay	5.72ns	7.14ns

2.1.2 Variable-length Coefficient Address Generator

The basic coefficient address generating function is mainly a counter with an adjustable counting step to realize varying stages and allow for varying FFT lengths. Hence, we can realize the coefficient address generator based on the content of the butterfly counter.

In fig. 2.7, we give an example of coefficient address generator which sustains 8192, 4096, and 1024-point FFT.

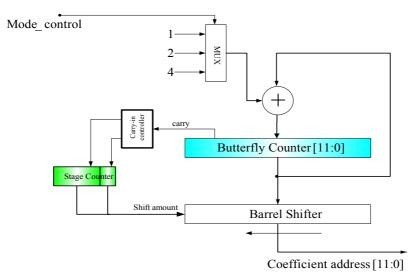


Fig. 2.7 The block diagram of variable-length coefficient index generator

2.1.3 Variable-length Processing Element

Although our design is based on radix-2² DIF FFT algorithm, we can still compute a general power-of-2 FFT by adding some minor modification to the radix-2² datapath. The unified radix-2²/2 datapath is shown in Fig. 2.8 and Fig. 2.9. In the fig. 2.8, the control line "select=0" programs the PE to as radix-2² mode so as to execute radix-2² algorithm, otherwise, in fig. 2.9, the four adders on the right hand side and the multiplier W_N^{2n} is bypassed so that the PE is configured as radix-2 mode such that two radix-2 butterflies are processed simultaneously. The "swap r/i" unit, that interchanges real part with imaginary part, is to implement the required multiplication with "-j". This shared hardware design does not increase the complexity of data address generator.

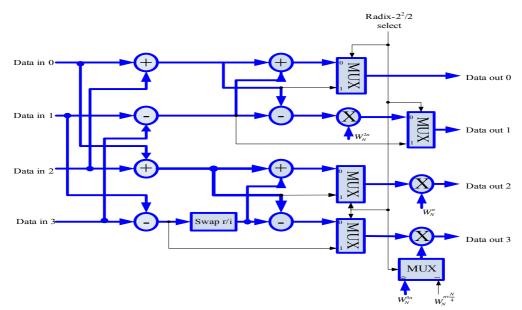


Fig. 2.8 The radix- 2^2 mode datapath of the PE

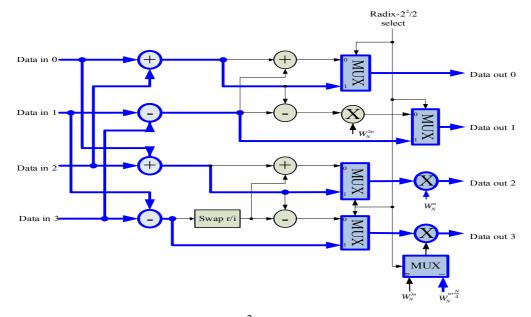


Fig. 2.9 The radix- 2^2 mode datapath of the PE

2.1.4 Variable-length Commutate Mode

The memory access bandwidth is the critical issue in memory-based FFT processor design.

An N-point memory-based FFT processor based on radix-r algorithm needs $\frac{N}{r}\log_r N$ PE

operations to transform one *N*-point symbol. Further, each PE operation needs 2r memory accesses to read data from memory and write back to it, so that each *N*-point symbol requires $2N \log_r N$ memory accesses. In order to handle this requirement, there are two solutions:

- 1. Use a higher-radix algorithm to reduce total memory accesses.
- 2. Increase memory access bandwidth by distributing memory accesses into several memory banks or multiple memory ports.

However, it is expense to increase the arithmetic complexity. Further, the number of memory ports is not controlled by architecture designer but cell library provider and device vendor, and the desirable case of the in-place design is simultaneously delivering r complex data from memory to radix-r butterfly PE and writing back r complex data from output ports of butterfly PE to the data memory. Therefore, the solution of memory access bandwidth is to partition memory into r banks, and than assign r input data for radix-r butterfly PE to proper memory banks for conflict-free memory access.

There are several efforts on memory partition and addressing methods to achieve conflict-free memory access [2], [3]. The general conflict-free memory partition scheme [2] that translates sequential data count into bank index and data index of each bank is shown in equation (2.4).

$$n = \lceil \log_{r} N \rceil$$

$$Data_count = [d_{n-1}d_{n-2}.....d_{2}d_{1}d_{0}]_{r}$$

$$Bank_index = (\sum_{t=0}^{n-1} d_{t}) \mod r$$

$$Data_index = [d_{n-1}d_{n-2}.....d_{2}d_{1}]_{r}$$

$$(2.4)$$

Similar result can also be found in Lo's scheme derived by *vertex coloring rule* [3]. For radix-*r* butterfly PE, this allocation algorithm can access *r* data from *r* different banks simultaneously at proper addresses according to the original data addresses. The original data address *data_count* can be generated according to the content of the butterfly counter and the stage counter of FFT processing. The data_index is the new address assigned to each memory bank.

The bank index generator of our design is shown in Fig. 2.10. The commutate modes of the commutator which supports the variable-length FFT mentioned above are shown in Table 2.5.

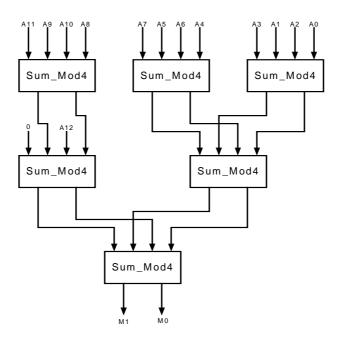
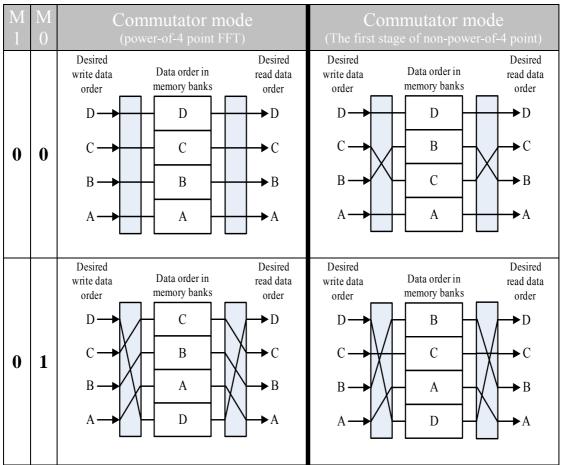
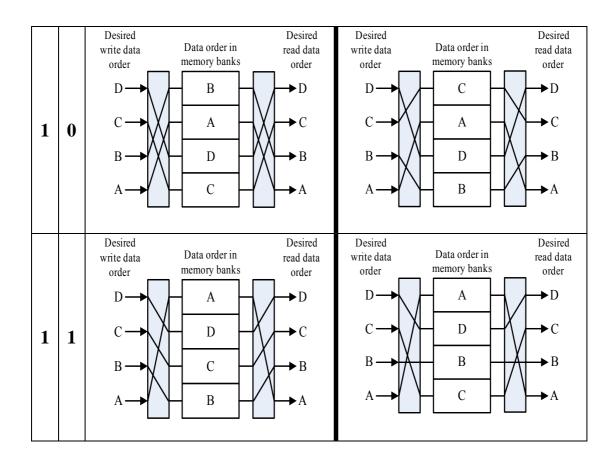


Fig. 2.10 Block diagram of bank index generator

Table 2.5 Four different commutator configuration linking desired data access port index to bank index of data.





2.1.5 The Proposed Variable-length FFT Processor Architecture

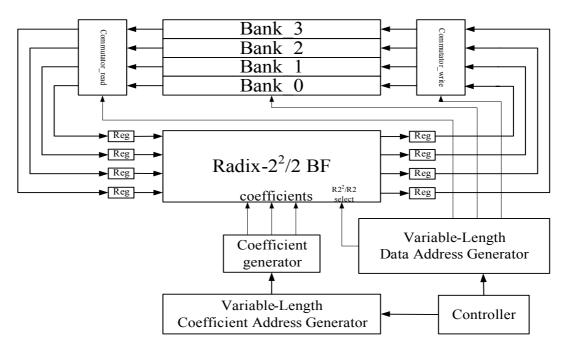


Fig. 2.11 Block diagram of the proposed FFT processor

A general memory-based FFT processor structure mainly consists of a PE, a main memory, ROM for twiddle factor storage, and a controller. The main memory stores processed data. The controller contains three functional units: data memory address generator, coefficient index generator, and operation state controller. The Butterfly PE is responsible for the butterfly operations required by FFT operations.

Inside the FFT processor, operation can be divided into three major parts: memory read, data processing, and memory write back. These three parts are isolated by two sets of register so that they can operate simultaneously and independently without conflict. The FFT operation diagram of our design example is shown in Fig. 2.12.

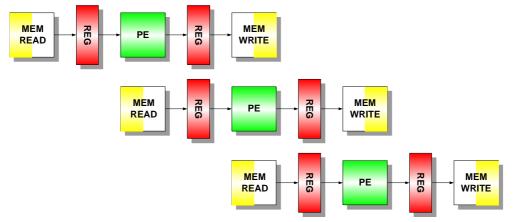


Fig. 2.12 Pipelined data path and shared devices of FFT processor

2.2 CORDIC-based Processing Element of FFT Processor

2.2.1 The CORDIC Algorithm and Architecture

In many FFT applications, the butterfly processing element (PE) often is realized with complex multipliers which have characteristics of high complexity and huge amount of area. Further, for the requirement of the twiddle factor multiplications, the twiddle factors must be stored in a look-up table which is generally implemented by ROM in advance. However, since long-length FFTs are commonly used in modern applications such as 8192-point FFT in DVB-T, the look-up table approach becomes inefficient because of enormous chip area cost. For example, even if we employ the symmetric property of the sinusoid function, the total ROM space requirement is 2*12*8192 / 8 = 24576(bits) ≈ 3 (KB) in an 8192-point FFT with 12-bit accuracy. For this reason, the CORDIC (Coordinate Rotation Digital Computer) algorithm is proposed here to substitute for conventional complex multiplier and look-up table approach.

The CORDIC algorithm developed by Volder [7] in 1959 is a generalized algorithm that can perform vectoring and rotation operations of a two dimensional vector. The rotation operation is to compute the target vector of the initial vector and the given rotation angle θ , while the intention of the vectoring operation is to compute the angle between the start vector and the end vector. Furthermore, there are three different kinds of coordinate systems: the linear coordinate system, the circular coordinate system, and the hyperbolic coordinate system. Walther [8] extend the algorithm to compute multiplication, division, and hyperbolic functions. The applications of CORDIC-based are 3-D graphic [9], [10], adaptive filter [11], floating point unit, DSP processor, and so on. When employing CORDIC algorithm to FFT PE, we only investigate the most popular circular coordinate system and the rotation mode operations. The basic theory of the CORDIC algorithm is reviewed as follows section.

The rotation operations are approached by a sequence of micro-rotations (elementary angles) using only shift-and-add operations, and therefore it is very suited for VLSI implementation and DSP applications. There have been numerous improved CORDIC algorithms and structures proposed ever since its introduction. Most of the CORDIC algorithms assume a constant scale factor for the ease of scale factor compensation. However, they have to rotate even when the residual rotation angles have converged [12], [13], [14], [15]. In some cases, they either have to do accurate but slow decision operations for rotation directions or do rough direction decisions at the expense of extra compensation operations [12], [13]. To speedup CORDIC operations, the following techniques are widely used: (1) use carry-free redundant addition scheme [12], [13], [16-19]; (2) fast decision of rotation directions with only a few most significant digits (MSDs) of the control parameters [12], [13], [16-19]; (3) skip unnecessary rotations; (4) effectively recode rotation angles for saving rotation iterations [20]; (5) apply radix-4 rotation schemes [17], [21], [22], [23], to reduce iteration numbers; and (6) predict the rotation sequence for parallel and pipelined processing.

Some of the mentioned techniques result in variable scale factors. Variable scale factors have the trouble of complicated scale factor computation followed by penalty compensation [18], [19]. Due to the considerable overhead generated by variable scale factor, most of the existing radix-4 CORDIC algorithms resort to constant scale factor approach [17], [22]. However, these constant-scale-factor CORDICs are basically hybrid radix-2 and radix-4 algorithms. As a result, their iteration numbers are not fully reduced. Recently, we proposed CORDIC algorithms with variable scale factors [21] skip unnecessary rotations and at the same time perform low-complexity on-line decompositions and compensations for the variable scale factors. Specifically, the radix-4 algorithm costs less iteration (including rotations and compensations) than the existing radix-4 algorithms. The radix-4 CORDIC algorithm proposed in [23] is similar to the one in [21], except the ways they handle variable scale factors. Both designs share the same low iteration number of 0.8n. Although the very high-radix CORDIC algorithm has an number, it is irregular realization which extremely small iteration in needs multiplication-and-accumulation circuits. Its efficiency is high dependent on practical circuit optimization.

To reduce the shift-and-add operations of both rotation iterations and scale factor compensations, we will present a new table lookup recoding scheme for rotation angles and variable scale factors. The new method can speedup both the convergence rates of the residual rotation angles and our fast variable scale factor decomposition and compensation algorithm [21]. For more reduction of iteration number, the new CORDIC algorithm also applies the leading-one bit detection operations to both residual rotation angles and decomposition of variable scale factors.

2.2.2 The New Angle Decomposition Scheme

For speeding up convergence, first we detect the leading-one (leading-zero) bit positions, for positive (negative) residual angle z_i , respectively, in the i-th iteration. This action can avoid unnecessary rotations required by conventional CORDIC algorithms. Then the most significant r bits (denoted as $z_{i,r}$), counted from the leading-one (or leading-zero) bit of z_i , are used to access δ_m and δ_n information from a table. These two retrieved parameters correspond to a combined rotation angle $\tan^{-1}2^{-m} + \tan^{-1}2^{-n}$ that best matches $z_{i,r}$ (in a least-square error sense), which makes $z_{i,r} - (\tan^{-1}2^{-m} + \tan^{-1}2^{-n})$ as close to zero as possible. This approach corresponds to the following iteration operation (2.5), and this iteration results in a variable scale factor described as the following equation (2.6).

$$\begin{cases} x'_{i+1} = x_i - 2^{-m_i} y_i \\ y'_{i+1} = y_i + 2^{-m_i} x_i \end{cases} \stackrel{=}{\Rightarrow} \begin{cases} x_{i+1} = x'_{i+1} - 2^{-n_i} y'_{i+1} \\ y_{i+1} = y'_{i+1} + 2^{-n_i} x'_{i+1} \end{cases}$$

$$\begin{cases} x_{i+1} = x_i (1 - 2^{-(m_i + n_i)}) - y_i (2^{-m_i} + 2^{-n_i}) \\ y_{i+1} = y_i (1 - 2^{-(m_i + n_i)}) + x_i (2^{-m_i} + 2^{-n_i}) \end{cases}$$

$$(2.5)$$

$$K = \prod_{i=1}^{l} \cos \theta_{m_i} \cos \theta_{n_i} = \prod_{i=1}^{l} \frac{1}{\sqrt{1 + 2^{-2m_i}}} \frac{1}{\sqrt{1 + 2^{-2n_i}}}$$
(2.6)

In generalization, we may include more than two δ_n 's to speedup the convergence rate. However, the computational complexity increases significantly, and therefore we only investigate the case of two combined direction parameters here. Similar techniques can be extended to the general case. Based on equation (2-5), some lookup tables for the residual rotation angles can be constructed by computer search with the closest match as mentioned before. In a sense, it approximately amounts to a radix-2^r CORDIC algorithm, by examining the MSB part $z_{i,r}$ of the residual rotation angle z_{i} . Since an optimal table depends on the iteration index i, it is better to have an optimized lookup table for each i. However, it will increase the table size accordingly. From easy Taylor expansion, we can get $\tan^{-1}2^{-i} \approx 2^{-i}$ when $i \ge 0$. Then, in computer simulations, we find that it is enough to have good results by using only two different tables, as shown below.

Here, we take r=4 bits (i.e., radix-2⁴) as a design example. Table 2.6 shows the stored optimized m and n of the δ_m and δ_n patterns, corresponding to the $z_{i,r}$ information. From Taylor's expansion of $\theta_k = tan^{-1}2^{-k}$, we find that the binary patterns of θ_0 and θ_1 are noticeably different from those of the θ_k 's, k>1. Therefore, two different tables are used for the cases of k= {0,1} and k>1, respectively, where k is the leading-one (or leading-zero) bit position of the residual rotation angle z_i .

Table	2.6 Recoung tabl	1	ition of residual rota	tion angle	
	Optimized patterns of m and n				
$\theta_i(2^{-k} \sim 2^{-k-3})$	k=(),1	k>1		
	m	n	m	n	
1000	k	k+3	k	k+4	
1001	k	k+2	k	k+3	
1010	k	k+2	k	k+2	
1011	k	k+1	k	k+1	
1100	k	k+1	k	k+1	
1101	Unused , for $\theta_0 = 0 \sim \pi/4$		k	k+1	
1110	Unused, for	$\theta_0 = 0 \sim \pi/4$	k-1	k+5	
1111	Unused, for	$\theta_0 = 0 \sim \pi/4$	k-1	k+3	

Table 2.6 Recoding table for the decomposition of residual rotation angle

2.2.3 Table reducing scheme

In above description of new angle encoding scheme, the given table size does not include the term n*p for {tan⁻¹2⁻ⁱ, i=0,1,2,...,n-1}, required by conventional CORDIC algorithms. We can find the equation (2.7) in Taylor expansion.

$$\tan^{-1} x = x - \frac{x^3}{(1+x^2)^2} + O(x^7)$$
, where $O(x^7)$ is the max error range (2.7)

i	$\tan^{-1}2^{-1}$ (radius)	tan ⁻¹ 2 ⁻ⁱ (degree)
1	0.463867 (001110110110 ₂)	$26.565051(110101001000_2)$
2	0.245117 (000111110110 ₂)	14.036243 (111000001001_2)
3	0.124512 (000011111111 ₂)	7.125016 (11100100000 ₂)
4	0.062500 (000010000000_2)	<i>3.576334 (111001001110₂)</i>
5	$0.031250(000001000000_2)$	1.789911 (011100101000 ₂)
6	$0.015625(00000100000_2)$	$0.895174(001110010100_2)$
7	$0.007813(00000010000_2)$	$0.447614(000111001010_2)$
8	$0.003906(00000001000_2)$	$0.223811(000011100101_2)$
9	$0.001953 (00000000100_2)$	0.111906 (000001110010 ₂)
10	0.000977 (00000000010_2)	0.055953 (000000111001 ₂)
11	$0.000488(0000000001_2)$	$0.027976(00000011100_2)$

Table 2.7 the table of $\tan^{-1}2^{-i}$ value for the 12-bit accuracy

In equation (2.7), if we need n bit output precision and $x = 2^{-i}$, we can ignore the second item when $i \ge n/3$. Then, we can get the tan⁻¹2⁻ⁱ value by shifting tan⁻¹2⁻⁽ⁱ⁻¹⁾. By the method, we only need n/3 words to store the angle tan⁻¹2⁻ⁱ, replacing the traditional n words. For instance, the terms of tan⁻¹2⁻ⁱ value which have be stored in ROM are 4 and 5 for radius and degree representation respectively.

2.2.4 On-line variable factor compensation

For low-complexity on-line variable scale factor compensation described by equation (2.6), here we further improve and speedup our previous efficient variable scale factor algorithm, by using a on-line variable factor compensation. The whole improved algorithm is detailed below.

Rewriting equation (2.6), K can be first transformed to

$$K_i = \frac{1}{\sqrt{1 + 2^{-2m_i}}} \frac{1}{\sqrt{1 + 2^{-2n_i}}}$$
(2.8)

The same in Taylor, we can find $K_i = (1-2^{-(2m+1)})(1-2^{-(2n+1)})+O(2^{-(4m+1)})$. From this expansion, the K_i will approximate to 1 when i > (n/2)-1. Therefore, we can get the most suitable scale factor compensation values when we get the rotation items δ_m and δ_n . And the compensation computation can also be calculated by shift-and-add operation. In every time scale factor compensation, we will have an error item $O(2^{-(4m+1)})$, when i < (n/4)-1. The error will be store and than be compensated just after the rotation operations i > (n/2)-1.

2.2.5 The Overall Operation Flow

In summary, by combing the leading-one bit detection scheme, the residual recoding technique, and the on-line variable scale factor compensation, we have a CORDIC algorithm as detailed by the following steps:

- (1) Set the initial iteration number i = 0, initial residual angle $z_0 = \theta$, initial rotation vector $(x_0, y_0) = (x, y)$, and initial exponent residual $T_0 = 0$. If $\theta = 0$, then (x', y') = (x, y), and exit the rotation iteration. Otherwise, proceed to step (2).
- (2) Check leading-one bit position k and obtain z_{i,r} of z_i. If z_i≠0, go to step (3). Otherwise, z_i = 0: rotation operations are completed and set the total iteration number *I*=*i*-1; go to step (5).
- (3) Using $z_{i,r}$ retrieve the optimized m and n of δ_m and δ_n , and then get the value of $\tan^{-1}2^{-m}$ and $\tan^{-1}2^{-n}$ from lookup tables. To perform the iteration as shown in equation (2.5) and $z_{i+1} = z_i - (\tan^{-1}2^{-m} + \tan^{-1}2^{-n})$. And the scale variable compensation:

If
$$i < (n/4 - 1)$$
, $x_{i+1} = x'_{i+1}(1 - 2^{-(2l_i + 1)})$
 $y_{i+1} = y'_{i+1}(1 - 2^{-(2l_i + 1)})$

We will store the compensation error, $e_i = m_i$.

If
$$i > (n/4-1)$$
, $x_{i+1} = x'_{i+1}(1+e_i 2^{-(2l_i+1)})$
 $y_{i+1} = y'_{i+1}(1+e_i 2^{-(2l_i+1)})$

(4) Set i=i+1, go to step (2).

(5) Calculation complete and the output values are (x_{i+1}, y_{i+1}) .

Fig. 2.13 shows the architecture for our new CORDIC processor. However, for the consideration of high-speed operations, they can be put in a pipelined structure in cascade. The pipelined structure is particularly efficient for the applications that require intensive and sustaining vector rotation operations.

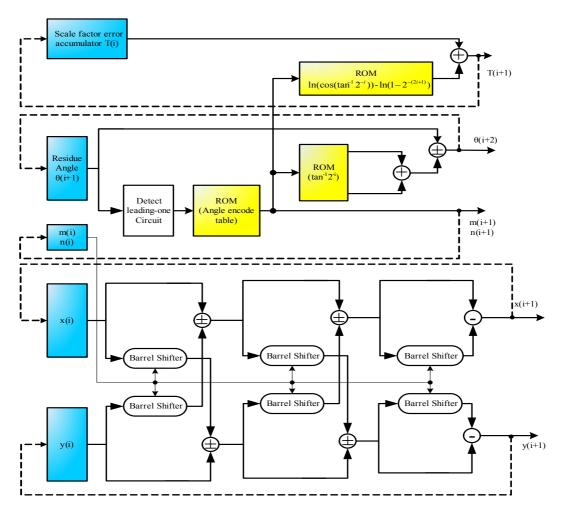


Fig. 2.13 The structure of new CORDIC algorithm

2.2.6 Simulations Results

Based on the structures shown in Fig. 2.13, we performed fixed-point hardware simulations using Matlab & Verilog hardware description language, assuming 8-bit, 12-bit and 16-bit accuracy (including 2-bit integer part). Exhausted simulations were conducted for all the rotation angles in the range of $0^{\circ} \sim 45^{\circ}$. The simulation result will be shown in the table 2.8.

	8	12	16	
	Angle composition	1.835	2.727	3.644
Average	Scale factor composition	1.786	3.092	4.153
	Overall iteration	2.437	3.482	4.424
	Angle composition	3	4	5
Worst case	Scale factor composition	4	5	6
	Overall iteration	4	5	6

Table 2.8 Simulation results in different output bits precision with our new CORDIC algorithm

3. Conclusion

In section 2.1, we propose an in-place memory-based variable-length FFT processor architecture, which is suited for multi-mode and multi-standard OFDM systems including 802.11a, 802.16a, DAB, DVB-T, and VDSL. The design is featured with the following low-complexity components including: a butterfly PE, a variable-length data address generator, and a variable-length coefficient address generator. The design is published in ISCAS'04 and currently under final EDA realization. The design will be taped out soon in a few weeks. Due to page limitation, we just include our results on channel estimation in the appendix. The result is a high-performance DCT-based channel estimation algorithms which is accepted by ICC04.

In addition, the new CORDIC algorithm considerably reduces the iteration number efficiently. It is achieved by combining several design techniques, including efficient high radix rotation scheme, angle encoding, leading-one bit detection, and on-line variable factor compensation. Our further work is to implement this new CORDIC-based PE for FFT processors of OFDM systems.

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DESIGN OF AN EFFICIENT VARIABLE-LENGTH FFT PROCESSOR

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ABSTRACT

In this paper, we propose an efficient variable-length FFT processor architecture suitable for multi-mode and multi-standard OFDM communication systems. The FFT processor is based on radix-2² DIF FFT algorithm and also supports non-power-of-4 FFT computation. The design contains an efficient processing element (PE), which can execute radix- 2^2 butterfly (BF) operations, as well as radix-2 BF operations. Moreover, in order to achieve high-performance variable-length FFT operations and data accesses, an efficient variable-length address generator and twiddle factor generator are designed. The design has the merits of low complexity and high speed performance. The designs consider seven different FFT lengths including 64, 256, 512, 1024, 2048, 4096, and 8192 points, which cover all the required FFT lengths by 802.11a, 802.16a, DAB, DVB-T, VDSL and ADSL.

1. INTRODUCTION

Fast Fourier Transform (FFT) unit, is one of the critical components in OFDM (orthogonal frequency division multiplexing) systems. Because of high real-time throughput rate demand by current OFDM systems, such as ADSL, VDSL, 802.11a, 802.16, DAB, and DVB-T, an efficient FFT processor is required for real-time operations.

FFT architectures can be categorized as two types: the pipelined architectures and the memory-based architectures [1], [2], [3]. For hardware simplicity, this work only focuses on memory-based designs. Memory-based architectures generally include a single butterfly PE (or more than one to enhance computation power), a centralized memory block to store input or intermediate data, and a control unit to handle memory accesses and data flow direction.

Since the existing OFDM communication systems all have similar baseband architectures and FFT/IFFT operations, it is advantageous to design a single variable-length memory-based FFT/IFFT module suitable for multi-mode and multi-standard operations. With this consideration, there are many design problems to be addressed and overcome for the realization of an efficient variable-length FFT/IFFT processor. Some of the key design issues include: (1) a high-performance PE capable of executing FFT butterfly operations for various FFT algorithms; (2) a high-performance data-address generator that supports in-place variable FFT length data accesses; (3) an efficient multi-bank memory structure that support low cycle-count conflict-free data accesses; (4) an efficient address generator for variable-length twiddle factor accesses or generations.

There are some PE designs in the literature [1], [4], [5]. Here we adopt the conventional multiplier-and-adder based butterfly structure, based on radix-4 FFT algorithm, and also consider general power-of-two FFT operations. For the complex multiplication, four real multipliers are replaced by three multipliers. For the design of variable-length address generator, not much was proposed in the past. However, there are some efficient conflict-free in-place memory addressing schemes [2], [3], [5], [6]. All these designs require area-consuming barrel shifters. We will propose a much efficient design which has a small area, meanwhile supports variable-length FFT data addressing. Correspondingly, we will also need a four-bank memory that matches the in-place memory address generator for high-bandwidth data access.

For twiddle factor addressing and generation, we propose an on-line generation design, which has a much smaller area and higher speed than conventional ROM-based designs. The design is detailed in [7].

2. MEMORY-BASED FFT ARCHITECTURES

A general memory-based FFT processor structure mainly consists of a PE, a main memory, ROM for twiddle factor storage, and a controller. The main memory stores processed data. The controller contains three functional units: data memory address generator, coefficient index generator, and operation state controller. The Butterfly PE is responsible for the butterfly operations required by FFT operations.

For performance consideration, ideally the PE should simultaneously fetch r complex data from memory then write back r complex computed output data to the data

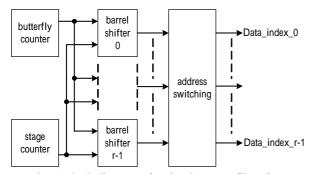


Fig. 1 Block diagram of an in-place, conflict –free, multi-bank data address generator

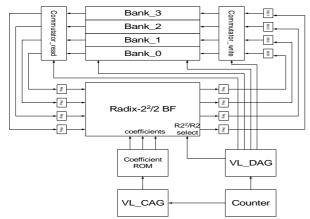


Fig. 2 Block diagram of the proposed variable-length FFT processor

memory. Therefore, memory design should consider multi-bank data addressing and partition the memory into r banks for r concurrent conflict-free data accesses. There are some efforts on memory partition and addressing methods to achieve conflict-free memory access [5], [6]. In summary, those approaches can be described by the following efficient functions [5]:

$$n = \lceil \log_{r} N \rceil$$

$$Data _count = [d_{n-1}d_{n-2}.....d_{2}d_{1}d_{0}]_{r} \qquad (1)$$

$$Bank _index = (\sum_{i=0}^{n-1} d_{i}) \bmod r$$

Data _ index = $[d_{n-1}d_{n-2}....d_2d_1]_r$

Those mapping functions are efficient in that they are regular and simple for varying butterfly operations and conflict-free memory accesses. They can be realized by the data address generator structure shown in Fig. 1 [5]. In the figure, data_index_n is the new address in the assigned memory bank. The butterfly counter value indicates the sequence number of a butterfly operation from 0 to N/r. This counter value is appended a symbol value to its LSB, ranging from 0 to r-1, and shifted left by an amount equal to the content of the stage counter.

These r input data addresses for butterfly PE are translated to r corresponding bank indices and addresses

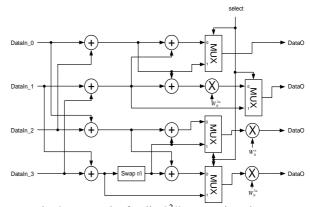


Fig. 3 Data path of radix- $2^{2/2}$ processing element within the memory banks. This facilitates r simultaneous conflict-free read operations from the r memory banks. Although this address generator is very efficient, it is area consuming, and it is only suitable for fixed-length FFT operations. Later, we will propose a variable-length address generator with smaller area than the design of Fig. 1.

3. THE PROPOSED VARIABLE-LENGTH FFT ARCHITECTURES

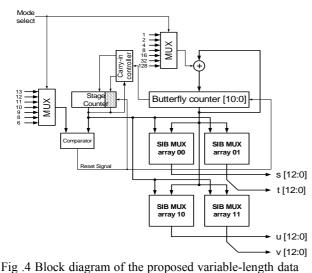
Our design is an 8192-point variable-length FFT processor suited for various FFT lengths of 802.11a, 802.16, DAB, DVB-T, and VDSL. Block diagram of our design is shown in Fig. 2.

3.1 The Butterfly PE

Although our design is based on radix-2² DIF FFT algorithm, we can still compute a general power-of-2 FFT by adding some minor modification to the radix-2² datapath. The unified radix-2²/2 datapath is shown in Fig. 3. In the figure, the control line "select=0" programs the PE as radix-2² mode so as to execute radix-2² algorithm, otherwise, the four adders on the right hand side and the multiplier W_{N}^{2n} is bypassed so that the PE is configured as radix-2 mode such that two radix-2 butterflies are processed simultaneously. The "swap r/i" unit, that interchanges real part with imaginary part, is to implement the required multiplication with "-j". This shared hardware design does not increase the complexity of data address generator.

3.2 The variable-length data address generator (DAG)

The proposed data address generator significantly improves the address generator mentioned in section 2, by considering radix- 2^2 DIF FFT algorithm and variable-length FFT operations, and by simplifying the original area-consuming barrel-shifter based designs with a few simpler multiplexer-based addressing functions. The four addresses required by radix- 2^2 butterfly PE in power-of-4 point FFT correspond to the 4 different banks. The



addresses of the generator addresses are denoted as <s, t, u, v> which can be calculated by the following equations. $s = [i_{\log_4 N-2} i_{\log_4 N-3} \dots i_{\log_4 N-1-k} 0 i_{\log_4 N-2-k} i_{\log_4 N-3-k} \dots i_1 i_0]_4$ $t = [i_{\log_4 N-2} i_{\log_4 N-3} \dots i_{\log_4 N-1-k} 1 i_{\log_4 N-2-k} i_{\log_4 N-3-k} \dots i_1 i_0]_4$ $u = [i_{\log_4 N-2} i_{\log_4 N-3} \dots i_{\log_4 N-1-k} 2 i_{\log_4 N-2-k} i_{\log_4 N-3-k} \dots i_1 i_0]_4$ $v = [i_{\log_4 N-2} i_{\log_4 N-3} \dots i_{\log_4 N-1-k} 3 i_{\log_4 N-2-k} i_{\log_4 N-3-k} \dots i_1 i_0]_4$ (2) where $i = [i_{\log_4 (N)-2} i_{\log_4 (N)-3} \dots i_2 i_1 i_0]_4$ is the

where $l = \lfloor l_{\log_4(N)-2} l_{\log_4(N)-3} \dots l_2 l_1 l_0 \rfloor_4$ is the butterfly counter content, and k is the stage counter content.

On the other hand, in non-power-of-4 point FFT operations, the radix-2² butterfly should be reconfigured as two radix-2 butterflies in the first stage of FFT operations. Hence, the data address generator should provide two different address-generation modes to accommodate both power-of-4 and non-power-of-4 point FFT operations.

In the first stage of non-power-of-4 FFT operations, data addresses $\langle s, t, u, v \rangle$ required by butterfly PE are generated by the following equations.

$$s = \begin{bmatrix} 0 & j_{\log N-1} & j_{\log N-2} & \dots & j_2 & j_1 & j_0 \end{bmatrix}_2$$

$$t = \begin{bmatrix} 01 & j_{\log N-1} & j_{\log N-2} & \dots & j_2 & j_1 & j_0 \end{bmatrix}_2$$

$$u = \begin{bmatrix} 10 & j_{\log N-1} & j_{\log N-2} & \dots & j_2 & j_1 & j_0 \end{bmatrix}_2$$

$$v = \begin{bmatrix} 11 & j_{\log N-1} & j_{\log N-2} & \dots & j_2 & j_1 & j_0 \end{bmatrix}_2$$
(3)

where j is bit-wise representation of butterfly counter content and N is the longest FFT length supported. The generalized data address generation equations are:

$$\begin{split} s &= [j_{\log N-1} \ j_{\log N-2} \dots j_{\log N-K} \ 0 \ 0 \ j_{\log N-K-1} \ j_{\log N-K-2} \dots j_1 \ j_0]_2 \\ t &= [j_{\log N-1} \ j_{\log N-2} \dots j_{\log N-K} \ 0 \ 1 \ j_{\log N-K-1} \ j_{\log N-K-2} \dots j_1 \ j_0]_2 \\ u &= [j_{\log N-1} \ j_{\log N-2} \dots j_{\log N-K} \ 1 \ 0 \ j_{\log N-K-1} \ j_{\log N-K-2} \dots j_1 \ j_0]_2 \\ v &= [j_{\log N-1} \ j_{\log N-2} \dots j_{\log N-K} \ 1 \ 1 \ j_{\log N-K-1} \ j_{\log N-K-2} \dots j_1 \ j_0]_2 \\ (4) \end{split}$$

where *K* is a special stage counter content, which is increased by one each time when all the radix-2 butterfly operations within the current stage are completed, or increased by two after one stage of radix- 2^2 butterfly operations is completed.

The hardware block diagram of variable-length data address generator for our FFT processor capable of executing 8192, 4096, 2048, 1024, 512, 256, and 64-point FFTs is shown in Fig. 4. In the figure, "carry-in controller" adds the carry-out signal from butterfly counter to the LSB (the shaded area) or its left immediate bit of the stage counter to alternate the counter step of the stage counter between one and two; "comparator" compares stage counter content with the maximum stage count corresponding to each FFT length and reset all counters if they are equal; input signal "mode select" controls the butterfly counter step and maximum stage count to vary FFT length; "SIB MUX array" denotes shift-insertion-bypass multiplexer array. It greatly simplifies the address generator of Fig. 1, as will be detailed below.

In our design, we define several functions to simplify the design to replace those area-consuming barrel shifters with much simpler multiplexers. The functions include the required left shift operations, symbol bit insertion operations, and bypass the remaining bits, for the realization of the variable-length data address generation algorithm. Detailed architecture of the shift-bypass-insertion multiplexer array is shown in Fig. 5.

In the figure, the input signal "symbol" to MUX_n module can be 00, 01, 10, or 11, where block diagram of MUX_n is shown in Fig. 6, and function of MUX_n output is explained in Table 1. Timing and area comparisons of data address generator between SIB-MUX array approach and barrel shifter approach are shown in Table 2, and the result is synthesized by TSMC 0.25 μ m standard cell library with Synopsis Design Analyzer.

3.3 The variable-length coefficient address generator

Instead of using conventional ROM-based twiddle factor generation scheme, we propose a new twiddle factor generator, which has a smaller area and a higher speed than the ROM-based design. The design is presented in [7]. We will not detail it here. However, if conventional ROM-based twiddle factor generation is adopted, we can use the following efficient twiddle factor address generator, as detailed below. The basic coefficient address generating function is mainly a counter with an adjustable counting step to realize varying stages and allow for varying FFT lengths. Hence, we can realize the coefficient address generator based on the content of the butterfly counter. Coefficient address w for the i-th butterfly of the k-th stage in radix-2, $N/2^c$ -point DIF FFT can be generated based on the following equation:

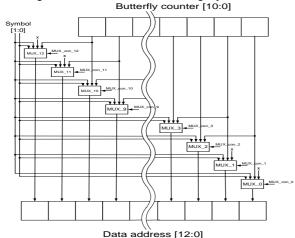


Fig. 5 The architecture of Shift-insert-bypass MUX array Table 1 Output functions of the MUX n.

Output	Function
Insert symbol	Select symbol bit 0 as the n-th bit of data
0 (I0)	address.
Insert symbol	Select symbol bit 1 as the n-th bit of data
1 (I1)	address.
Bypass (BP)	Select the n-th bit of butterfly counter as the
	n-th bit of data address.
Shift 2 (S2)	Select the (n-2)-th bit of butterfly counter as
	the n-th bit of data address.

Table	2 Comparison (of DAG	units.
		-	1 1 . 0

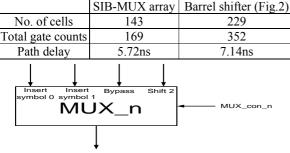


Fig. 6 Block diagram of MUX_n module

w

$$= (i \times 2^{c+k}) \mod(\frac{N}{2})$$

where N is the longest FFT length and w is from 0 to N/2-1 that corresponds to coefficient from W_N^0 to $W_N^{\frac{N}{2}-1}$. As mentioned previously, the content of butterfly counter is i*2^c, where 2^c is the ratio of longest FFT length

to the current processed FFT length. Hence, coefficient address w can be derived from

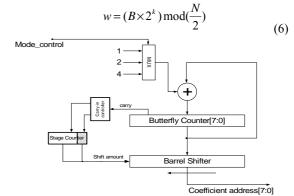


Fig. 7 The variable-length coefficient index generator. where B is the content of butterfly counter. In a fixed-radix design, equation (6) can be implemented by shifting the content of butterfly counter to left by an amount related to the stage counter's content. Furthermore the stage counter unit is similar to Fig. 4. The hardware block diagram which depicts a coefficient address generator for 512, 256, and 128-point FFT is shown in Fig 7.

4. CONCLUSION

In the paper, we propose an in-place memory-based variable-length FFT processor architecture, which can suit for multi-mode and multi-standard OFDM systems including 802.11a, 802.16a, DAB, DVB-T, and VDSL. The design is featured with the following low-complexity components including: a butterfly PE, a variable-length data address generator, and a variable-length coefficient address generator. The design is currently under final EDA realization and will be reported in the final paper.

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APPENDIX 2: Paper Accepted by Internaitonal Conference on Communications, June, 2004, Paris, France

DCT-Based Channel Estimation for OFDM Systems

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Abstract—In this paper, based on the property of channel frequency response and the concept of interpolation in transform domain, we propose two discrete cosine transform (DCT)-based pilot-symbol-aided channel estimators, which can mitigate the aliasing error and high-frequency distortion of the direct discrete Fourier transform (DFT)-based channel estimators when the multipath fading channels have non-sample-spaced path delays. Both proposed estimators outperform the conventional DFT-based channel estimators. Of these two DCT-based estimators, one has its performance close to MMSE estimator, while the other one has the advantage of easy implementation with a little performance degradation. Furthermore, in implementation, the DCT-based estimators have the advantages of utilizing mature fast DCT algorithms and architectures, which is favorable to matrix-based channel estimators.

Keywords-OFDM; channel estimation; FFT; DCT; interpolation

I. INTRODUCTION

Multicarrier systems have received much attention these days. It is a promising technique for high data rate transmission. Examples include wireless OFDM systems, such as IEEE 802.11a wireless LAN, IEEE 802.16a wireless MAN, DAB and DVB-T systems, and the wired DMT systems, such as ADSL and VDSL systems. They are robust to multipath inter-symbol interference (ISI). However, they still suffer from multipath frequency-selective fading. To remove the channel effect and do accurate data demodulation, one has to perform accurate channel estimation.

The optimal interpolation filtering in minimum mean square error (MMSE) sense is a well-known channel estimator [1], [2]. However, the statistical characteristics of a channel, i.e., autocorrelation matrix of channel frequency response and signal-to-noise ratio (SNR), must be obtained in advance. Usually this is impossible because of wide-varying channel conditions. An alternative is to use recursive least-square (RLS) method to track the channel [3]. Although RLS algorithm is quite effective, high computation complexity is a serious disadvantage. In [1], [2], the authors proposed a robust approach in which the actual autocorrelation matrix is replaced by a properly approximated matrix with small mismatch and performance loss. Although reasonable suboptimal solution is achievable using this algorithm, the required computation complexity is still very high. Hence it may not be practical.

Another popular estimator is DFT-based interpolator [4], [5]. The DFT-based channel estimator can theoretically achieve ideal lowpass interpolation and has the advantage of Sau-Gee Chen Department of Electronics Engineering and Institute of Electronics 1001 Ta Hsueh Rd Hsinchu, Taiwan, ROC

low complexity by exploiting FFT algorithm. This works well when the interpolated signal is originally band-limited. For channel frequency response to be interpolated and estimated, this condition corresponds to time-limited channel impulse response. This is true when the multipath delays are all integer multiples of the sampling time and short enough so as not to cause aliasing error, if it is obtained from the IDFT of a limited number of pilot frequency responses.

If there exists any non-sample-spaced path delay, the equivalent discrete channel impulse response will be dispersive in time domain. As a result, the DFT-based interpolation process will be using the aliased data of the dispersive impulse response. This results in considerable performance degradation. To alleviate the problem, recently we proposed a DCT-based channel estimation algorithm [8] (termed DCT/EIDCT channel estimator), which is much effective than the conventional DFT-based channel interpolation algorithms. The algorithm can effectively reduce the aliasing error and achieve better interpolation performance than the popular DFT-based methods. In this paper, we will provide a more generalized and complete treatment on the DCT-based channel estimation. In addition to reviewing our recently proposed DCT/EIDCT-based channel estimation algorithm, we will also propose a fast DCT algorithm for its low-complexity realization, plus that we will propose another DCT-based channel estimator (termed IDCT/DCT-based channel estimator). The new DCT-based channel estimators also has a much better performance than the conventional DFT-based channel estimators, while is comparable with the DCT/EIDCT method. In addition, the new DCT-based channel estimators have the advantages of utilizing mature fast-DCT algorithms and architectures. They can be implemented with even lower complexity compared with DFT-based channel estimators

In section 2, we will describe the OFDM system model and DFT-based channel estimators. Two new DCT-based channel estimators will be introduced in section 3, followed by their simulation results in section 4 and finally the conclusion.

II. OFDM SYSTEM MODEL AND DFT-BASED CHANNEL ESTIMATORS

A. OFDM System Model

First, the transmitted data is split into several low-rate streams and then these data streams are transmitted in different subcarriers. We assume the data transmitted at the k-th

This work was supported by National Science Council, Taiwan, under the grant contracts NSC 92-2219-E-009 -017 and NSC 92-2220-E-009 -021

subcarrier is d(k). The multicarrier modulation is done by inverse discrete Fourier transform (IDFT) as

$$x(n) = \frac{1}{N} \sum_{k=0}^{N-1} d(k) e^{j2\pi n k/N} \qquad n = 0, 1, 2, \Lambda, N-1$$
(1)

where N is the total number of subcarriers. Then before transmitting x(n), cyclic prefix is inserted to prevent ISI and ICI.

The time-varying multipath channel can be characterized by

$$h(t,\tau) = \sum_{l=0}^{\nu-1} \alpha_l(t) \delta(\tau - \tau_l)$$
⁽²⁾

where ν is the number of paths, α_i is the path gain and τ_i is path time delay. Usually $\alpha_i(t)$'s are modeled as complex Gaussian processes with Jakes' power spectrum [6], and all the delay paths are uncorrelated to each other. This is so-called the multipath Rayleigh fading channel. The mean-square value of $\alpha_i(t)$ is usually described by a exponentially-decayed function with respect to the path delay time τ_i , which has the form of

$$E\left[\left|\alpha_{l}(t)\right|^{2}\right] = e^{\frac{\tau_{l}}{\sigma}}$$
(3)

where σ is the power delay time constant. Another important issue about path gain is the variation along time direction. Doppler frequency is commonly used as an indicator of the variation rate and is defined as

$$f_d = f_c \mathbf{v}/\mathbf{c} \tag{4}$$

where f_c is the carrier frequency, v is the vehicle speed and c is velocity of light.

If the channel length is shorter than the cyclic prefix, the received signal can be expressed as

 $y(n) = x(n) \otimes h(n) + \tilde{n}(n)$ $n = 0,1,2,\Lambda$, N-1 (5) where \otimes denotes circular convolution, $\tilde{n}(n)$ is additive white Gaussian noise, and h(n) is the equivalent discrete channel impulse response (assuming the channel is fixed over an OFDM symbol) as described by [7]

$$h(n) = \frac{1}{N} \sum_{l=0}^{\nu-1} \alpha_l e^{-j\frac{\pi(n+(N-l)\tau_l)}{N}} \frac{\sin(\pi\tau_l/T_c)}{\sin(\pi(\tau_l/T_c-n)/N)} \qquad n = 0, 1, 2, \Lambda, N-1$$
(6)

where T_c is the sampling period. Then the received signal at each subcarrier can be obtained by performing discrete Fourier transform (DFT) on y(n) as

$$Y(k) = \sum_{n=0}^{N-1} y(n) e^{-j2\pi i k \cdot N} = X(k) H(k) + N(k)$$

$$H(k) = \sum_{l=0}^{\nu-1} \alpha_l e^{\frac{-j2\pi i k \cdot r_l}{NT_c}}, \quad N(k) = \sum_{n=0}^{N-1} \widetilde{n}(n) e^{-j2\pi i k \cdot N}, \quad k = 0, 1, 2, \Lambda, N-1$$
(7)

A. The DFT-Based Channel Estimators [5]

For simplicity, the DFT-based estimators can be summarized by the following steps:

1) Perform the least-square (LS) estimation [7] of channel response at the pilot subcarriers:

$$H_{p}(k) = Y_{p}(k) / P(k) = H_{p}(k) + N_{p}(k) / P(k) = H_{p}(k) + N_{p}(k)$$
(8)

$$Y_p(k) = Y(Nk/M)$$
 $k = 0,1,2,\Lambda, M-1$ (9)

where P(k) is the prior known data transmitted at pilot subcarriers.

2) Perform phase rotations of the pilot subcarrier channel response:

$$\hat{H}'_{p}(k) = \hat{H}_{p}(k) \times e^{j\pi \frac{\omega_{n}}{M}}$$
(10)

where Δ is the minimum integer larger than τ_{max}/T_c , and τ_{max} is the maximum path delay time. The phase shift is equivalent to time shift by $-\Delta/2$ units of the channel impulse response. Doing so, the power of channel impulse response is roughly centered around n = 0.

3) Perform IDFT of $\hat{H}'_{n}(k)$:

$$\hat{h}_{p}(n) = IDFT\left\{\hat{H}'_{p}(k)\right\} = \frac{1}{M} \sum_{k=0}^{M-1} \hat{H}'_{p}(k) e^{j\frac{2\pi nk}{M}} \quad n = 0, 1, 2, \Lambda, M-1$$
(11)

4) Increase channel samples by padding zeros to $\hat{h}_p(n)$:

$$\hat{h}(n) = \begin{cases} \hat{h}_{p}(n) & 0 \le n \le M/2 - 1\\ 0 & otherwise\\ \hat{h}_{p}(M+n-N) & N - M/2 \le n \le N - 1 \end{cases}$$
(12)

5) Interpolate channel response by performing $DFT[\hat{h}(n)]$:

$$H'(k) = \sum_{n=0}^{N-1} \hat{h}(n) e^{-j\frac{2\pi nk}{N}} \qquad k = 0, 1, 2, \Lambda, N-1$$
(13)

6) Restore the phase of interpolated channel response:

$$\hat{H}(k) = H'(k) \times e^{-j\pi \frac{2k}{N}}$$
 $k = 0, 1, 2, \Lambda, N-1$ (14)

II. THE PROPOSED DCT-BASED CHANNEL ESTIMATORS

DFT of a set of N-point data is equivalent to the discrete-time Fourier transform (DTFT) of the infinite-length periodical signals extended from the original N-point data. Therefore, if it is discontinuous between two ends of the *N*-point data, there will be an abrupt variation in between the period boundaries. As a result, there are high frequency components in the DFT results. Under this condition, the DFT results are quite different from the desired frequency response of the original aperiodic signal, which has smaller high-frequency components. In addition, those high-frequency components will generate large aliasing errors accordingly, in the channel interpolation process. Therefore, in this case, we have a high tendency of getting error-prone interpolated channel frequency samples. As such, those high-frequency errors should be avoided in the frequency-domain process as possibly as it can be. To achieve this goal, let's review the characteristics of a multipath channel of (6). We can find that when the multipath time delays are all sample-spaced (τ_i 's are all integer multiples of sampling period), the equivalent channel impulse response is time-limited. Therefore, in this case, DFT-based channel estimator works well. However, when the multipath time delays are non-sample-spaced, the power of channel impulse response is dispersive to the length of an OFDM symbol. In this case, the number of pilot subcarriers is normally insufficient and under-sampled. Hence, the introduced aliasing errors due to the under-sampled pilot channel responses will severely degrade the performance of DFT-based channel estimators.

Discrete cosine transform (DCT) is a well-known technique widely used in image processing. Compared with DFT, DCT can reduce high-frequency components in the transform domain by eliminating the effect of discontinuous edge in DFT-based approach, as mentioned before. The reason is that operation of an N-point DCT is equivalent to extending the original N-point data to 2N points by mirror extension, followed by 2N-point DFT of the extended data and their constant magnitude and phase compensation. Obviously, the operation of mirror extension can solve the signal discontinuity problem introduced in the DFT-based interpolation process. Therefore, DCT-based interpolation is expected to have better power concentration in low-frequency region and a better frequency approximation to the frequency response of the original channel impulse and lower aliasing error, than the DFT-based interpolation. In the following, we will describe the DCT-based channel estimators in detail.

A. The DCT/EIDCT-Based Channel Estimator & Its Fast Algorithm

We already proposed this estimator in [8]. Here for the completeness and convenience of later discussion and performance comparison we will first review its approach, and then propose a fast algorithm for its low-complexity realization, as follows. Since the idea is to make the data symmetric by mirror-extending the original data to get the periodic continuous signal. With the extended data, we can use the well-known DFT-based interpolator to estimate the channel frequency response with less aliasing effect and achieve better interpolation performance. Due to the symmetry property of input data, the DFT/IDFT operations in the interpolation process can be replaced by DCT-related ones. Therefore, we can get the equivalent interpolator based on DCT-related operations.

The DCT-based estimation is depicted in Fig. 1 and described by the following operation steps:

1) First, the same as DFT-based estimator, frequency response is estimated by LS method. Then instead of performing IDFT operation, DCT is used to transform the pilot frequency response as shown below:

$$\hat{h}_{c}(m) = w(m) \sum_{k=0}^{M-1} \hat{H}_{p}(k) \cos \frac{(2k+1)\pi m}{2M} \qquad m = 0, 1, \Lambda, M-1$$

$$w(m) = 1/\sqrt{M}, \ m = 0; \quad w(m) = \sqrt{2/M}, \ m \neq 0$$
(15)

2) Pad zero to the DCT-transformed data to obtain the desired signal in the transform domain:

$$\hat{h}_{N}(m) = \begin{cases} \hat{h}_{c}(m) & 0 \le m \le M - 1 \\ 0 & M \le m \le N - 1 \end{cases}$$
(16)

3) Finally, the estimated channel frequency response is obtained by performing extendible IDCT (EIDCT) [9] on $\hat{h}_{y}(m)$.

$$\hat{H}(k) = \sum_{m=0}^{M-1} w(m) \hat{h}_c(m) \cdot \cos\left(\frac{(2k+N/M)}{2N}\pi n\right) \qquad k = 0, 1, 2, \Lambda, N-1 \quad (17)$$

If N/M is even, this equation can be translated to the (N+1)-point type I IDCT [10] with some shift. On the other

hand, if N/M is odd, this equation is equivalent to conventional IDCT with shift equal to (N/M-1)/2. Therefore, the EIDCT can be

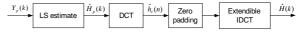


Figure 1. The DCT/EIDCT-based channel estimator.

implemented efficiently either by conventional fast IDCT algorithms or by fast type-I IDCT algorithms.

B. The IDCT/DCT-Based Channel Estimator

The DCT/EIDCT-based channel estimator has the advantage of low complexity and can reduce the aliasing error in channel interpolation compared with DFT-based estimator. Here, we will propose a different DCT-based channel estimator whose performance is very close to DCT/EIDCT-based channel estimator and is also much better than the DFT-based channel estimators. The advantage of this estimator is that it can be implemented with conventional DCT and IDCT software and hardware. Therefore, for the implementation consideration, this estimator is more favorable than our previously proposed DCT/EIDCT channel estimator.

The basic idea is still to make the data symmetric so as to reduce the high-frequency components, but perform IDCT on channel frequency response instead of DCT. Although direct mirror-extension is a quite suitable approach, it is not the only one. Here we adopt a different approach which defines the extended pilot channel frequency response as

$$\hat{H}_{2M}(k) = \begin{cases} \hat{H}_{p}(k) & 0 \le k \le M - 1\\ 0 & k = M\\ \hat{H}_{p}(2M - k)e^{\frac{j\pi(2M - k)}{M}} & M + 1 \le k \le 2M - 1 \end{cases}$$
(18)

The reason for this design is all for the compatibility with the conventional inverse discrete cosine transform. In the conventional DCT coefficients, there is always a zero response at the index *M* for an *M*-point DCT and magnitudes of the DCT coefficients are symmetric with respect to this zero. In this design, although inserting a zero at k = M would cause a rapid response dip, the high frequency component would not be significant due to data symmetry property. Therefore, interpolation by using $\hat{H}_{2M}(k)$ would be better than the original data $\hat{H}_{n}(k)$.

With $\hat{H}_{2M}(k)$, we can perform its IDFT-based interpolation to get the estimated channel frequency response. Since we have properly designed $\hat{H}_{2M}(k)$, the whole interpolation process can be translated to DCT-based operation. The new IDCT/DCT-based interpolator is shown in Fig. 2.

1) First, multiply $\hat{H}_{n}(k)$ by a gain factor defined by

$$\hat{H}'_{p}(k) = \begin{cases} \frac{1}{\sqrt{2}} \hat{H}_{p}(k) & k = 0 \\ \frac{1}{\sqrt{2}} e^{\frac{j\pi k}{2M}} \hat{H}_{p}(k) & 1 \le k \le M - 1 \end{cases}$$
(19)

2) $\hat{H}'_{r}(k)$ is transformed to time domain by IDCT

$$\hat{h}(n) = \sum_{k=0}^{M-1} w(k) \hat{H}_{p}(k) \cos \frac{\pi (2k+1)n}{2M} \quad m = 0, 1, \Lambda, M-1$$
(20)

3) Pad zeros to the end of $\hat{h}(n)$ and extend the data to N points to obtain the desired signal in time domain.

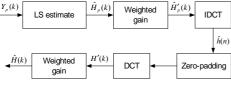


Figure 2. IDCT/DCT-based channel estimator.

4) Transform the extended data to frequency domain by *N*-point DCT.

5) Finally, a weighted gain is applied to each DCT coefficient to obtain the final interpolated channel response as shown below

$$\hat{H}(k) = \begin{cases} \sqrt{\frac{2N}{M}} H'(k) & k = 0 \\ \sqrt{\frac{N}{M}} e^{\frac{j\pi k}{2N}} H'(k) & 1 \le k \le N - 1 \end{cases}$$
(21)

We can find that the whole interpolation process only involves conventional DCT and IDCT operations. Therefore, it can be implemented directly by conventional fast DCT and IDCT algorithms and architectures. This is more convenient than our previously proposed DCT/EIDCT channel estimation algorithm in practical applications.

As mentioned before, the interpolated channel response will go down to zero for the frequency location beyond the last pilot frequency position. This is because the corresponding DFT-based interpolation puts a zero at k=M (18) due to symmetry of time-domain signal, which certainly leads to the descent in that region. However, this will not affect other region significantly due to the symmetry property. Therefore, if we don't use the subcarriers beyond the last pilot as usually is the case, the performance will be close to DCT/EIDCT-based interpolator.

The frequency responses at the pilot subcarrier frequencies are the down sampled version of the complete channel frequency responses at all the N subcarrier frequencies. To avoid severe aliasing, the delay of multipath channel cannot be too large. Since the operations of these two DCT-based estimators are both real, the interpolations are also real processes, that is, the real part and imaginary part of the interpolated signal are only dependent on the real part and imaginary part of input data respectively. Therefore, the Nyquist criterion can be applied in this case. That is

$$\tau_{\text{max}} / T_{e} < N / 2D_{f} = M / 2 \tag{22}$$

where τ_{\max} is the maximum path delay duration and D_f is the ratio of N to M.

I. SIMULATION RESULTS

We assume a 16QAM OFDM system with a total number of subcarriers N = 1024 including 32 equispaced pilot subcarriers. The system occupies a bandwidth of 5MHz and the sampling period is $T_c = 0.2 \mu s$. The length of cyclic prefix is $T_g = 16T_c$ and then the duration of an OFDM symbol is equal to $208 \mu s$.

As for the transmission environment, a multipath Rayleigh fading channel is assumed and the channel is simulated by Jakes' model [6]. We choose the "Vehicular A" channel parameters defined by ETSI for the evaluation of UMTS radio interface proposals [11]. The multipath time delays τ_{l} 's and the average power of the multipath gains α_{l} 's of the "Vehicular A" channel are shown in Table 1. The Dominer fractionary is get to 50 Hz hence, $\zeta \tau_{l} = 0.01$

Doppler frequency is set to 50 Hz, hence $f_d T \approx 0.01$.

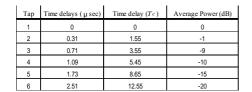
In the simulation, we assume perfect synchronization in the receiver. Since usually it is hard to estimate the channel frequency response beyond the last pilot accurately, this region is assigned as guard band. The system symbol error rate (SER) is shown in Fig. 3, while the mean-square error (MSE) of the estimated channel frequency response is shown in Fig. 4 It is obvious that the performances of DCT-based channel estimators are better than DFT-based channel estimator. In the DFT-based channel estimator, the aliasing error is large and as a result, it leads to inaccurate channel estimation and an error floor for the OFDM systems. In contrast, the DCT-based channel estimators can reduce the aliasing effect and improve the symbol error rate under high SNR conditions. In the figures, we also show the performance of robust LMMSE channel estimator [2] assuming the following correlation function of the channel frequency responses

$$E[H(k)H^{*}(l)] = \begin{cases} 1 & k = l \\ \frac{1 - e^{-j2\pi(T_{g}(k-l)/TN)}}{j2\pi\frac{T_{g}(k-l)}{TN}} & k \neq l \end{cases}$$
(23)

This correlation function corresponds to a uniform power delay profile where the multipath time delays are assumed to be uniformly and independently distributed over the length of the guard interval and all paths have the same average power. The performance of the robust LMMSE channel estimator is about 1dB better than DCT-based channel estimator, but the complexity of LMMSE channel estimator is much higher than the proposed DCT-based channel estimators.

We also show the SER and MSE for the case that all subcarriers except pilots are used to transmit data in Fig. 5 and Fig. 6 respectively. Although DCT-based channel estimator is still better than DFT-based estimator, there are error floors in all cases. This is because the aliasing error has significant effect beyond the last pilot. In this case, we can find that the performance of IDCT/DCT-based estimator degrades more compared with DCT/EIDCT-based estimator, due to the descent effect of the IDCT/DCT-based interpolation process. Considering this severe aliasing error, usually an OFDM system would not assign data subcarriers beyond two ending pilot subcarriers.

Table 1. Characteristics of ETSI "Vehicle A" channel environment



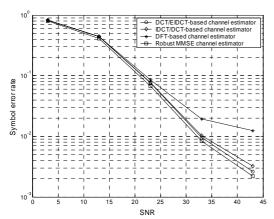


Figure 3. SER of channel estimators.

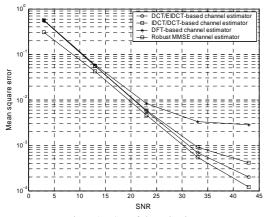
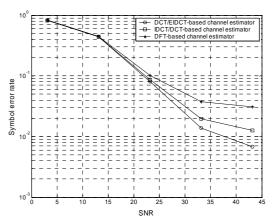


Figure 4. MSEs of channel estimators.

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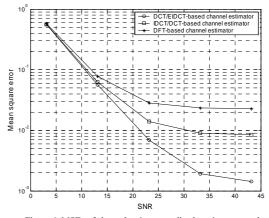


Figure 6. MSEs of channel estimators, all subcarriers are used.